

Lens Aberrations

Fundamentals

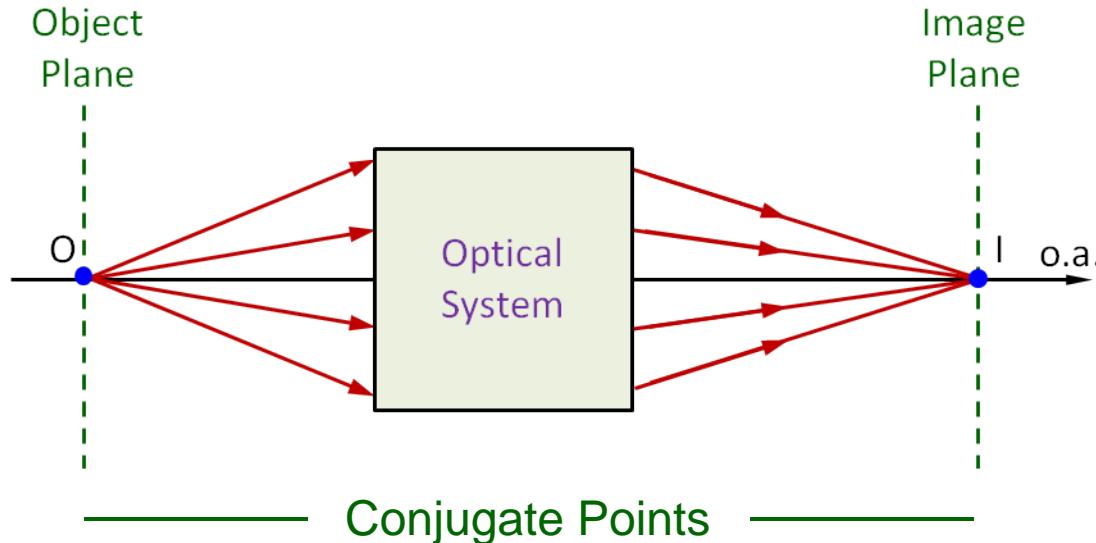
Optical Engineering

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Imaging



Imaging Limitations

- Scattering
- **Aberrations**
- Diffraction

F. L. Pedrotti and L. S. Pedrotti, Introduction to Optics, 2nd Ed., Prentice Hall, 1993.

Aberrations (3rd order – Seidel)

Chromatic



Monochromatic

Unclear
Image

Deformation
of Image

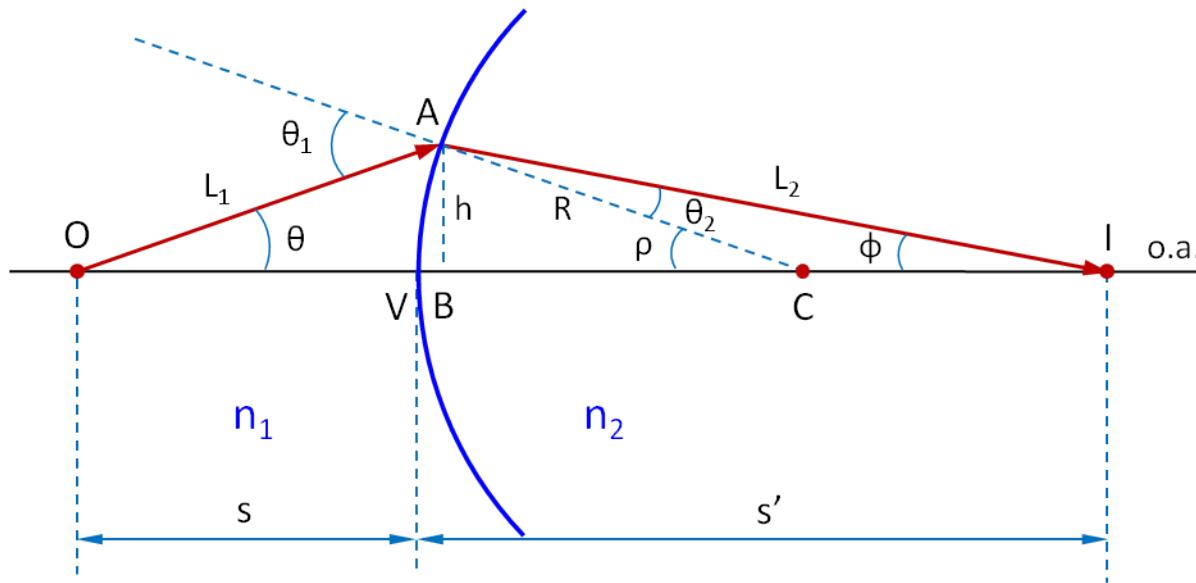
$$\sin x = x - \underbrace{\frac{x^3}{3!} + \frac{x^5}{5!}}_{3^{\text{rd}} \text{ order}} + O(x^7)$$

$$\cos x = 1 - \underbrace{\frac{x^2}{2!} + \frac{x^4}{4!}}_{3^{\text{rd}} \text{ order}} + O(x^6)$$

- Spherical
- Coma
- Astigmatism
- Field Curvature
- Distortion

optics.hanyang.ac.kr/~shsong/20-Aberration%20theory.pdf

Spherical Aberration



Paraxial Approximation:

$$\frac{n_1}{s} + \frac{n_2}{s'} = \frac{n_2 - n_1}{R}$$

Fermat's Principle: $OPL = n_1(OA) + n_2(AI) = n_1L_1 + n_2L_2$, where

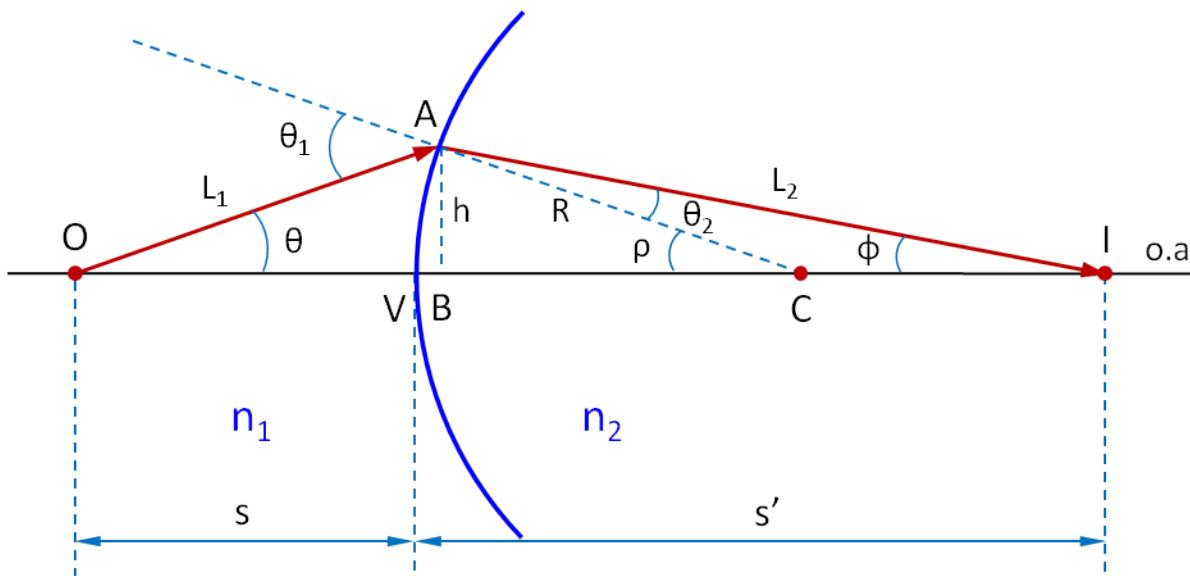
$$L_1 = [R^2 + (R+s)^2 - 2R(R+s)\cos\rho]^{1/2}, \quad \text{from OAC}$$

$$L_2 = [R^2 + (s'-R)^2 + 2R(s'-R)\cos\rho]^{1/2}, \quad \text{from IAC}$$

$$\frac{d(OPL)}{dh} = 0 \implies n_1 \frac{dL_1}{dh} + n_2 \frac{dL_2}{dh} = 0 \implies \left[n_1 \frac{dL_1}{d\rho} + n_2 \frac{dL_2}{d\rho} \right] \frac{d\rho}{dh} = 0 \implies$$

$$n_1 \frac{R(R+s)\sin\rho}{L_1} = n_2 \frac{R(s'-R)\sin\rho}{L_2},$$

Spherical Aberration (continue)



Fermat's Principle:

$$\frac{R^2}{\sin^2 \rho} \frac{1}{(s' - R)^2} + 2R \frac{\cos \rho}{\sin^2 \rho} \frac{1}{(s' - R)} + \frac{1}{\sin^2 \rho} = \frac{n_2^2}{n_1^2} \frac{L_1^2}{(R + s)^2 \sin^2 \rho}.$$

$$x^2 + \beta x + \gamma = 0, \quad \text{where}$$

$$\beta = 2 \frac{\sqrt{R^2 - h^2}}{R^2},$$

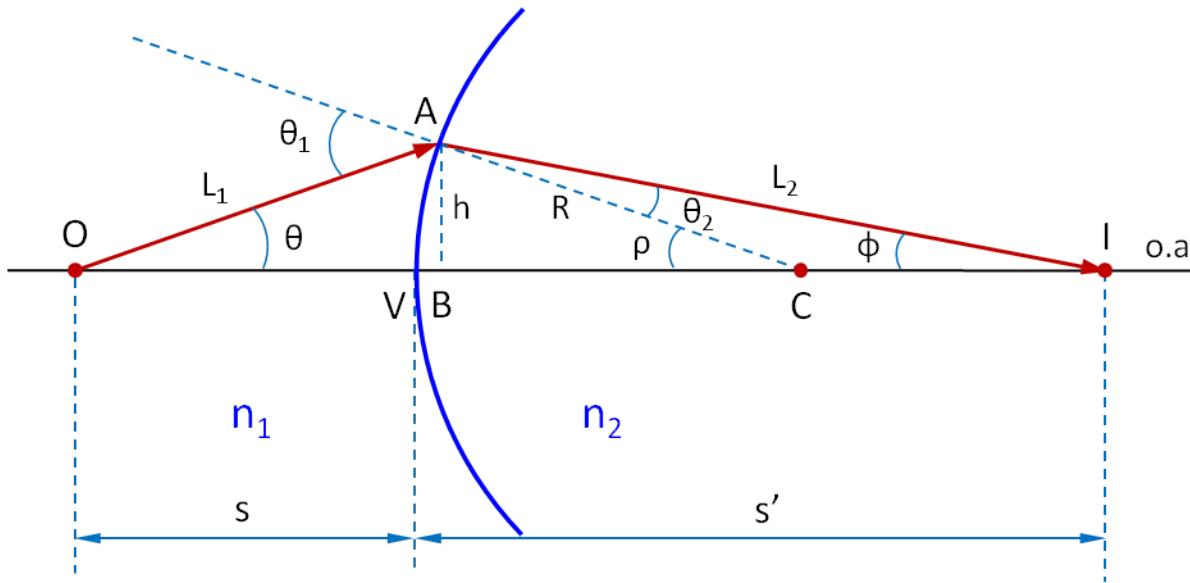
$$\gamma = \frac{1}{R^2} \left[1 - \frac{n_2^2}{n_1^2} \frac{L_1^2}{(R + s)^2} \right],$$

$$\Delta = \beta^2 - 4\gamma = \frac{4}{R^2} \left[-\frac{h^2}{R^2} + \frac{n_2^2}{n_1^2} \frac{L_1^2}{(R + s)^2} \right],$$

$$x_{1,2} = \frac{1}{s' - R} \Big|_{1,2} = \frac{-\beta \pm \sqrt{\Delta}}{2},$$

$$x_1 = (1/2)(-\beta + \sqrt{\Delta}) \rightarrow s' = (1/x_1) + R$$

Spherical Aberration (continue)



Using Trigonometry and Snell's Law:

$$\frac{\sin \theta}{R = AC} = \frac{\sin(\pi - \theta_1)}{R + s = OC} = \frac{\sin \rho}{OA} \implies \sin \theta_1 = \frac{R + s}{R} \sin \theta,$$

$$n_1 \sin \theta_1 = n_2 \sin \theta_2 \implies \sin \theta_2 = \frac{n_1 \sin \theta_1}{n_2} = \frac{n_1}{n_2} \frac{R + s}{R} \sin \theta,$$

$$OAC \implies \rho = \pi - \theta - (\pi - \theta_1) = \theta_1 - \theta,$$

$$ACI \implies \phi = \rho - \theta_2 = \theta_1 - \theta_2 - \theta.$$

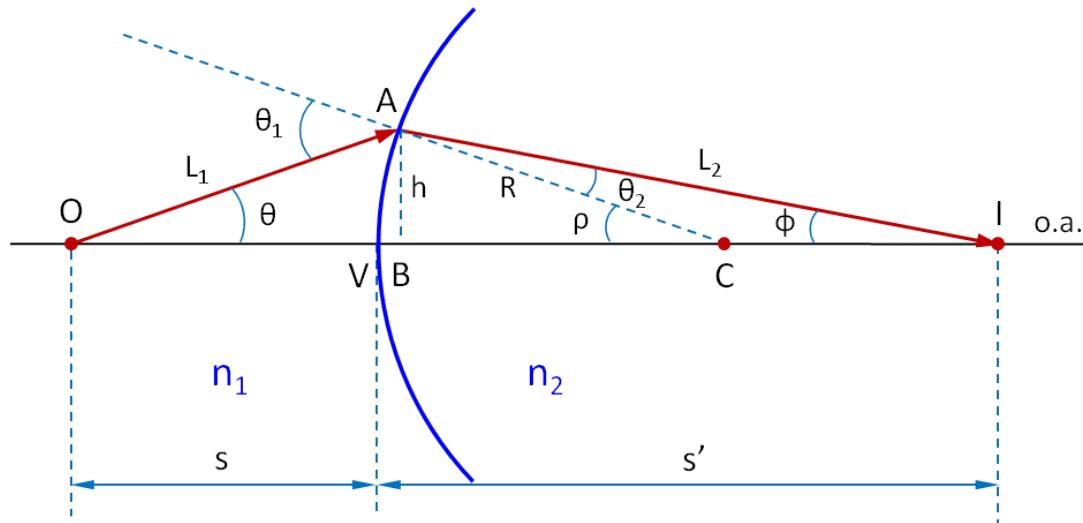
Triangle OAI:

$$\frac{\sin(\pi - \theta_1 + \theta_2)}{OI = s + s'} = \frac{\sin \phi}{OA} = \frac{\sin \theta}{AI},$$

$$OA = R \frac{\sin \rho}{\sin \theta} = R \frac{\sin(\theta_1 - \theta)}{\sin \theta}.$$

$$s' = R \frac{\sin(\theta_1 - \theta)}{\sin \theta} \frac{\sin(\theta_1 - \theta_2)}{\sin \phi} - s$$

Spherical Aberration (3rd order – Seidel)



3rd order – Seidel

$$\sin x \simeq x - \frac{x^3}{3!} + \frac{x^5}{5!}$$

$$\cos x \simeq 1 - \frac{x^2}{2!} + \frac{x^4}{4!}$$

$$(1+x)^{1/2} \simeq 1 + \frac{x}{2} - \frac{x^2}{8}$$

$$\alpha(A) = (n_1 L_1 + n_2 L_2) - (n_1 s + n_2 s') \quad \text{where}$$

$$L_1 = [R^2 + (R+s)^2 - 2R(R+s)\cos\rho]^{1/2}, \quad \text{from OAC}$$

$$L_2 = [R^2 + (s'-R)^2 + 2R(s'-R)\cos\rho]^{1/2}, \quad \text{from IAC}$$

$$\cos\rho = (1 - \sin^2\rho)^{1/2} = \left(1 - \frac{h^2}{R^2}\right)^{1/2} \Rightarrow$$

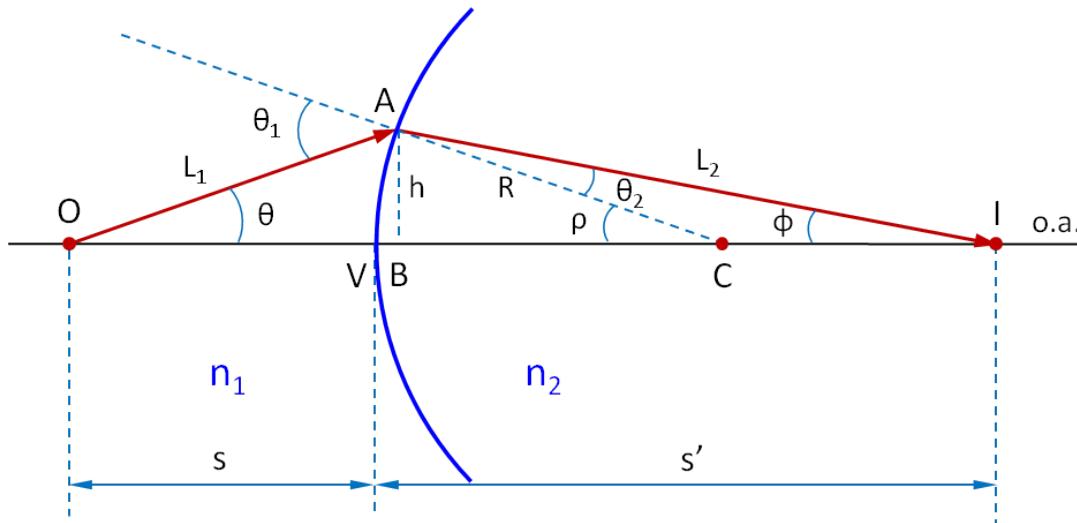
$$\cos\rho \simeq 1 - \frac{h^2}{2R^2} - \frac{h^4}{8R^4} \quad \text{resulting in}$$

$$L_1 \simeq s \left[1 + \frac{h^2(R+s)}{Rs^2} + \frac{h^4(R+s)}{4R^3s^2} \right]^{1/2}$$

$$L_2 \simeq s' \left[1 + \frac{h^2(R-s')}{Rs'^2} + \frac{h^4(R-s')}{4R^3s'^2} \right]^{1/2}.$$

$$(1+x)^{1/2} \simeq 1 + (x/2) - (x^2/8)$$

Spherical Aberration (3rd order – Seidel)

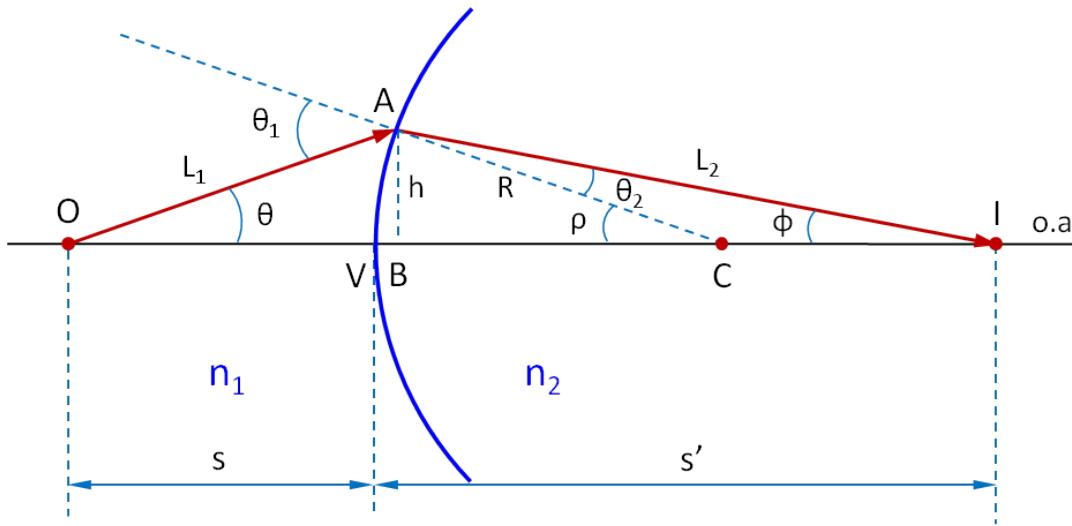


$$L_1 \simeq s \left[1 + \frac{h^2(R+s)}{2Rs^2} + \frac{h^4(R+s)}{8R^3s^2} - \frac{h^4(R+s)^2}{8R^2s^4} \right],$$

$$L_2 \simeq s' \left[1 + \frac{h^2(R-s')}{2Rs'^2} + \frac{h^4(R-s')}{8R^3s'^2} - \frac{h^4(R-s')^2}{8R^2s'^4} \right], \quad \text{resulting in}$$

$$\begin{aligned} \alpha(A) \simeq & \frac{h^2}{2} \left[\frac{n_1}{s} + \frac{n_2}{s'} - \frac{n_2 - n_1}{R} \right] \\ & - \frac{h^4}{8} \left[\frac{n_1}{s} \left(\frac{1}{s} + \frac{1}{R} \right)^2 + \frac{n_2}{s'} \left(\frac{1}{s'} - \frac{1}{R} \right)^2 - \frac{1}{R^2} \left(\frac{n_1}{s} + \frac{n_2}{s'} - \frac{n_2 - n_1}{R} \right) \right]. \end{aligned}$$

Spherical Aberration (3rd order – Seidel)



$$OPL = n_1 L_1 + n_2 L_2 \quad \text{with}$$

$$L_1 \simeq s \left[1 + \frac{h^2(R+s)}{2Rs^2} + \frac{h^4(R+s)}{8R^3s^2} - \frac{h^4(R+s)^2}{8R^2s^4} \right],$$

$$L_2 \simeq s' \left[1 + \frac{h^2(R-s')}{2Rs'^2} + \frac{h^4(R-s')}{8R^3s'^2} - \frac{h^4(R-s')^2}{8R^2s'^4} \right],$$

$$\frac{d(OPL)}{dh} = 0 \Rightarrow$$

$$n_1 \frac{R+s}{Rs} + n_1 \frac{h^2}{2} \frac{R+s}{R^3s} - n_1 \frac{h^2}{2} \frac{(R+s)^2}{R^2s^3} \\ + n_2 \frac{R-s'}{Rs'} + n_2 \frac{h^2}{2} \frac{R-s'}{R^3s'} - n_2 \frac{h^2}{2} \frac{(R-s')^2}{R^2s'^3} = 0 \Rightarrow$$

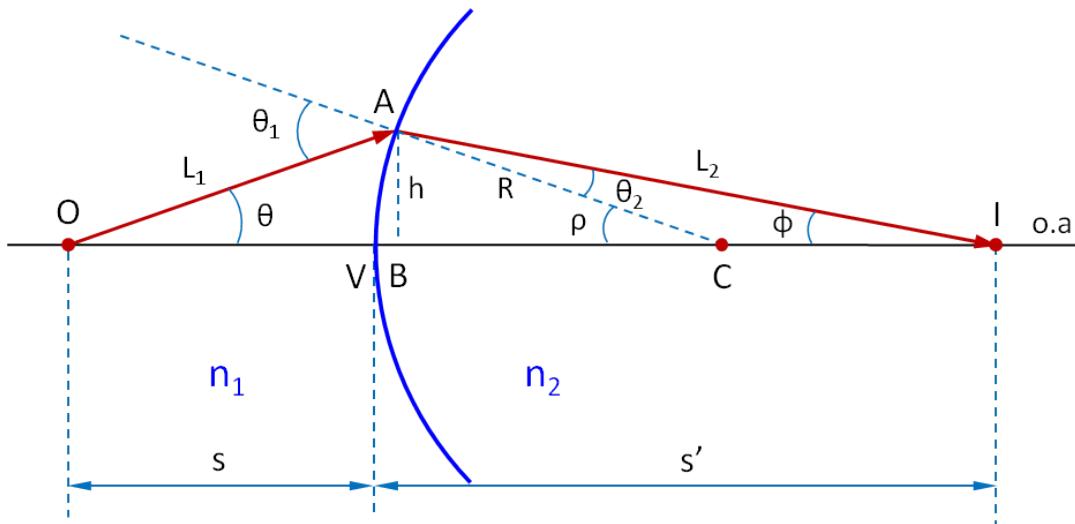
$$X \left(1 + \frac{h^2}{2R^2} \right) = \frac{h^2}{2} \left[\frac{n_1}{s} \left(\frac{1}{s} + \frac{1}{R} \right)^2 + \frac{n_2}{s'} \left(\frac{1}{s'} - \frac{1}{R} \right)^2 \right] \quad \text{where}$$

$$X = \frac{n_1}{s} + \frac{n_2}{s'} - \frac{(n_2 - n_1)}{R}.$$

$$X = \frac{h^2}{2} \left[\frac{n_1}{s} \left(\frac{1}{s} + \frac{1}{R} \right)^2 + \frac{n_2}{s'} \left(\frac{1}{s'} - \frac{1}{R} \right)^2 \right],$$

$$\frac{n_2}{f_p} = \frac{n_2 - n_1}{R},$$

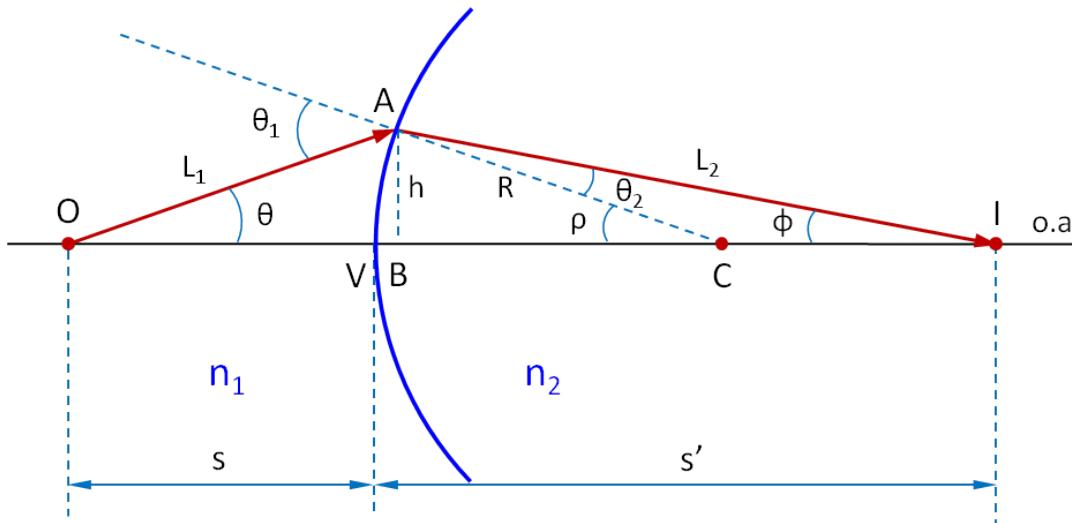
Spherical Aberration (3rd order – Seidel)



3-order Approximation:

$$\frac{n_1}{s} + \frac{n_2}{s'} = \frac{n_2 - n_1}{R} + \frac{h^2}{2} \left[\frac{R}{f_p} \frac{n_1^2}{n_2} \left(\frac{1}{R} + \frac{1}{s} \right)^2 \left(\frac{1}{R} + \frac{n_1 + n_2}{n_1} \frac{1}{s} \right) \right]$$

Spherical Aberration (3rd order – Seidel)



3-order Approximation (without any more approximations-exact):

$$\left(\frac{n_1}{s} + \frac{n_2}{s'} - \frac{n_2 - n_1}{R} \right) \left(1 + \frac{h^2}{2R^2} \right) = \frac{h^2}{2} \left[\frac{n_1}{s} \left(\frac{1}{s} + \frac{1}{R} \right)^2 + \frac{n_2}{s'} \left(\frac{1}{s'} - \frac{1}{R} \right)^2 \right]$$

$$a_0\psi^3 + a_1\psi^2 + a_2\psi + a_3 = 0, \quad \text{where}$$

$$\psi = \frac{1}{s'},$$

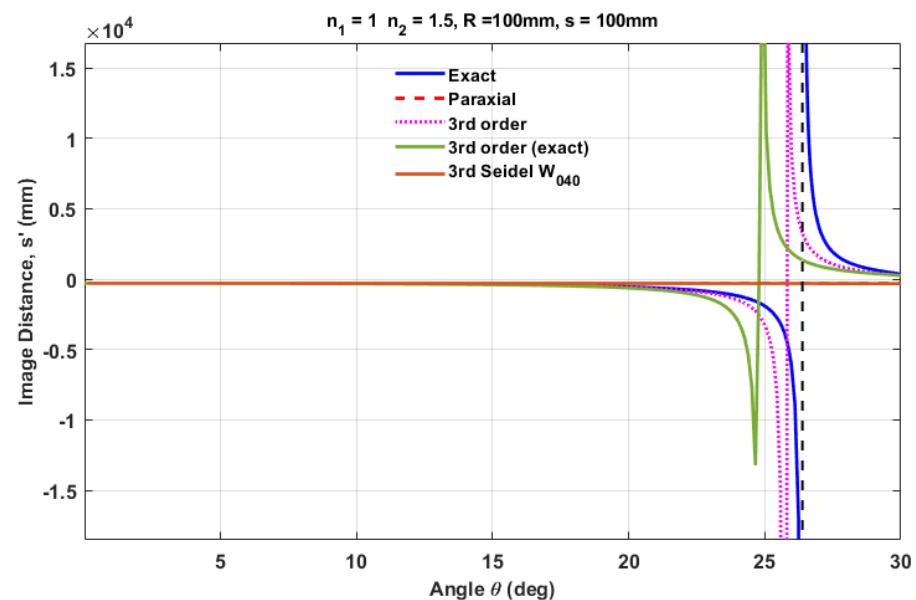
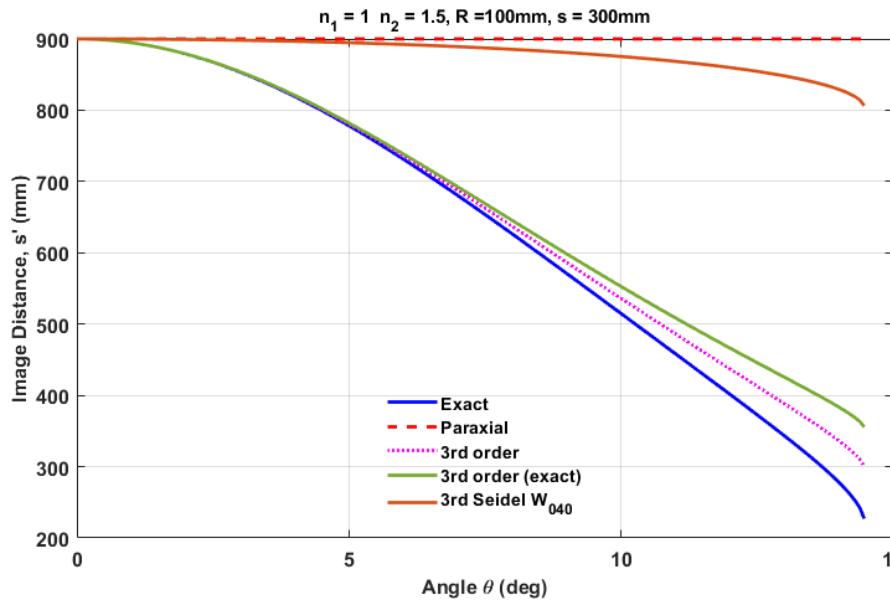
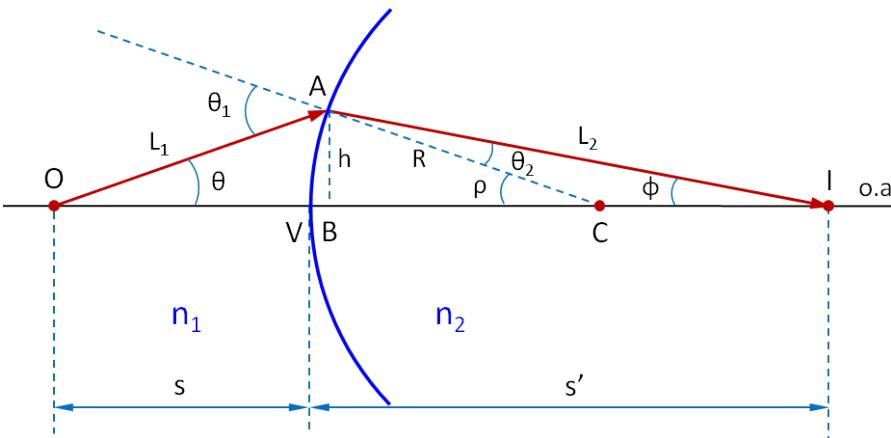
$$a_0 = \frac{h^2}{2}n_2,$$

$$a_1 = -\frac{h^2n_2}{R},$$

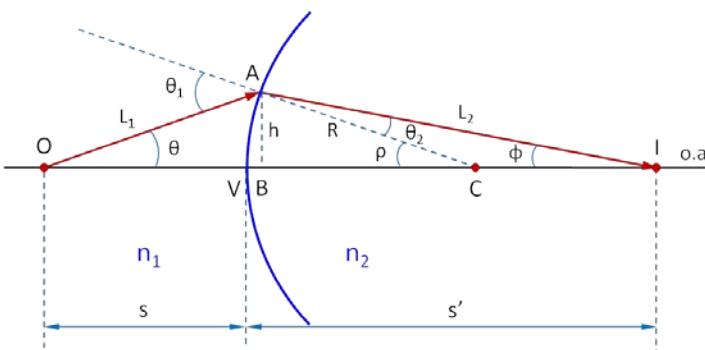
$$a_2 = \frac{h^2n_2}{2R^2} - \left(1 + \frac{h^2}{2R^2} \right) n_2,$$

$$a_3 = \frac{h^2}{2} \frac{n_1}{s} \left(\frac{1}{s} + \frac{1}{R} \right)^2 - \left(1 + \frac{h^2}{2R^2} \right) \left(\frac{n_1}{s} - \frac{n_2 - n_1}{R} \right).$$

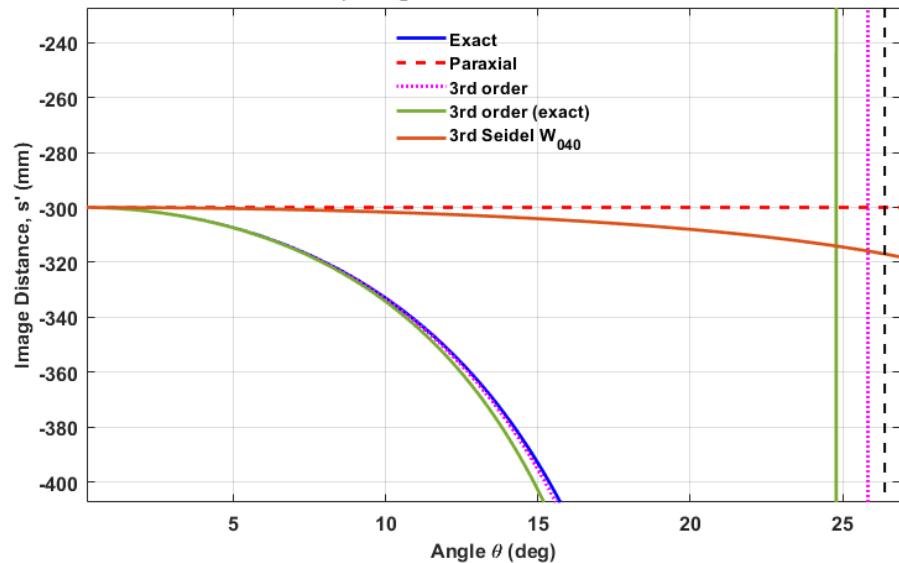
Spherical Aberration - Example



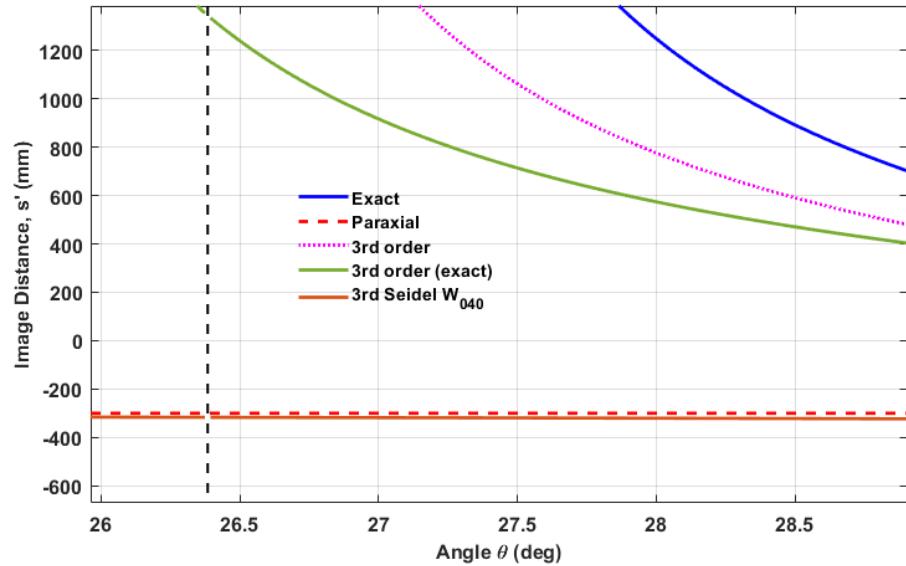
Spherical Aberration - Example



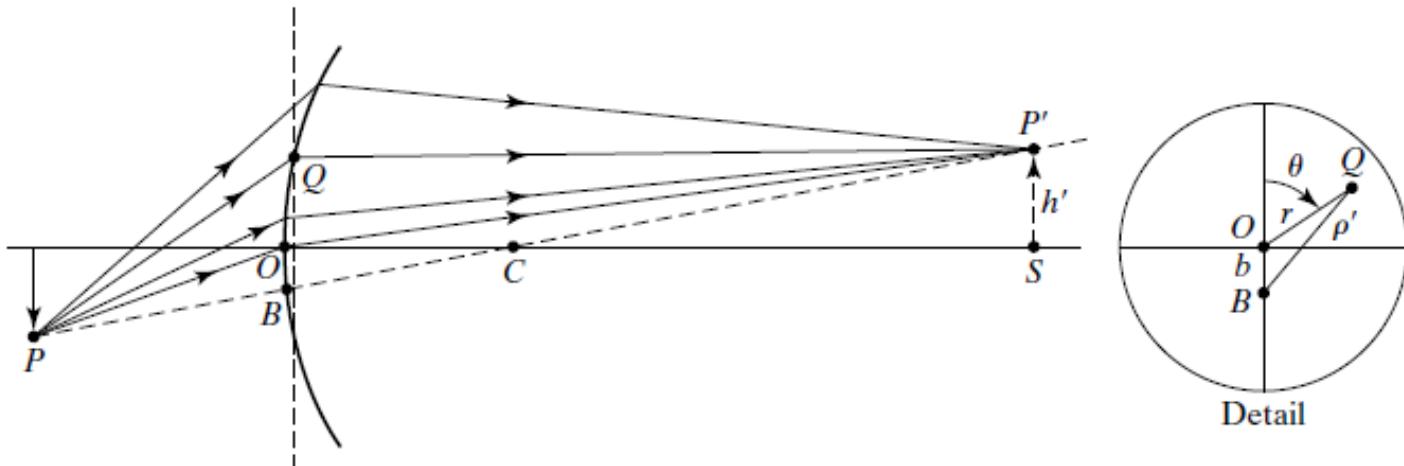
$n_1 = 1$ $n_2 = 1.5$, $R = 100\text{mm}$, $s = 100\text{mm}$



$n_1 = 1$ $n_2 = 1.5$, $R = 100\text{mm}$, $s = 100\text{mm}$



Aberrations (3rd order – Seidel)



$$a(Q) = {}_0C_{40}r^4 + {}_1C_{31}h'r^3 \cos \theta + {}_2C_{22}h'^2r^2 \cos^2 \theta + {}_2C_{20}h'^2r^2 + {}_3C_{11}h'^3r \cos \theta$$

r^4 : Spherical Aberration

$h'r^3 \cos \theta$: Coma

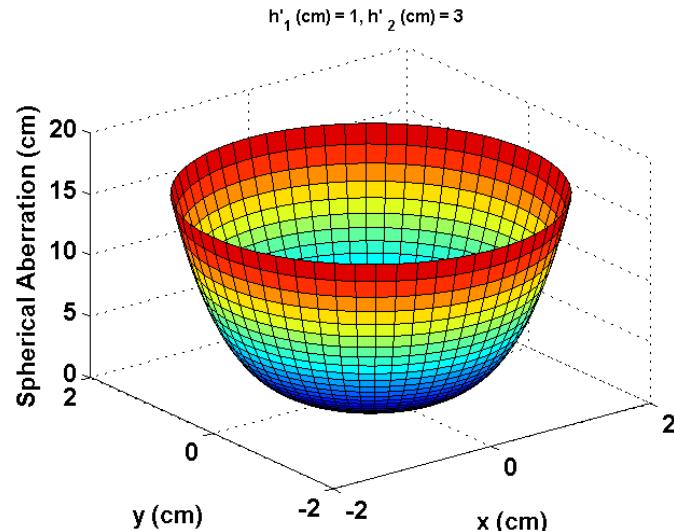
$h'^2r^2 \cos^2 \theta$: Astigmatism

h'^2r^2 : Field Curvature

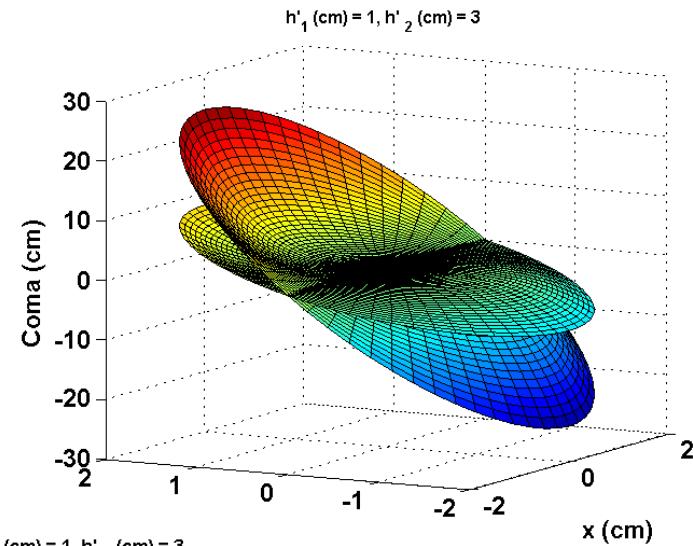
$h'^3r \cos \theta$: Distortion

Aberrations (3rd order – Seidel)

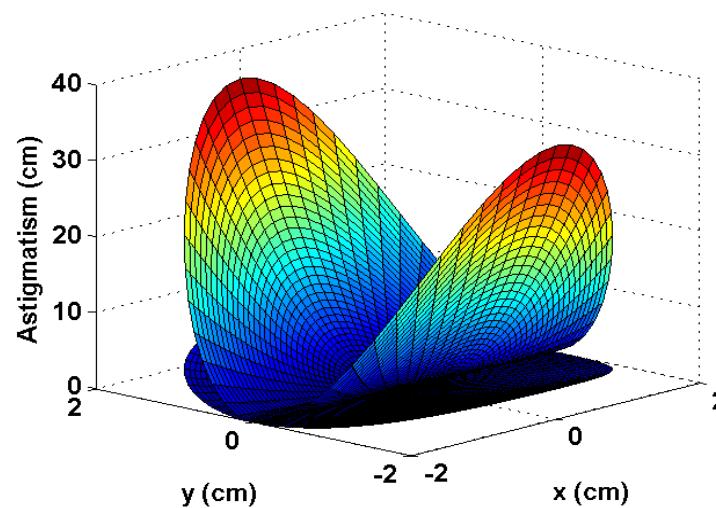
r^4 : Spherical Aberration



$h'r^3 \cos \theta$: Coma

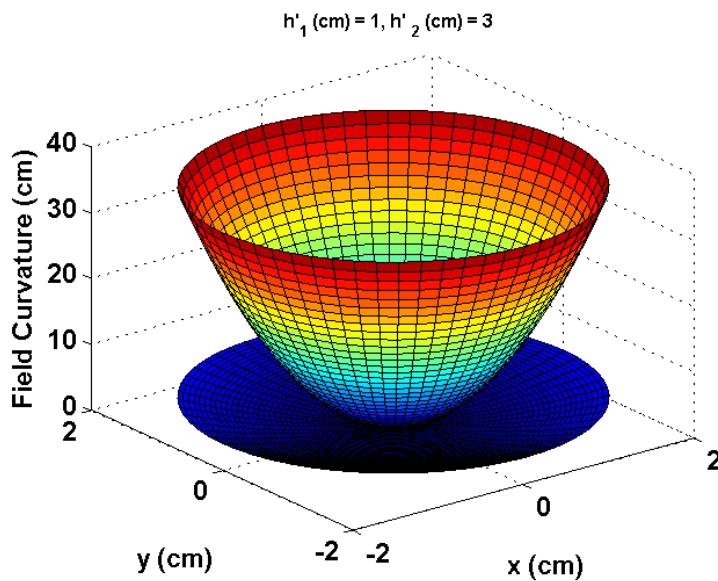


$h'^2 r^2 \cos^2 \theta$: Astigmatism

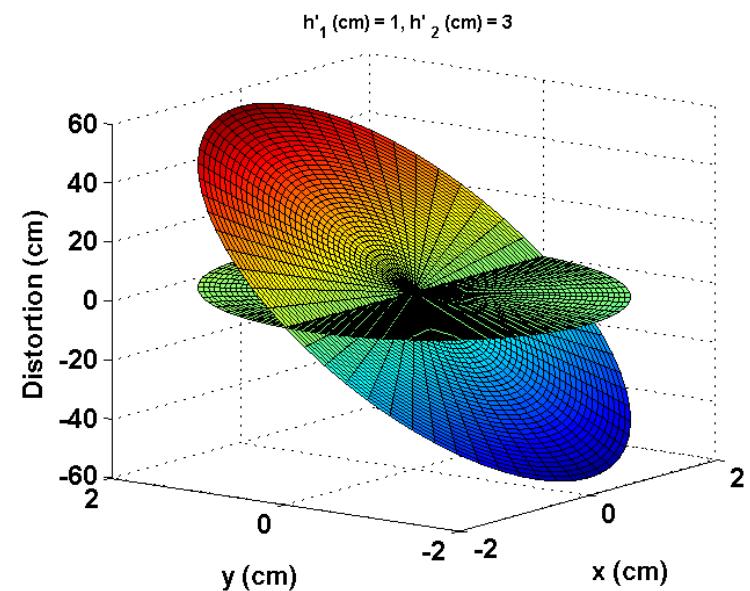


Aberrations (3rd order – Seidel)

$h'^2 r^2$: Field Curvature



$h'^3 r \cos \theta$: Distortion



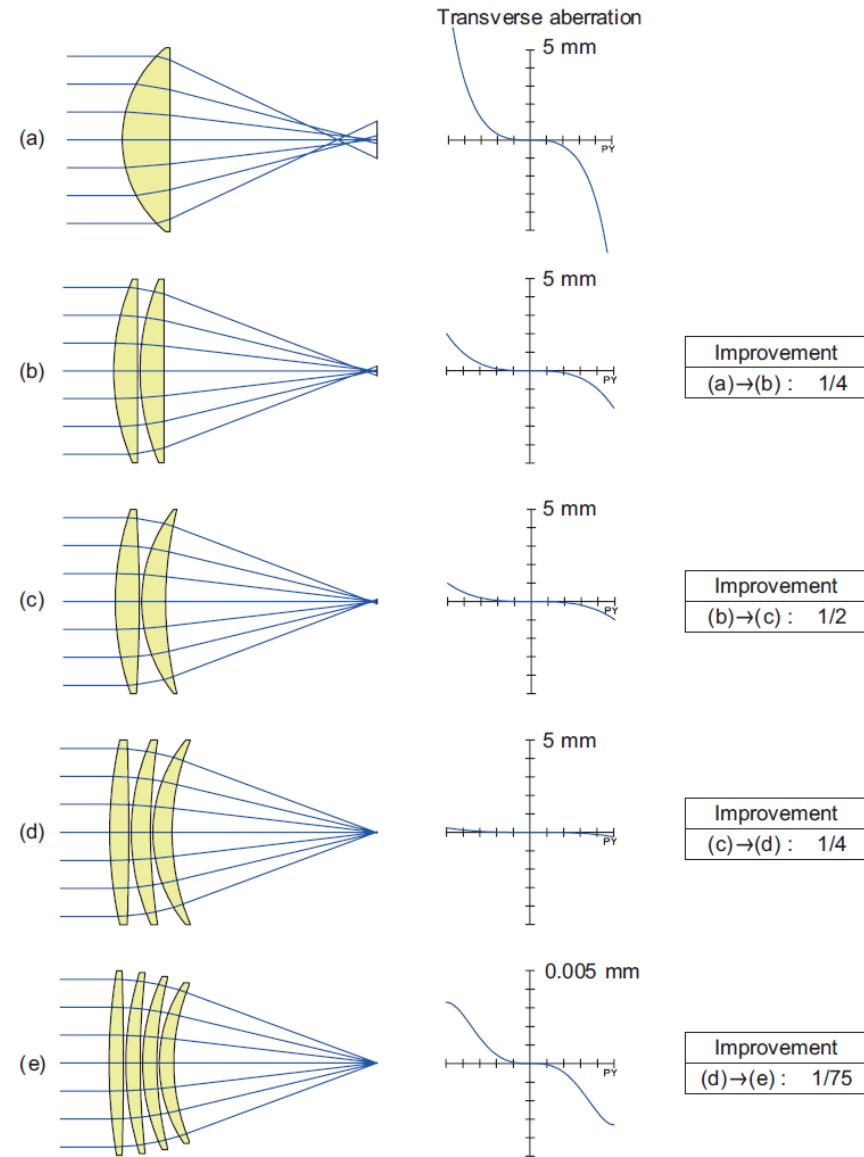
Lens Aberrations and Common Corrections

Aberration	Character	Correction
1. <u>Spherical aberration</u>	Monochromatic, on- and off-axis, image blur	Bending, high index, aspherics, gradient index, doublet
2. <u>Coma</u>	Monochromatic, off-axis only, blur	Bending, spaced doublet with central stop
3. <u>Oblique astigmatism</u>	Monochromatic, off-axis blur	Spaced doublet with stop
4. <u>Curvature of field</u>	Monochromatic, off-axis	Spaced doublet
5. <u>Distortion</u>	Monochromatic, off-axis	Spaced doublet with stop
6. <u>Chromatic aberration</u>	Heterochromatic, on- and off-axis, blur	Contact doublet, spaced doublet

<http://hyperphysics.phy-astr.gsu.edu/hbase/geoopt/aberrcon.html>

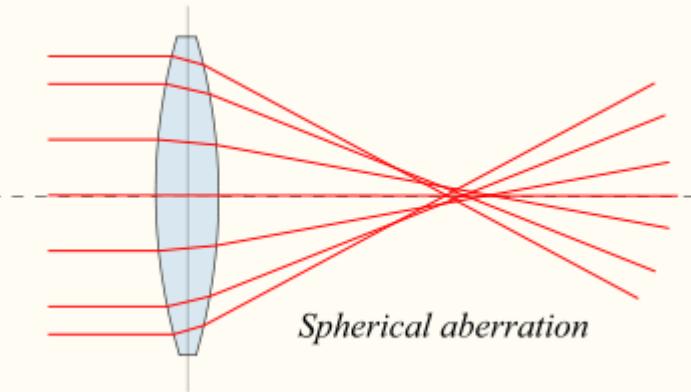
Lens Aberrations and Corrections Approaches

- Lens Bending
- Power Splitting
- Power Combination
- Distances
- Refractive Index
- Dispersion
- Gradient Index Materials
- Cemented Surfaces
- Aspherical Surfaces
- Diffractive Surfaces

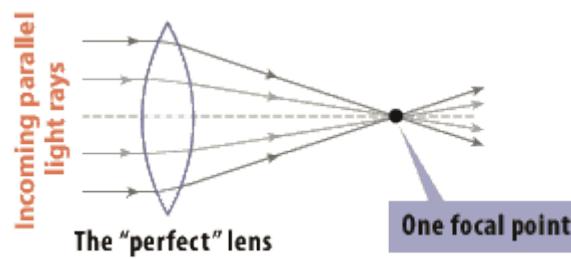
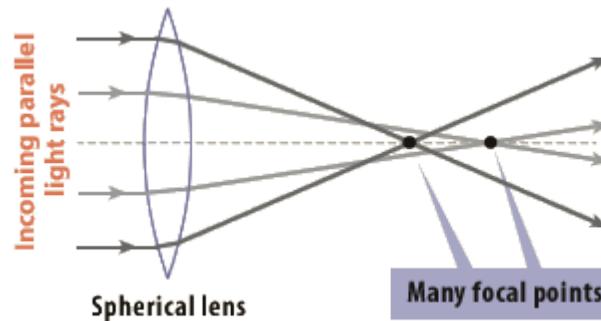


Example: Splitting and bending. In the examples shown $f' = 100 \text{ mm}$, the aperture is $f/1.4$, the refractive index $n = 1.5$. Note the change in the scale for the transverse aberration diagram in case (e) with four elements. The transverse aberration is shown with respect to the Gaussian image plane.

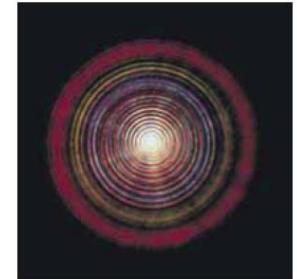
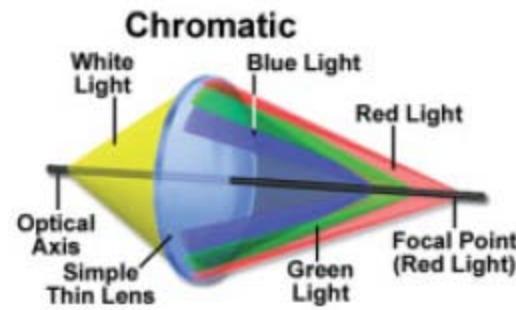
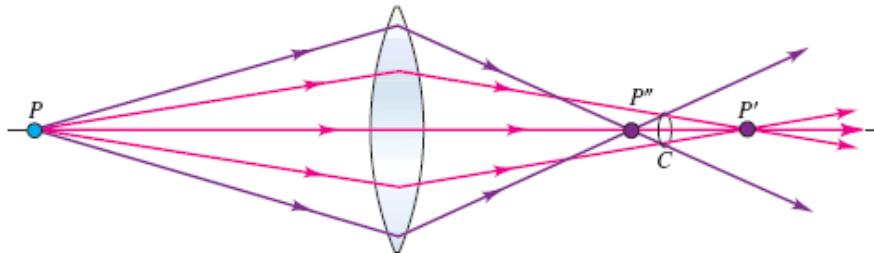
Spherical Aberration



[http://en.wikipedia.org/wiki/Lens_\(optics\)](http://en.wikipedia.org/wiki/Lens_(optics))



<http://amazing-space.stsci.edu/resources/explorations/groundup/lesson/basic/g11/>



Spherical Aberration Example



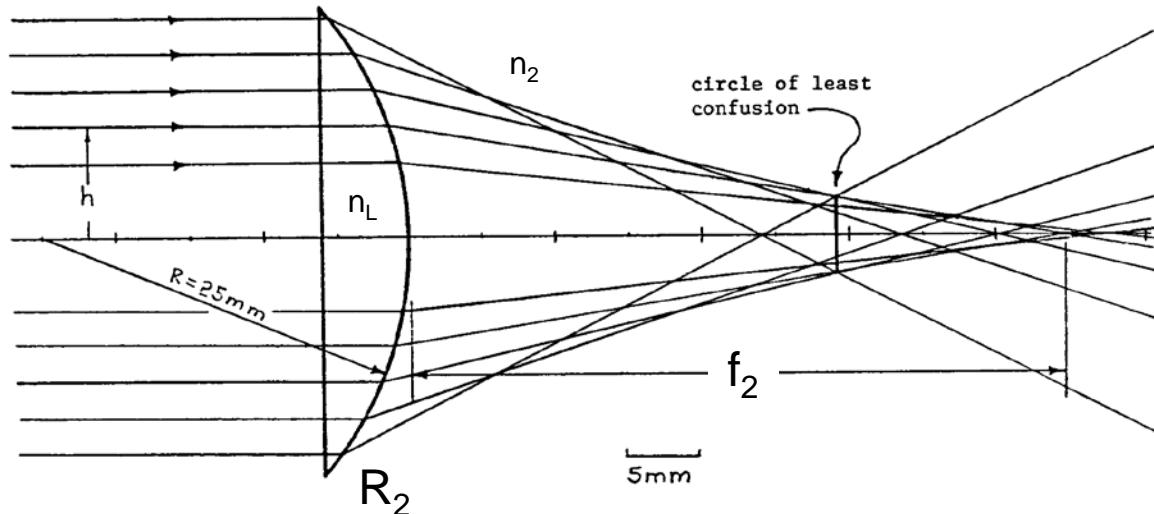
<https://www.wehelpchicagosee.com/blog/2015/01/28/high-definition-hd-vision-154460>

Plano-Convex Lens

A plano-convex lens has a radius of curvature of R and an index of refraction, n .

A collimated beam of light is incident upon the plano side of this lens in air as shown in the figure. Accounting for the plano-convex shape of the lens, the focal distance as defined in the figure, for an axial ray of displacement h from the principal axis is

$$f_2 = \frac{h}{\tan \left[\sin^{-1} \left(\frac{n_L}{n_2} \frac{h}{R_2} \right) - \sin^{-1} \left(\frac{h}{R_2} \right) \right]} - R_2 + \sqrt{R_2^2 - h^2}.$$

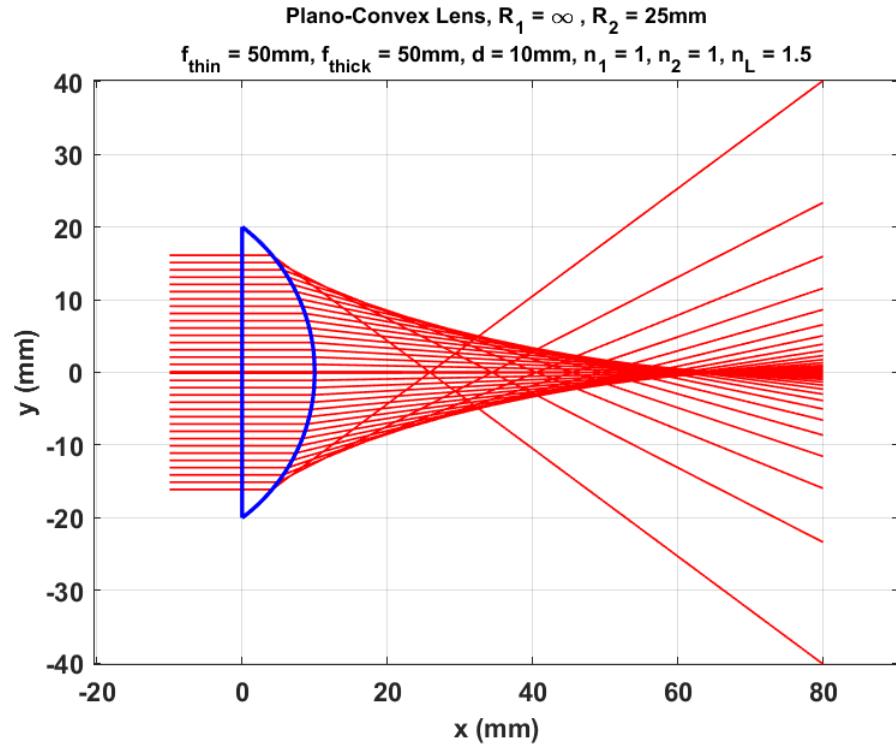
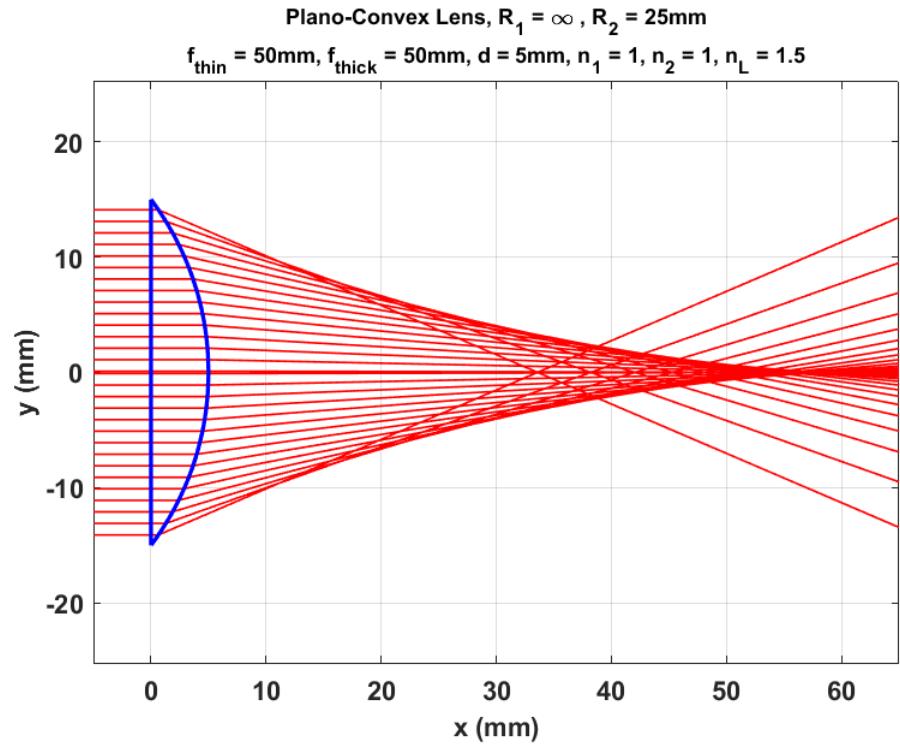


$h(\text{mm})$	$f(\text{mm})$
5.0	47.7
7.5	44.7
10.0	40.2
12.5	33.8
15.0	24.1

Fig. 1. Focusing of rays by plano-convex lens showing significant spherical aberration.

Notes from Prof. T. K. Gaylord in "Optical Engineering" Class (Georgia Tech)

Plano-Convex Lens



Convex-Plano Lens

A convex-plano lens has a radius of curvature of R , a thickness d , and an index of refraction, n . A collimated beam of light is incident upon the convex side of this lens in air as shown in the figure. Accounting for the convex-plano shape of the lens, the focal distance as defined in the figure, for an axial ray of displacement h from the principal axis is

$$f_2 = \frac{h - \left(d - R_1 + \sqrt{R_1^2 - h^2} \right) \tan \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{n_1 h}{n_L R_1} \right) \right]}{\tan \left\{ \sin^{-1} \left[\frac{n_L}{n_2} \sin \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{n_1 h}{n_L R_1} \right) \right] \right] \right\}}$$

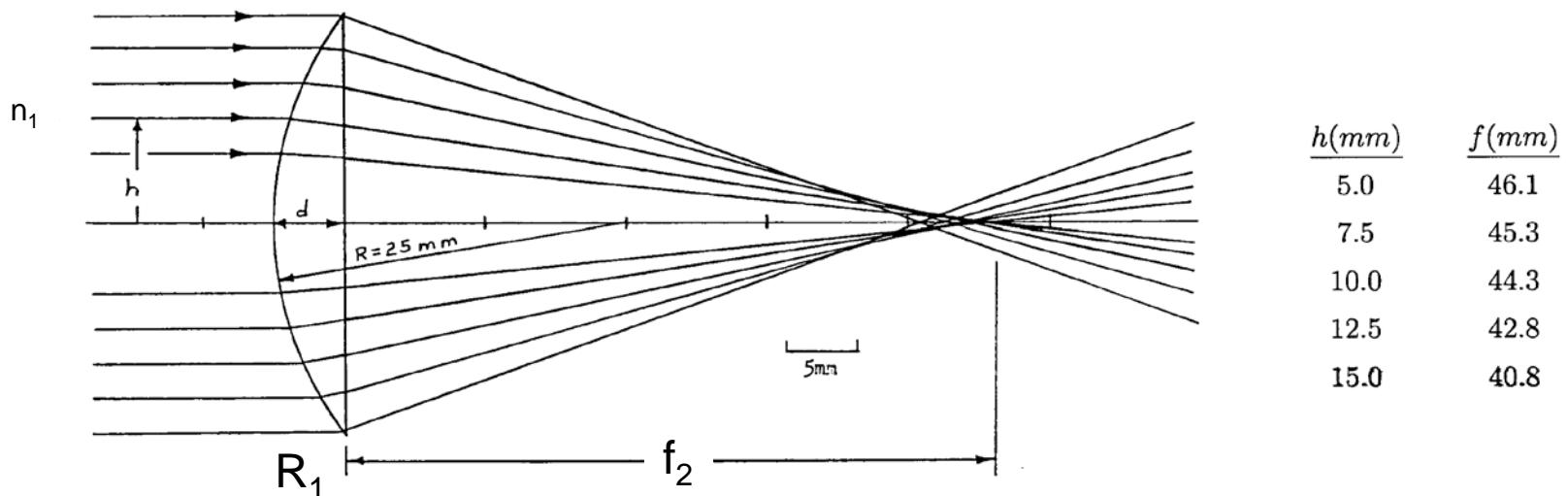
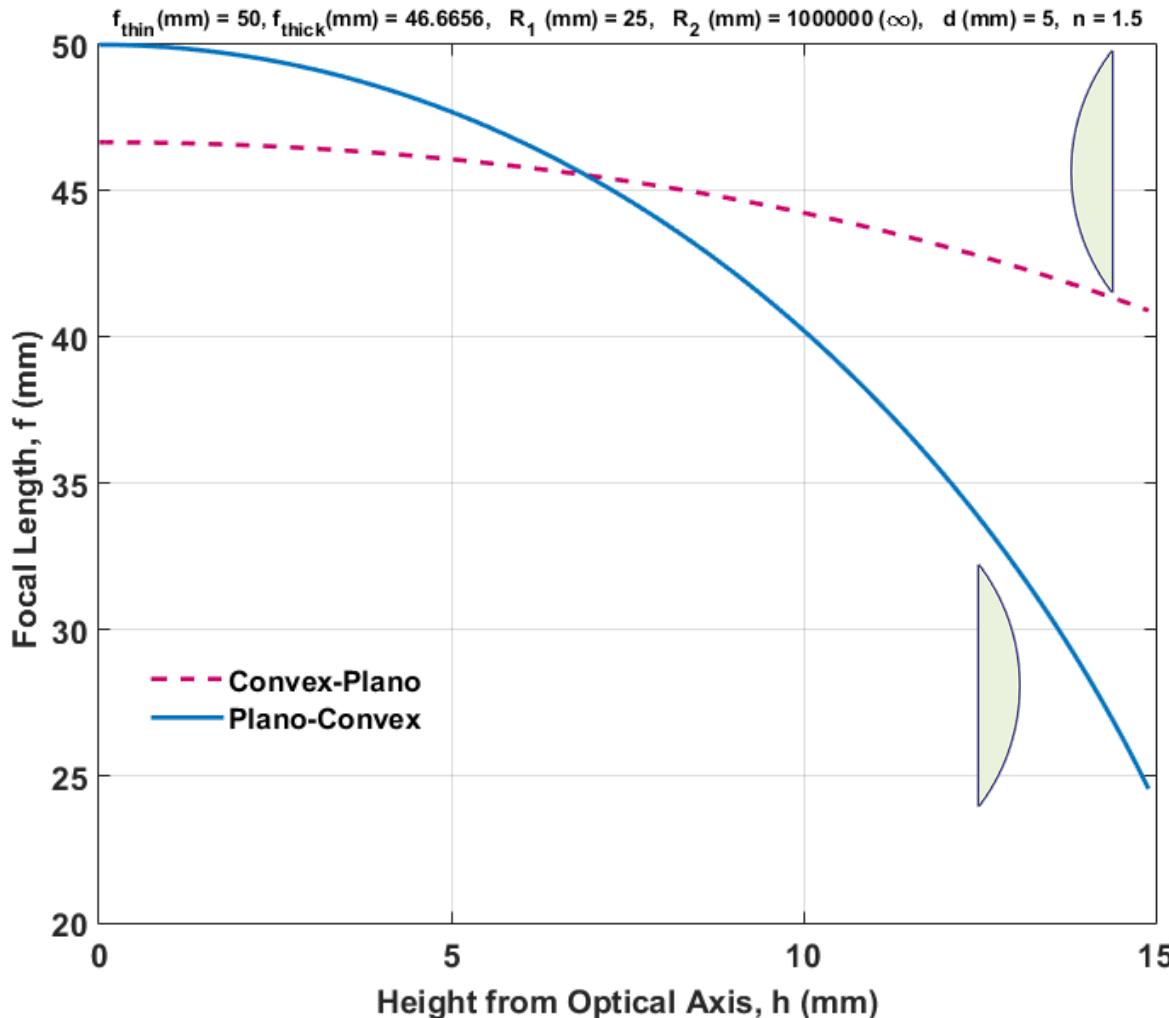


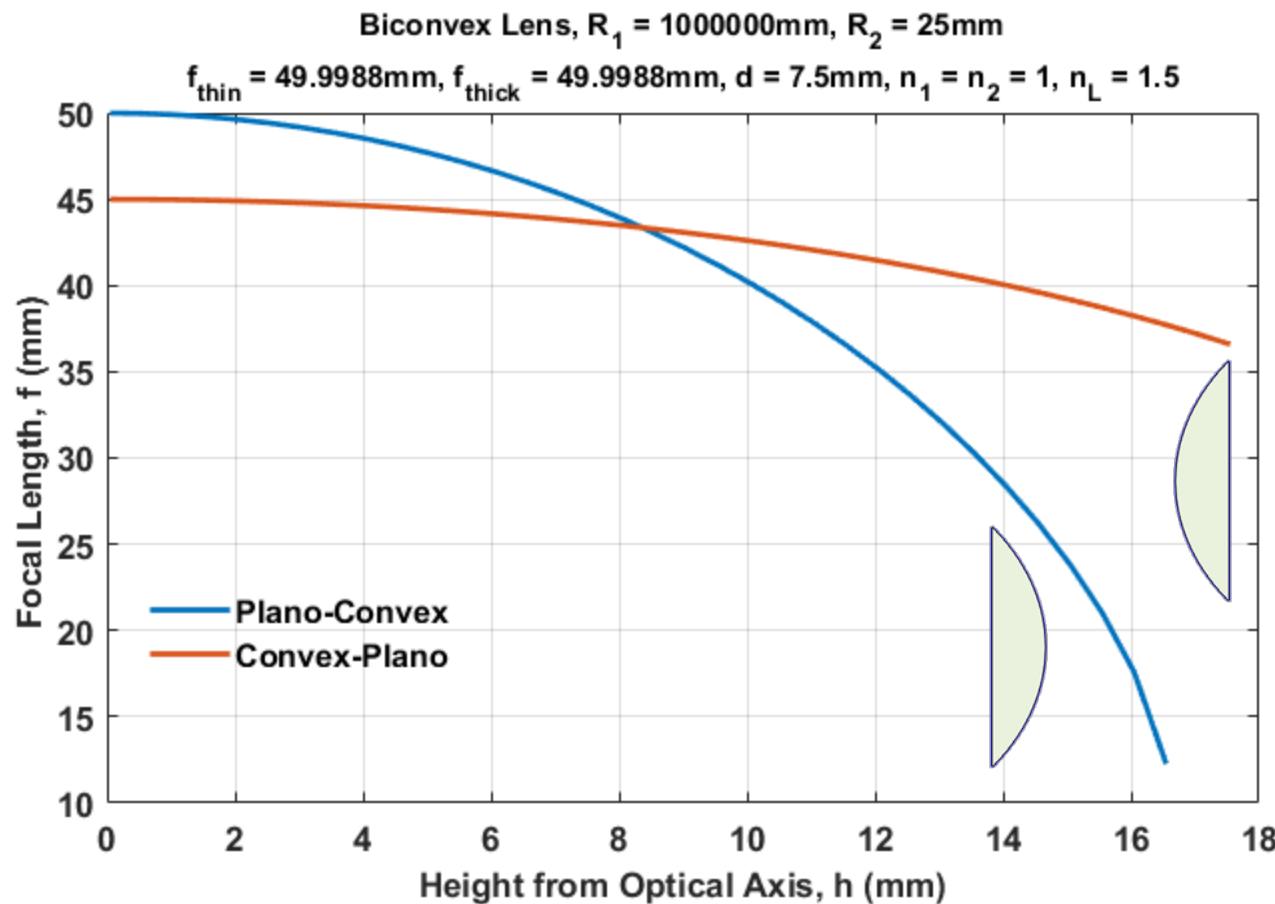
Fig. 1. Focusing of rays by convex-plano lens showing relatively small spherical aberration.

Notes from Prof. T. K. Gaylord in "Optical Engineering" Class (Georgia Tech)

Comparison of the Spherical Aberration of a Plano-Convex Lens and a Convex-Plano Lens



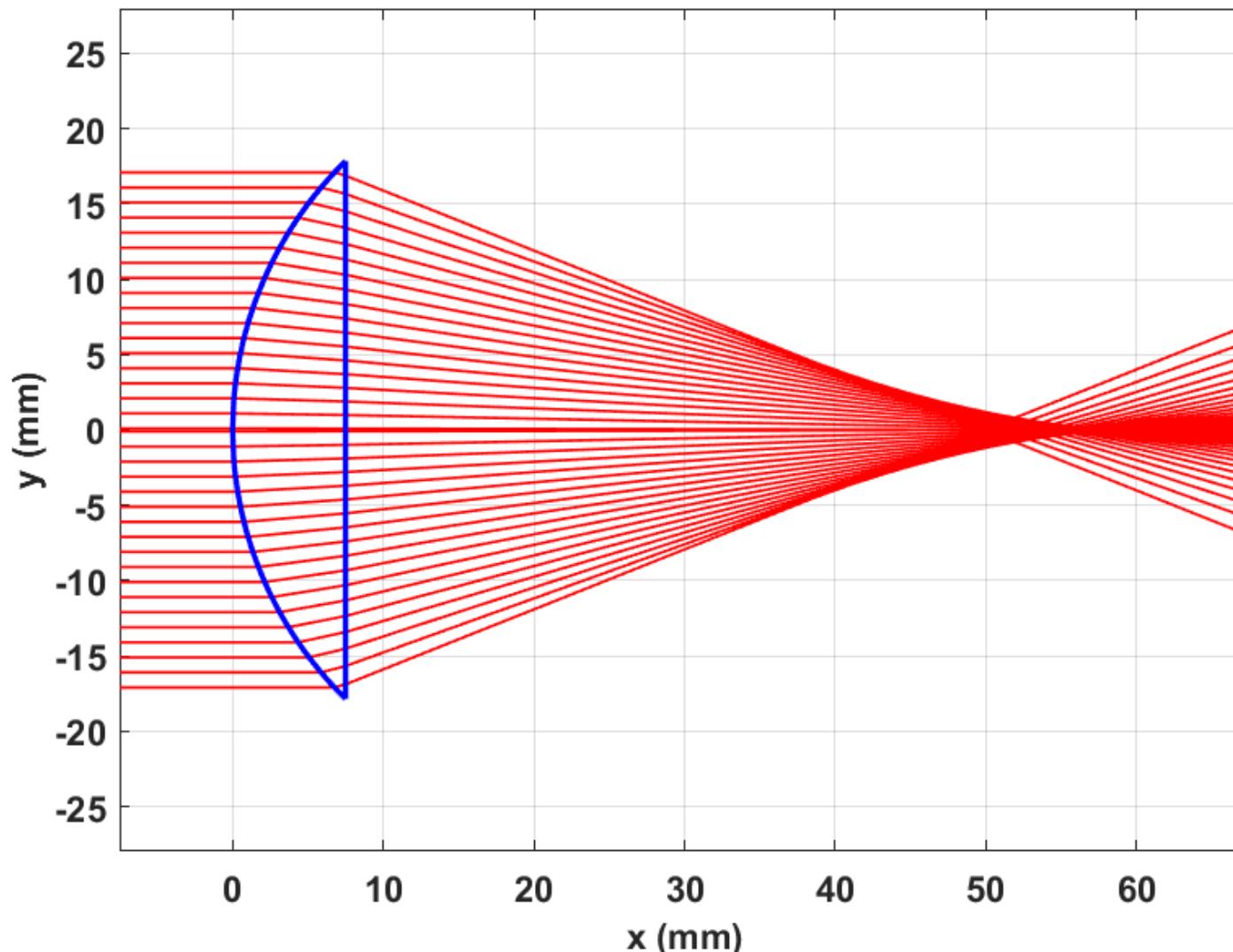
Convex-Plano Lens



Convex-Plano Lens

Biconvex Lens, $R_1 = 25\text{mm}$, $R_2 = 1000000\text{mm}$

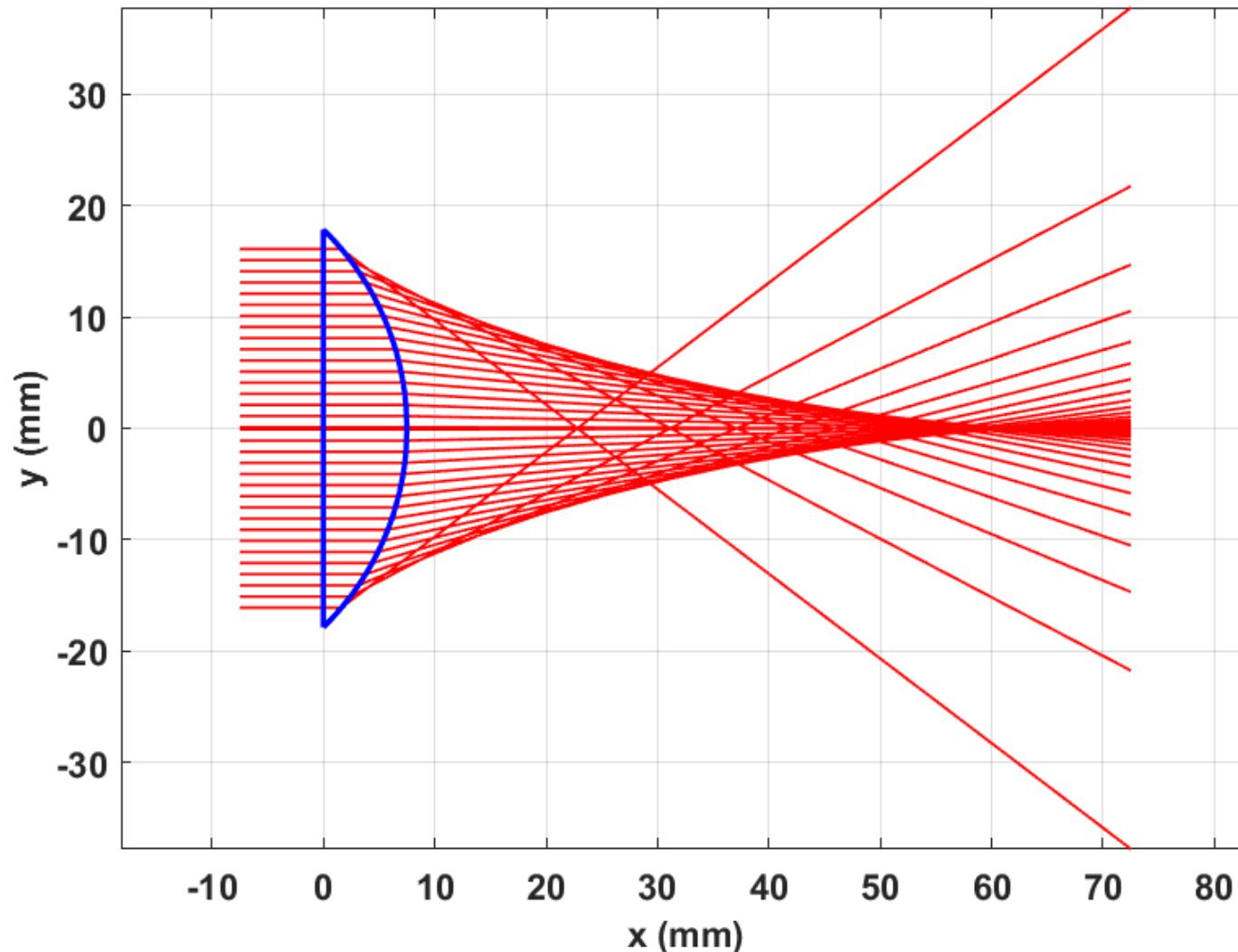
$f_{\text{thin}} = 49.9988\text{mm}$, $f_{\text{thick}} = 44.999\text{mm}$, $d = 7.5\text{mm}$, $n_1 = n_2 = 1$, $n_L = 1.5$



Convex-Plano Lens

Biconvex Lens, $R_1 = 1000000\text{mm}$, $R_2 = 25\text{mm}$

$f_{\text{thin}} = 49.9988\text{mm}$, $f_{\text{thick}} = 49.9988\text{mm}$, $d = 7.5\text{mm}$, $n_1 = n_2 = 1$, $n_L = 1.5$



Biconvex Lens

A biconvex lens has radii of curvature of R_1 and R_2 , a center thickness of d , and an index of refraction n . If R_1 and R_2 are taken to be magnitudes, the focal distance of this biconvex lens in air for an axial ray of distance h from the principal axis is

$$f = \left\{ n \left\{ (R_1 + R_2 - d) \sin \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{h}{nR_1} \right) \right] + \frac{h}{n} \right\} \middle/ \right.$$

$$\left. \sin \left[\left(\sin^{-1} \left\{ \left(\frac{n}{R_2} \right) (R_1 + R_2 - d) \sin \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{h}{nR_1} \right) \right] + \frac{h}{R_2} \right\} \right) \right. \right.$$

$$\left. \left. - \left(\sin^{-1} \left\{ \left(\frac{1}{R_2} \right) (R_1 + R_2 - d) \sin \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{h}{nR_1} \right) \right] + \frac{h}{nR_2} \right\} \right) \right]$$

$$\left. + \left[\sin^{-1} \left(\frac{h}{R_1} \right) - \sin^{-1} \left(\frac{h}{nR_1} \right) \right] \right\} - R_2$$

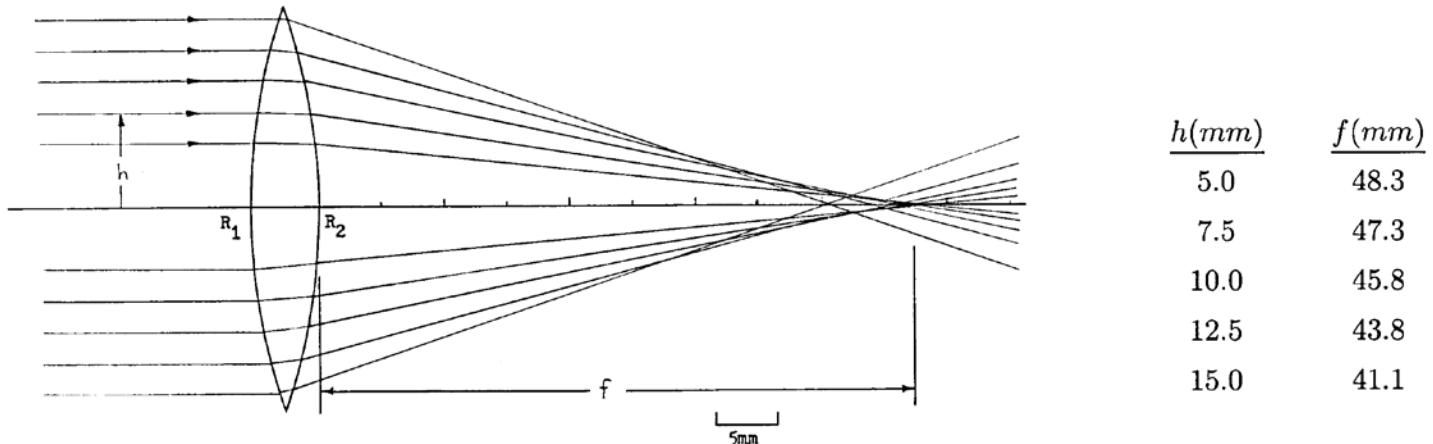
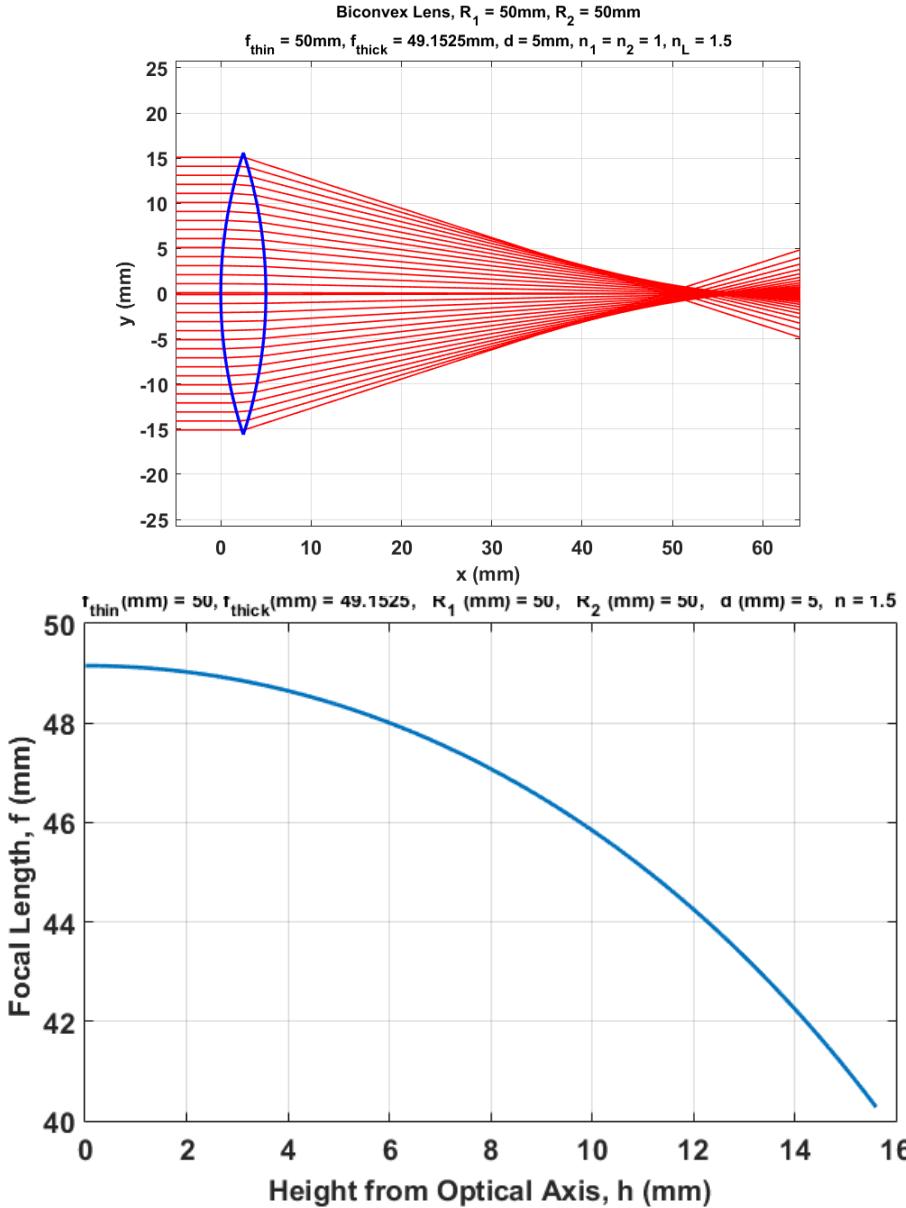


Fig. 1. Focusing of rays by biconvex lens showing spherical aberration.

Notes from Prof. T. K. Gaylord in "Optical Engineering" Class (Georgia Tech)

Prof. Elias N. Glytsis, School of ECE, NTUA

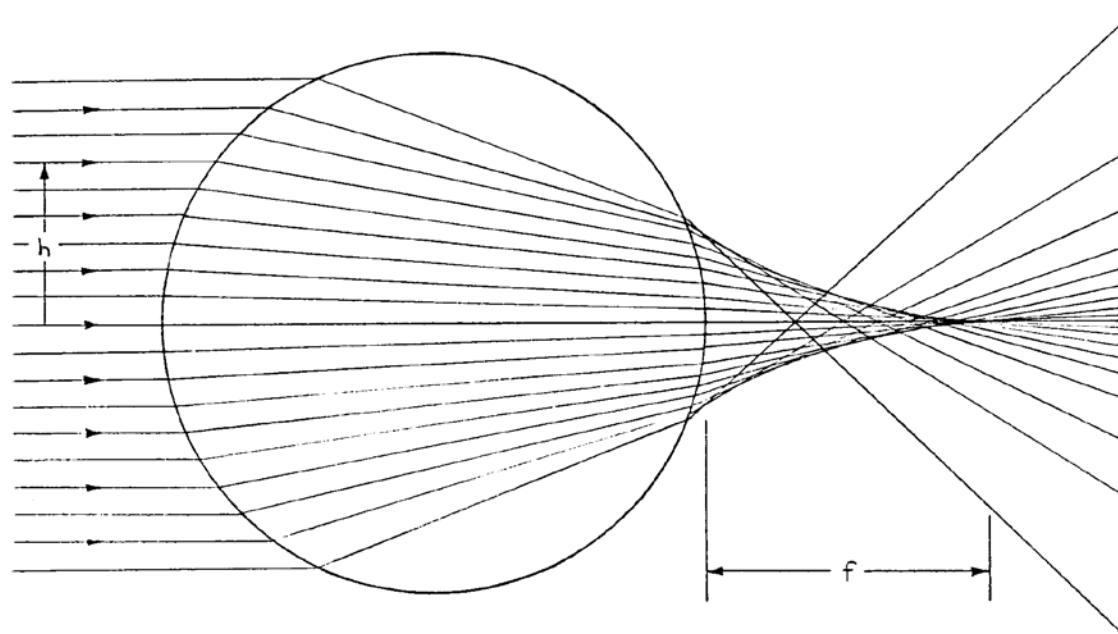
Spherical Aberration of a Biconvex Lens



Sphere Lens

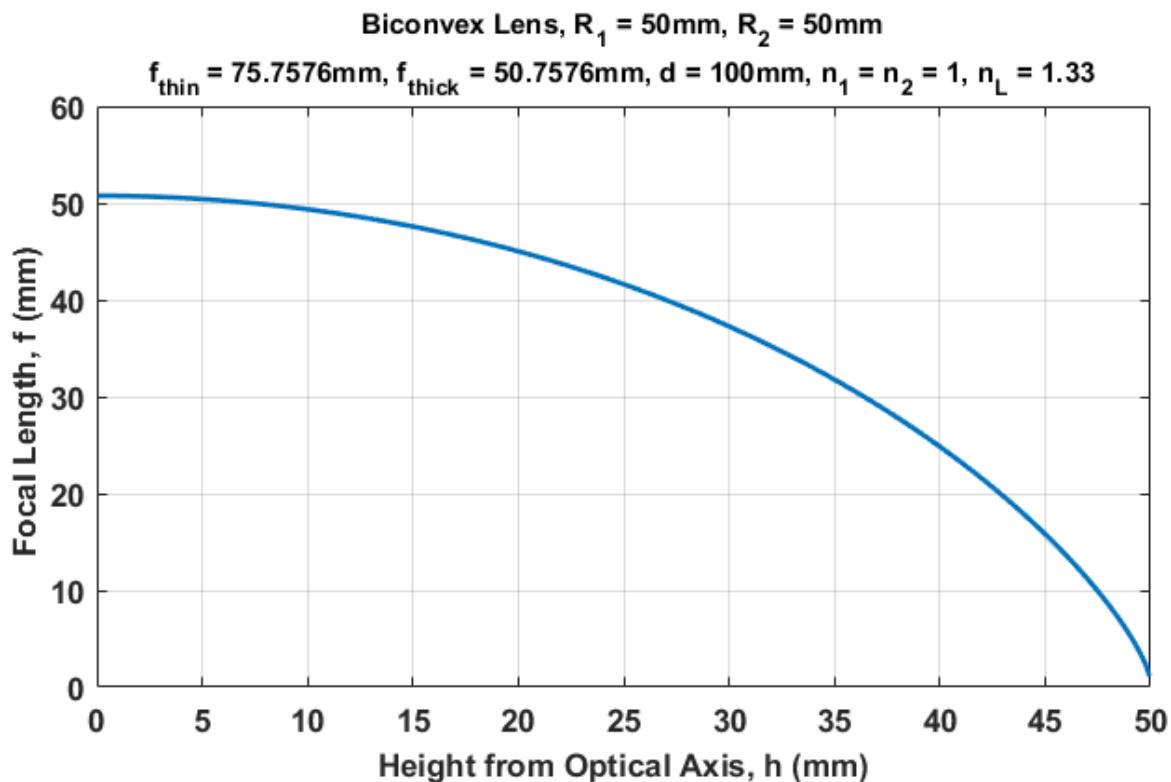
A sphere of radius R and an index of refraction n may be used as a lens. The focal distance of this lens in air for an axial ray of distance h from the principal axis is

$$f = R \left\{ \left[\left(\frac{h}{r} \right) \middle/ \sin \left\{ 2 \left[\sin^{-1} \left(\frac{h}{R} \right) - \sin^{-1} \left(\frac{h}{nR} \right) \right] \right\} \right] - 1 \right\}$$



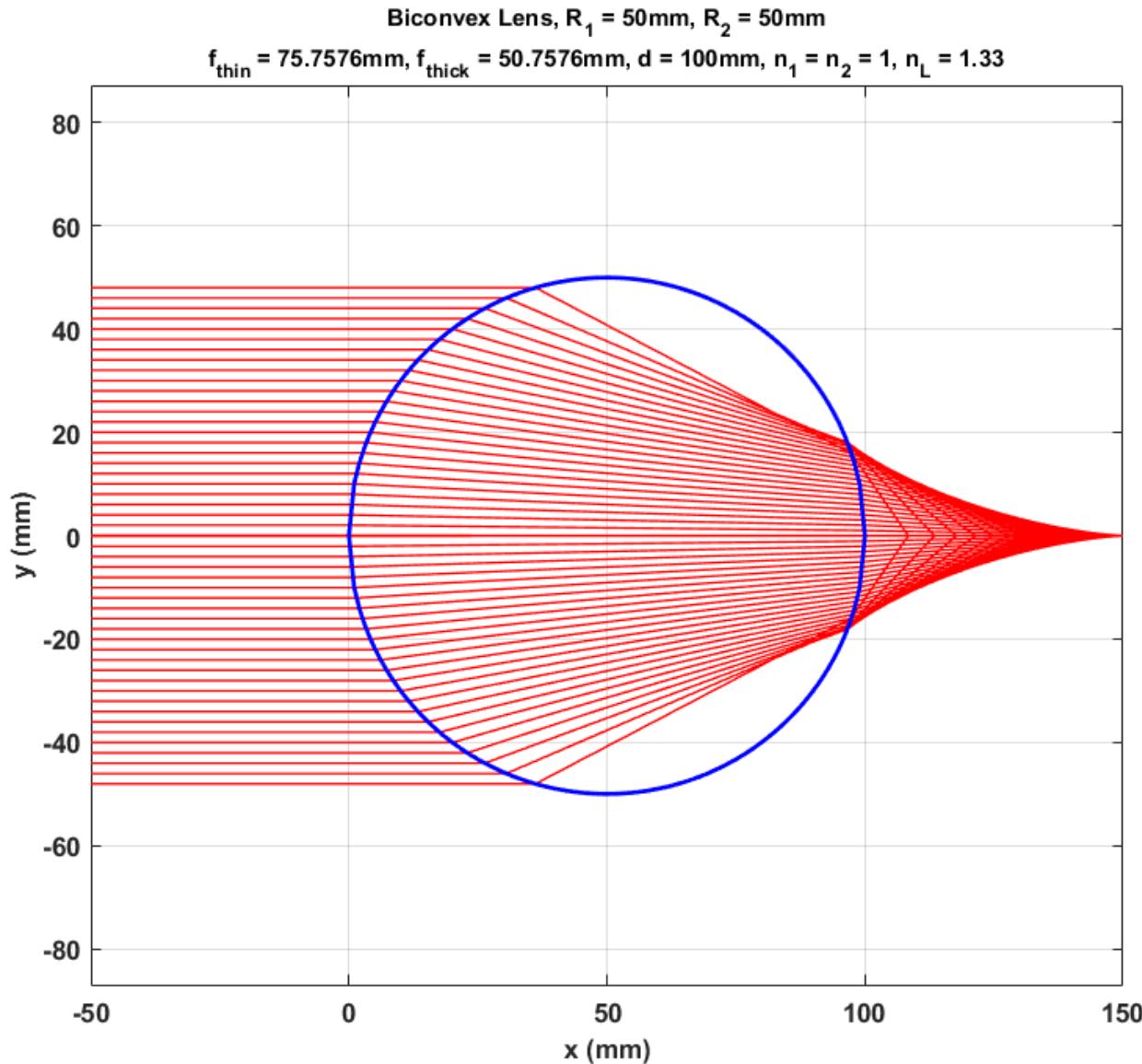
Notes from Prof. T. K. Gaylord in "Optical Engineering" Class (Georgia Tech)

Spherical Aberration of a Dielectric Sphere



h (mm)	f (mm)
5	50.4
10	49.4
15	47.6
20	45.0
25	41.6
30	37.3
35	31.8
40	24.8
45	15.8

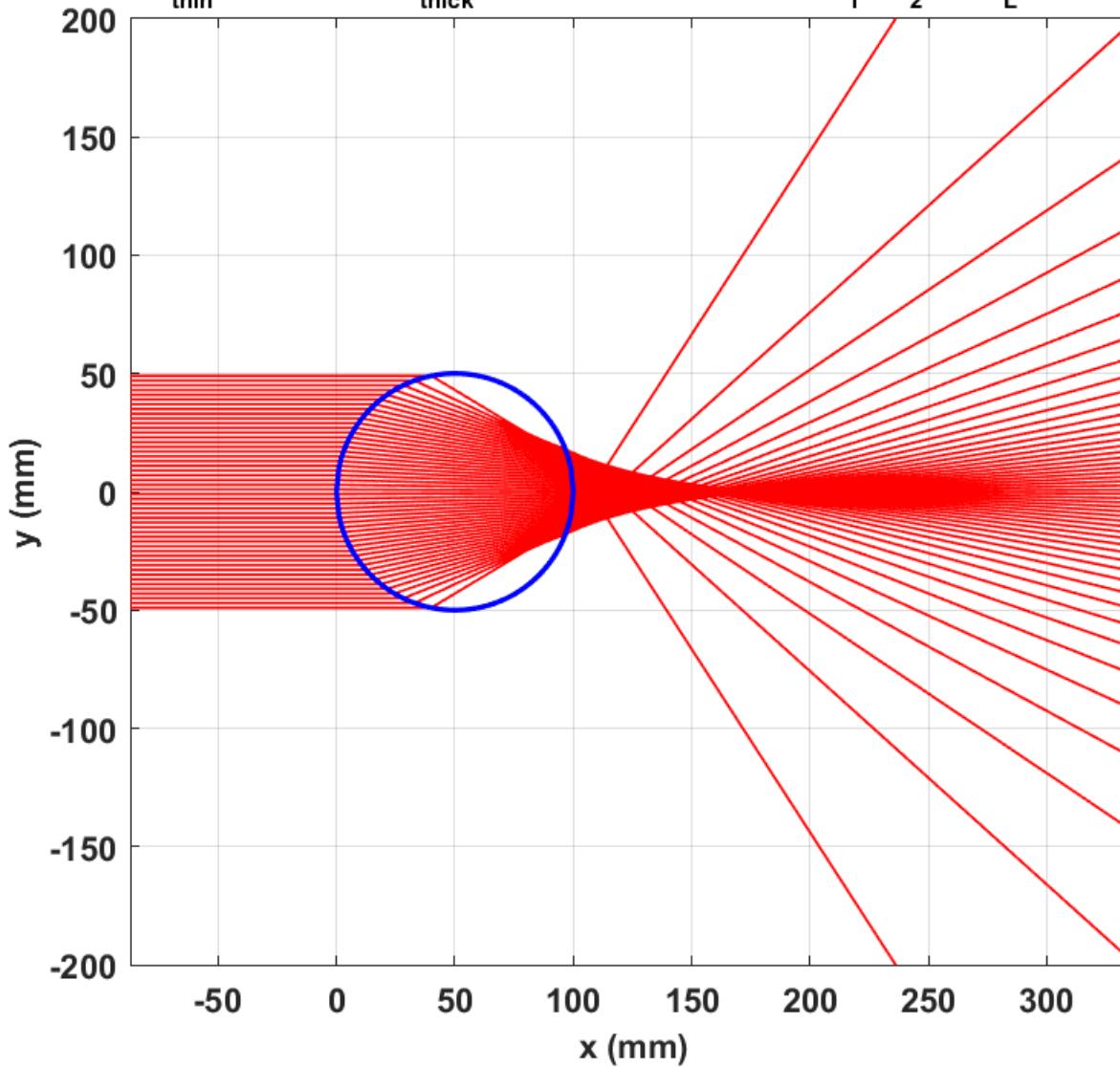
Spherical Aberration of a Dielectric Sphere



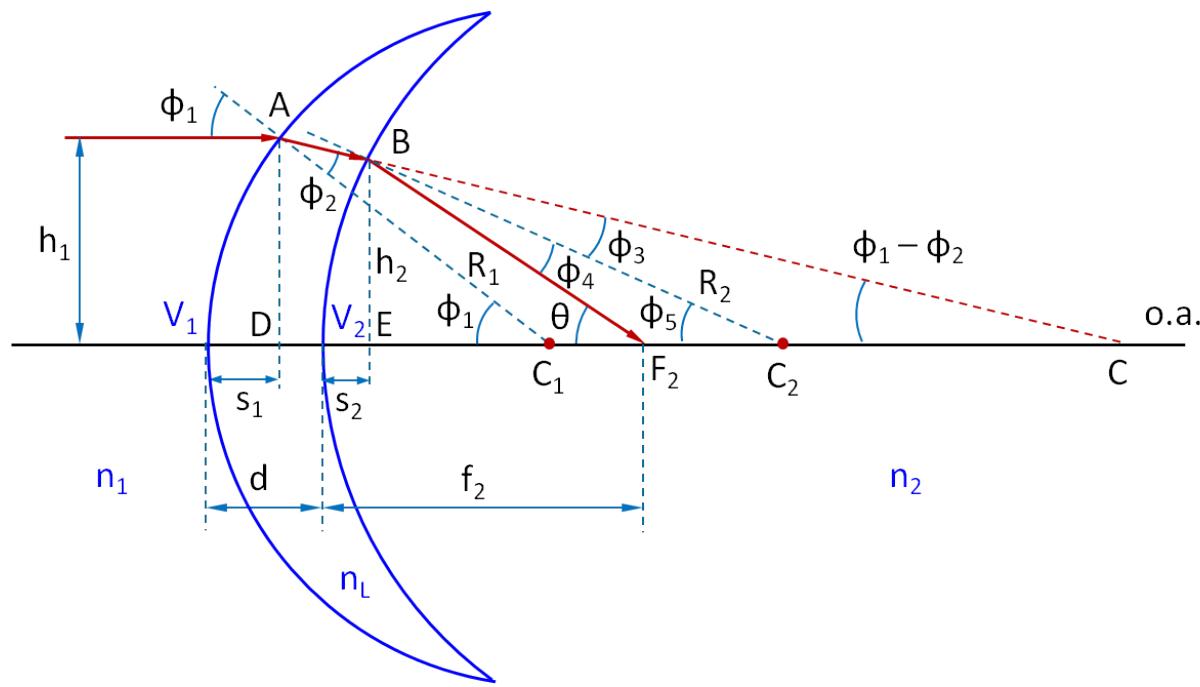
Spherical Aberration of a Dielectric Sphere

Biconvex Lens, $R_1 = 50\text{mm}$, $R_2 = 50\text{mm}$

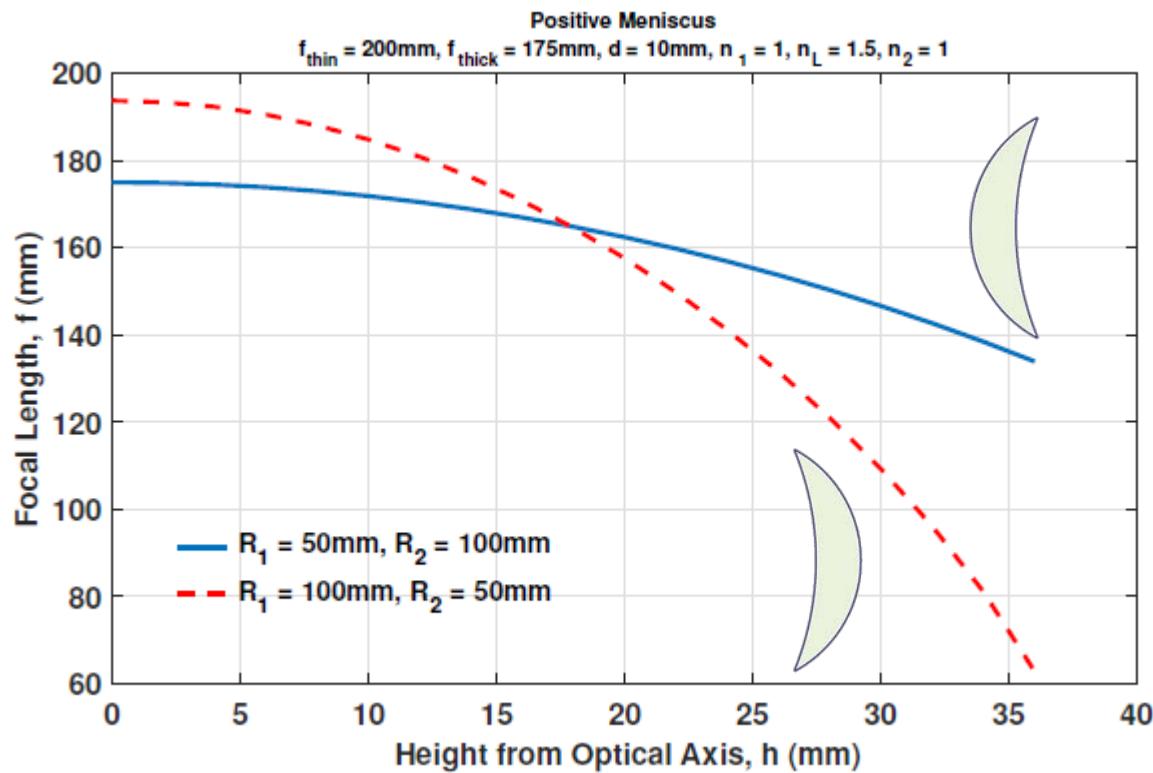
$f_{\text{thin}} = 75.7576\text{mm}$, $f_{\text{thick}} = 50.7576\text{mm}$, $d = 100\text{mm}$, $n_1 = n_2 = 1$, $n_L = 1.33$



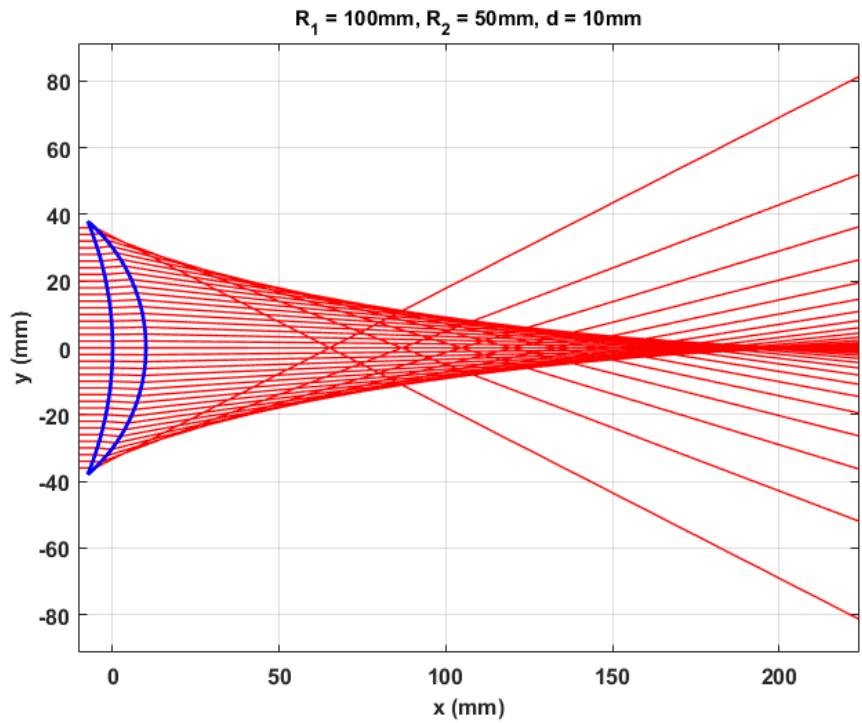
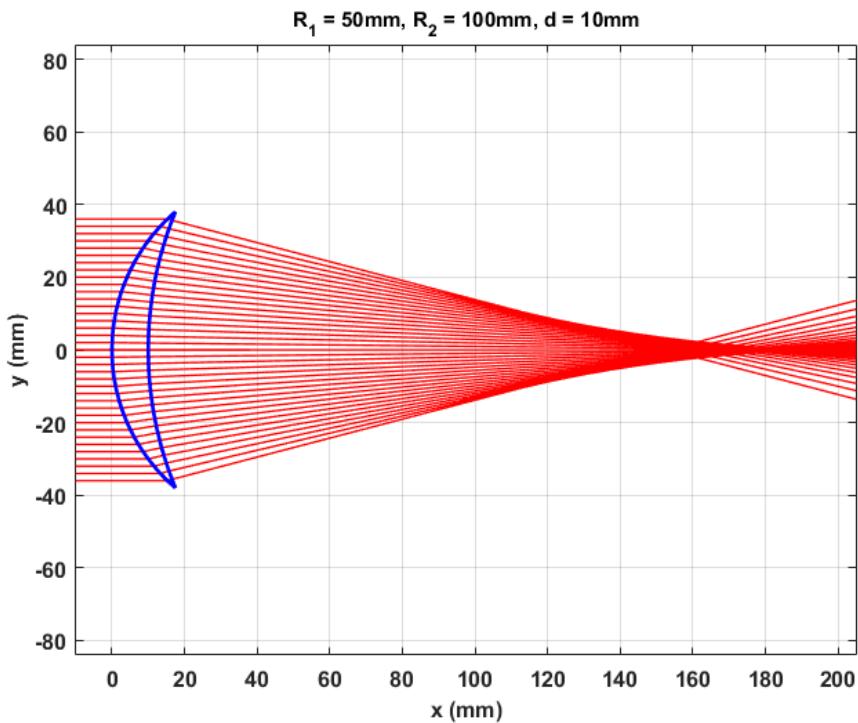
Spherical Aberration of a Positive Meniscus



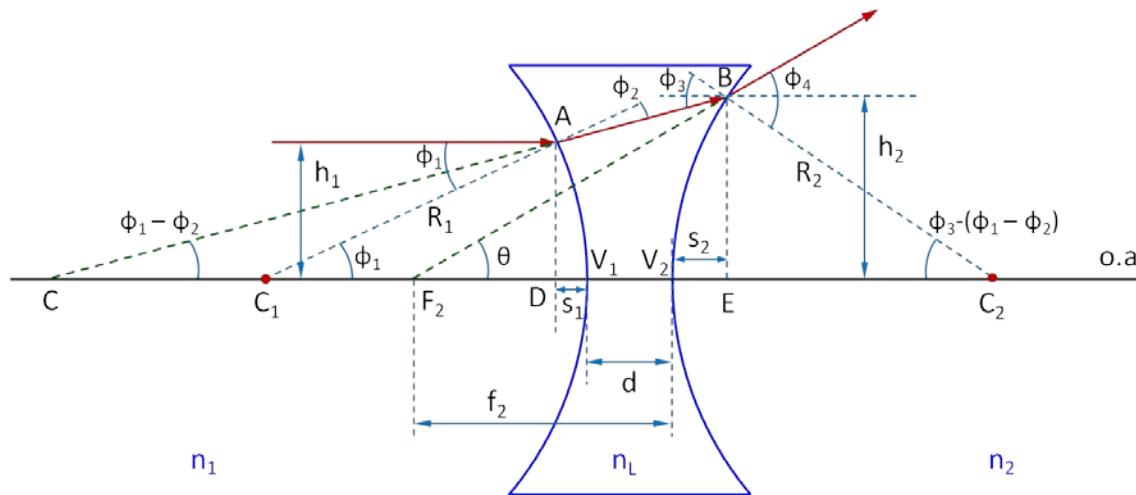
Spherical Aberration of a Positive Meniscus



Spherical Aberration of a Positive Meniscus

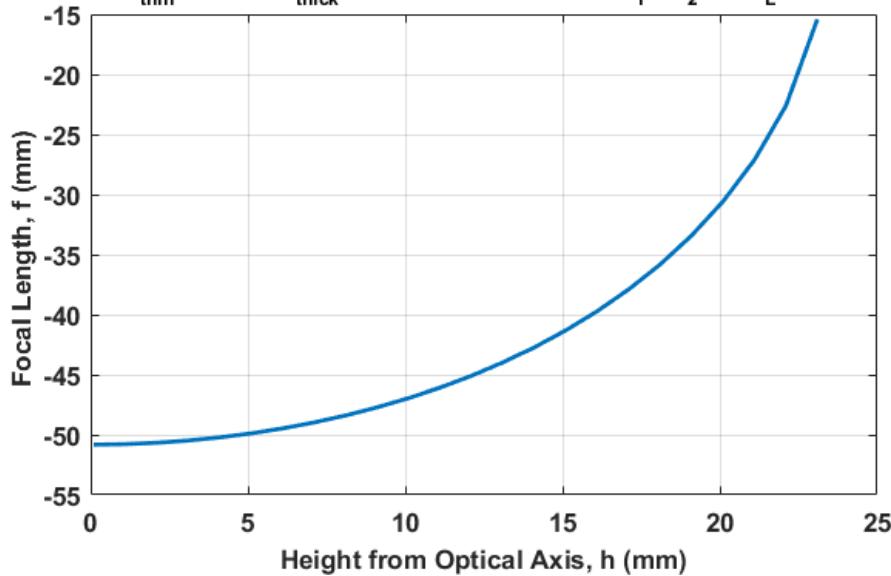


Spherical Aberration of a Biconcave Lens



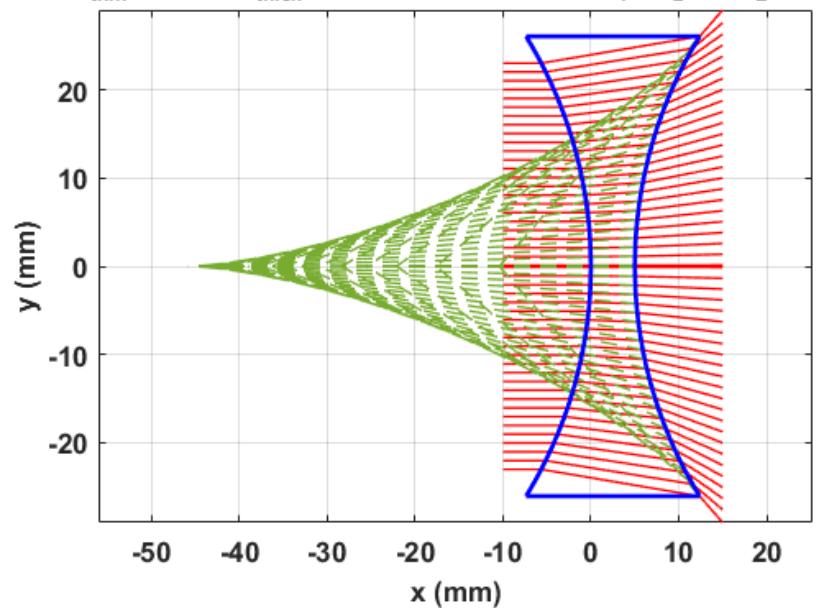
Biconcave Lens, $R_1 = 50\text{mm}$, $R_2 = 50\text{mm}$

$$f_{\text{thin}} = -50\text{mm}, f_{\text{thick}} = -50.8197\text{mm}, d = 5\text{mm}, n_1 = n_2 = 1, n_L = 1.5$$

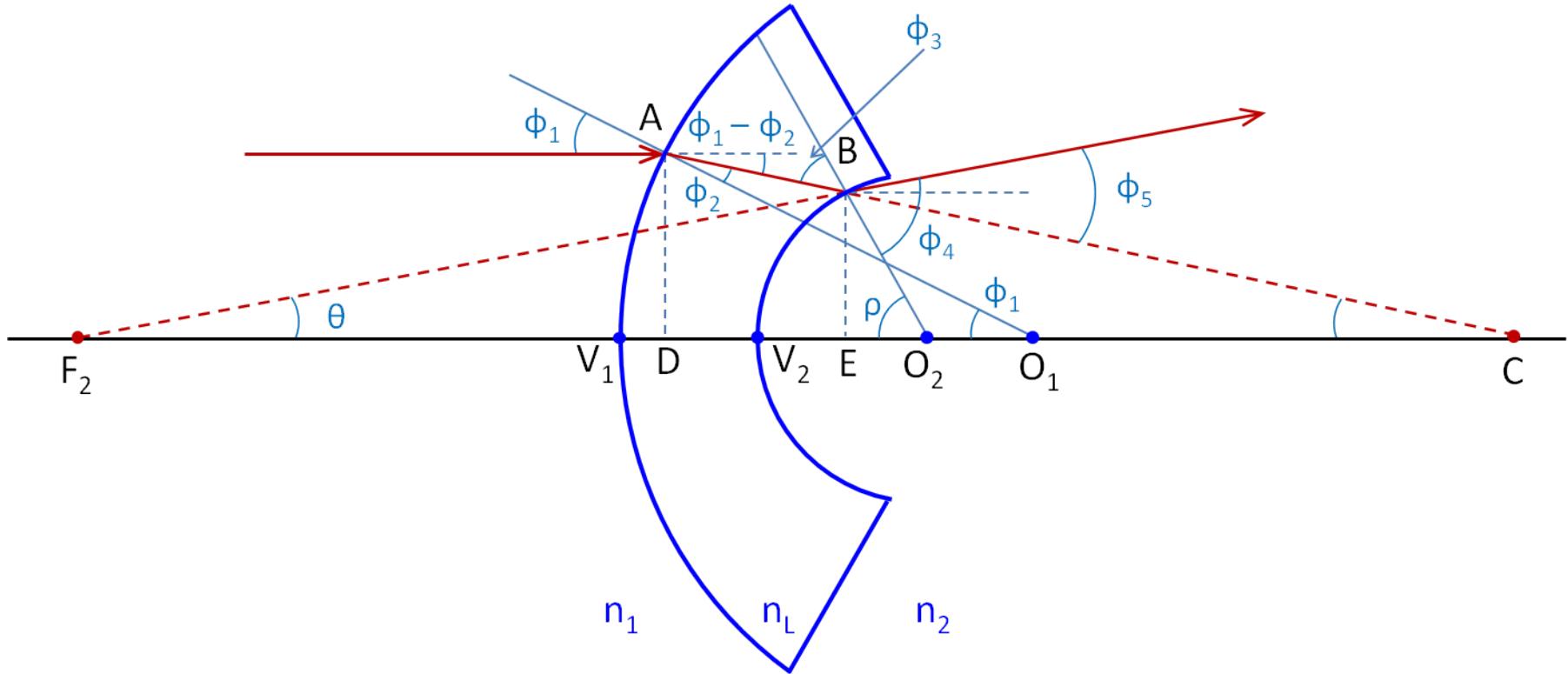


Biconcave Lens, $R_1 = 50\text{mm}$, $R_2 = 50\text{mm}$

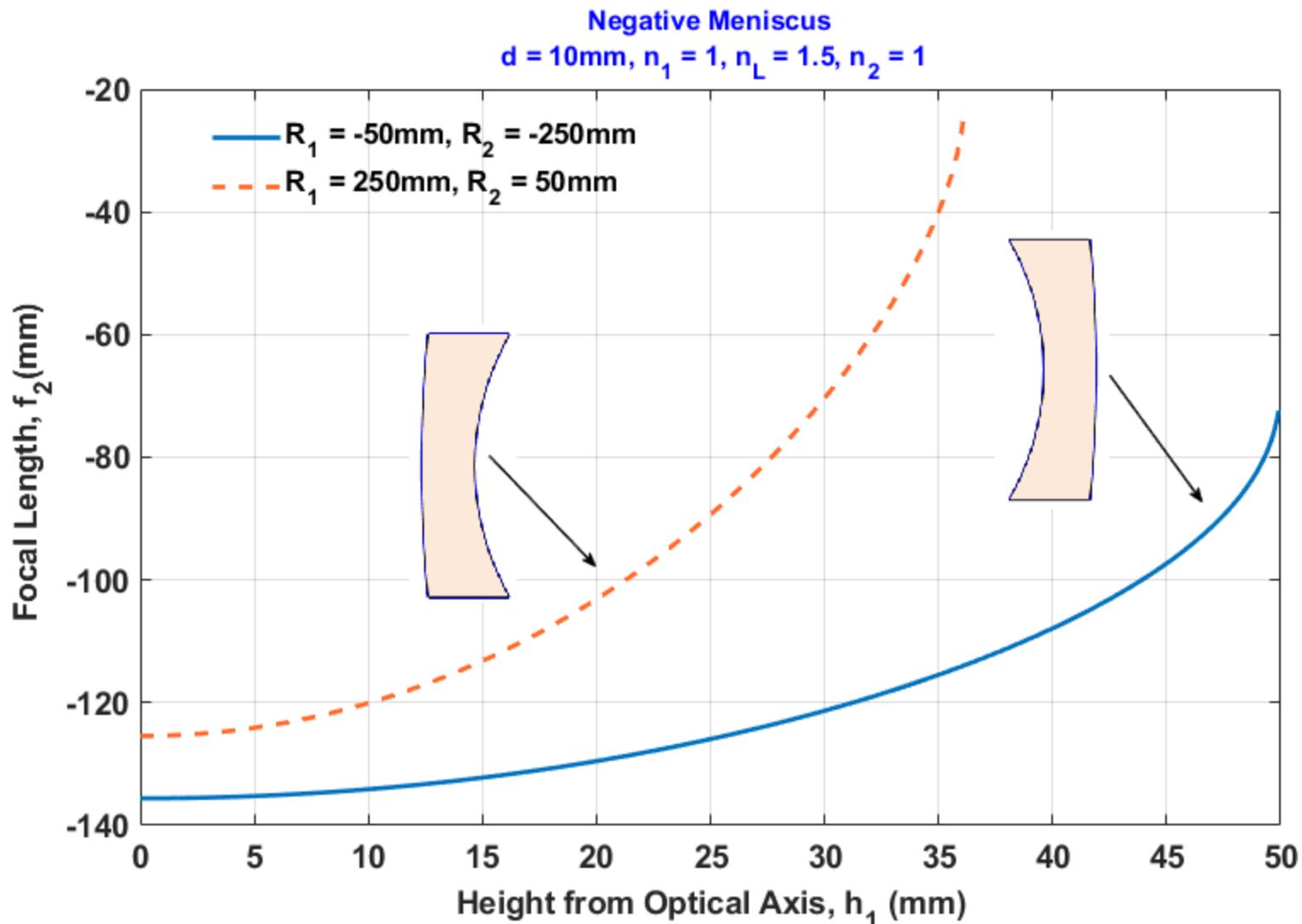
$$f_{\text{thin}} = -50\text{mm}, f_{\text{thick}} = -50.8197\text{mm}, d = 5\text{mm}, n_1 = n_2 = 1, n_L = 1.5$$



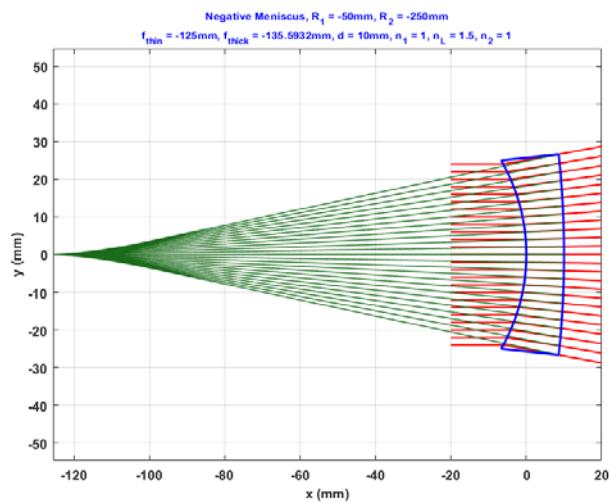
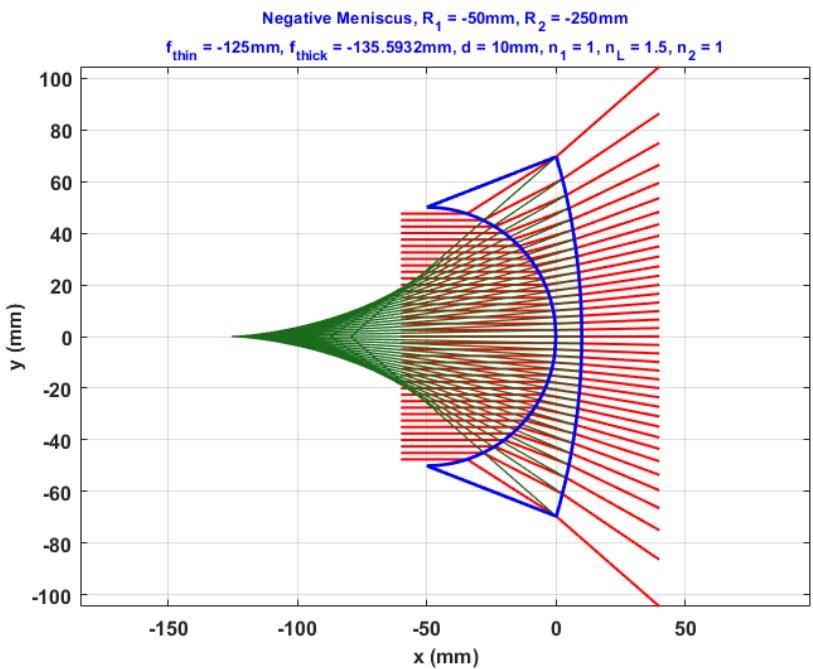
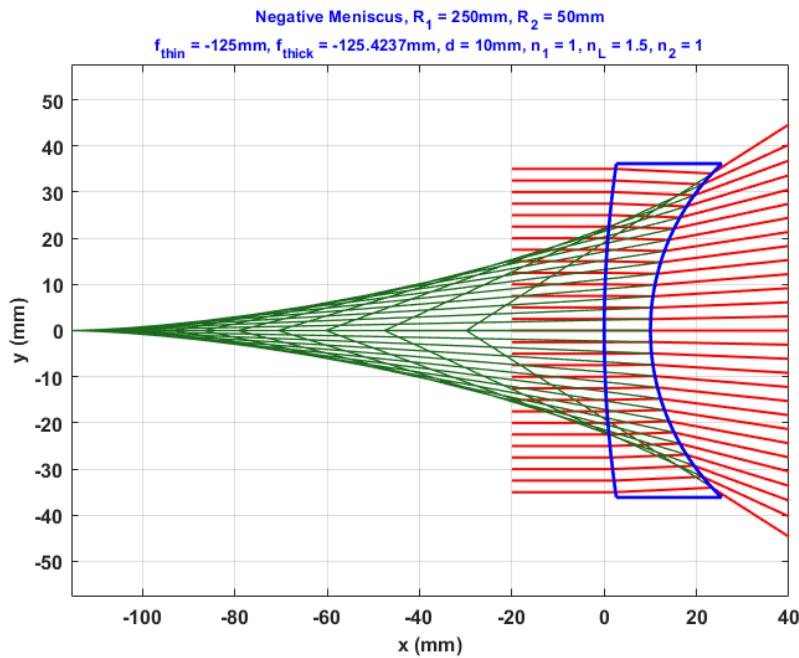
Spherical Aberration of a Negative Meniscus



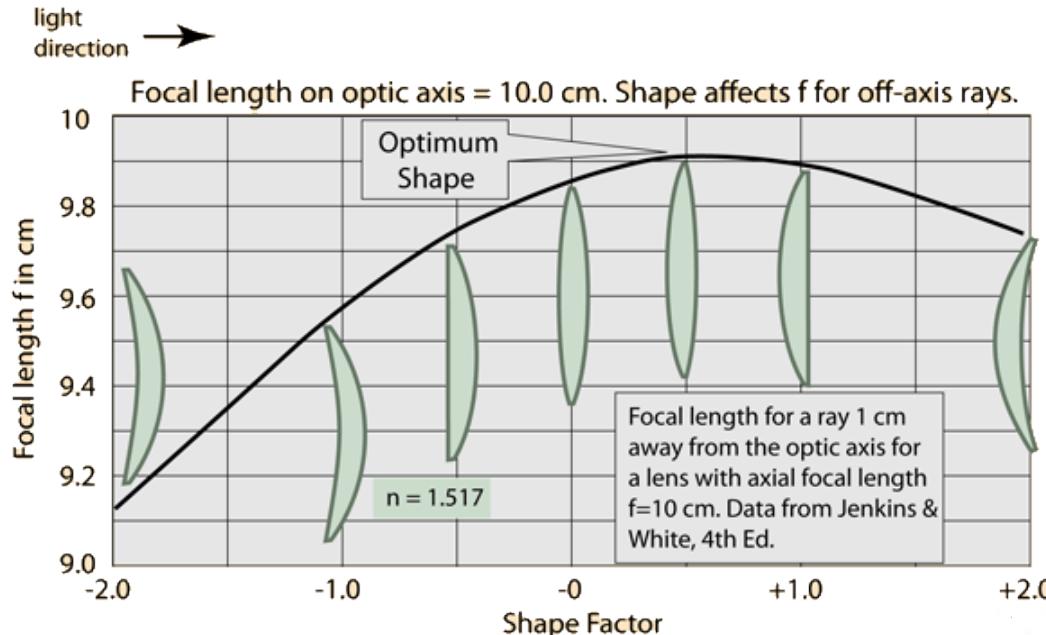
Spherical Aberration of a Negative Meniscus



Spherical Aberration of a Negative Meniscus



Spherical Aberration



<http://hyperphysics.phy-astr.gsu.edu/hbase/geoopt/imggo/meniscus.gif>

Shape Factor

$$\sigma = \frac{R_2 + R_1}{R_2 - R_1}$$

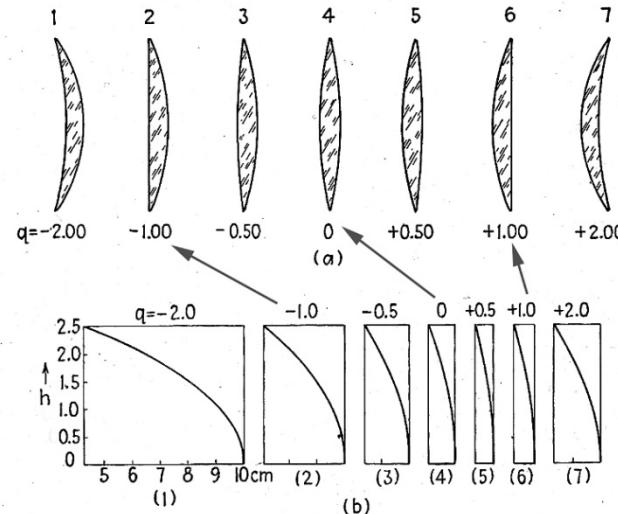
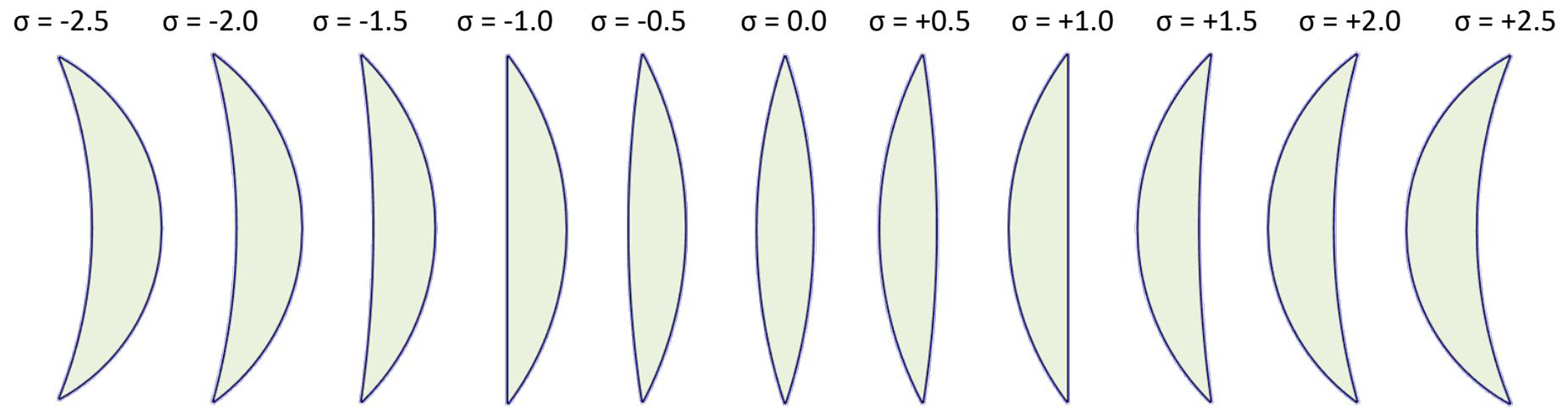


FIG. 9C (a) Lenses of different shapes but with the same power. The difference is one of "bending." (b) Focal length vs. radius for these lenses.

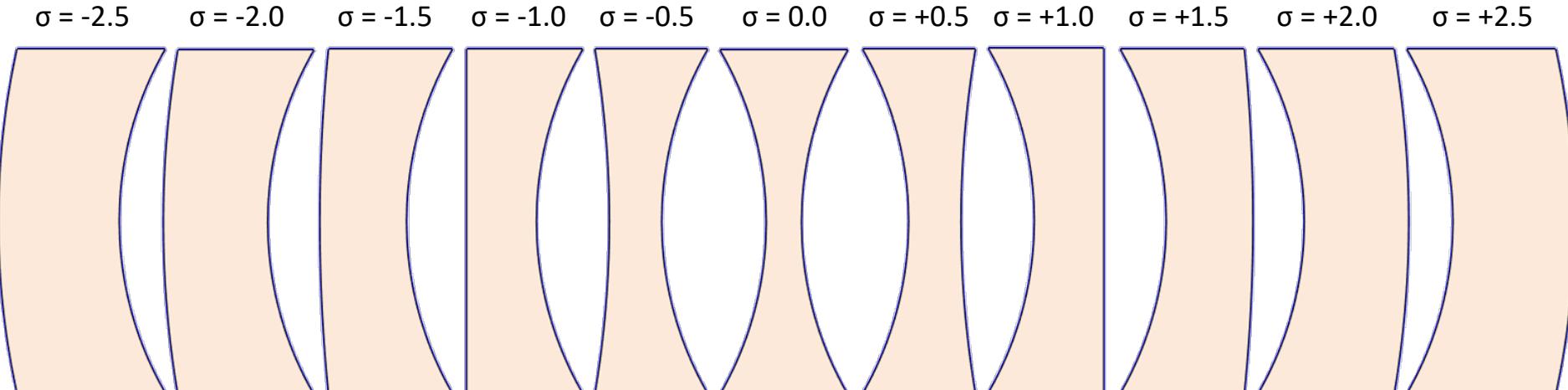
Jenkins and White, "Fundamentals of Optics", 4th Ed., McGraw-Hill, 2001

Spherical Aberration – Shape Factor

$f = 50\text{mm}$

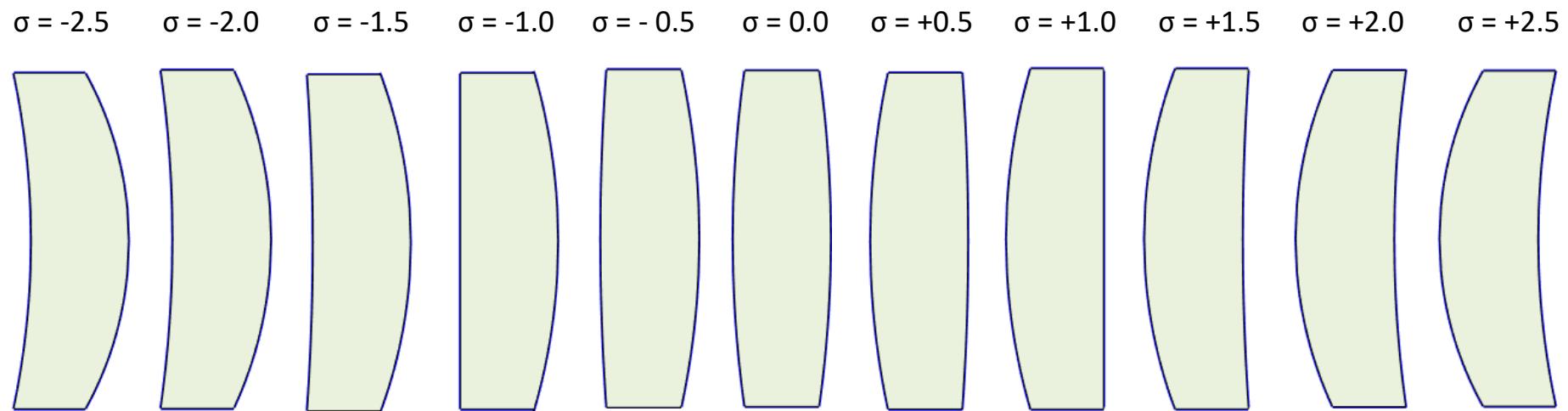


$f = -50\text{mm}$

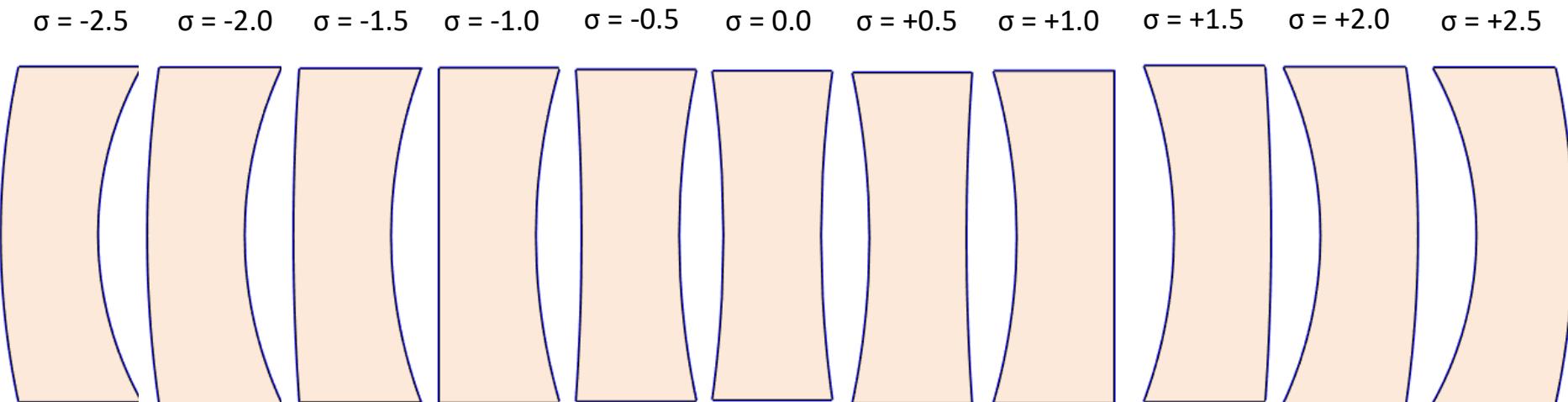


Spherical Aberration – Shape Factor

$f = 50\text{mm}$



$f = -50\text{mm}$

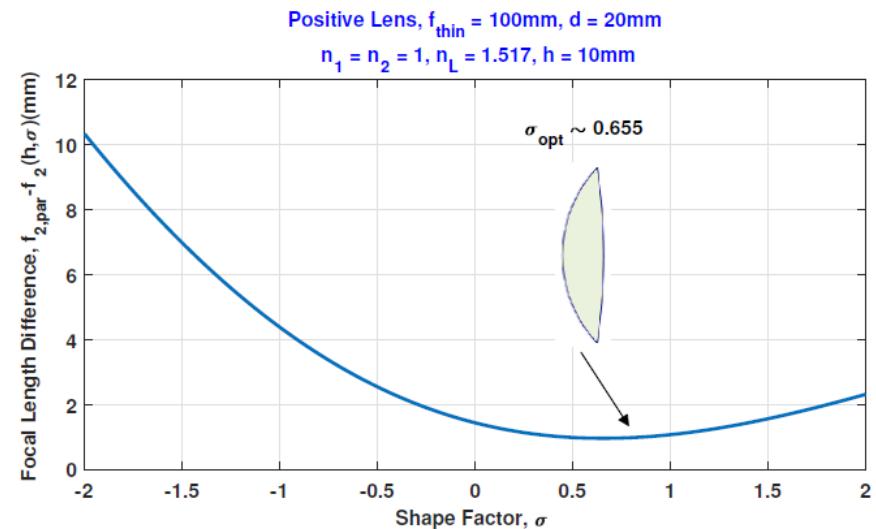
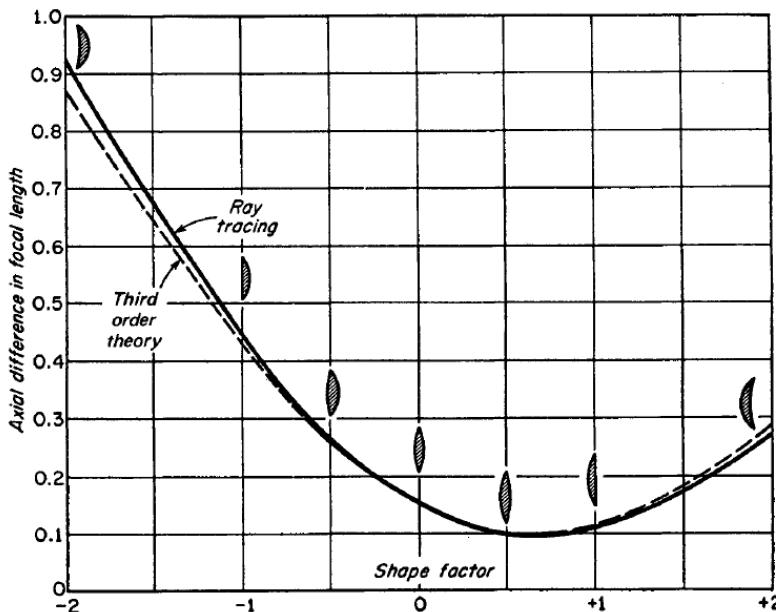


Spherical Aberration (3rd order)

$$\frac{1}{s'(h)} - \frac{1}{s'(0)} = \frac{h^2}{8f^3 n(n-1)} \left[\frac{n+2}{n-1} \sigma^2 + 4(n+1)p\sigma + (3n+2)(n-1)p^2 + \frac{n^3}{n-1} \right]$$

$$p = \frac{s' - s}{s' + s}, \quad \sigma = \frac{R_2 + R_1}{R_2 - R_1}$$

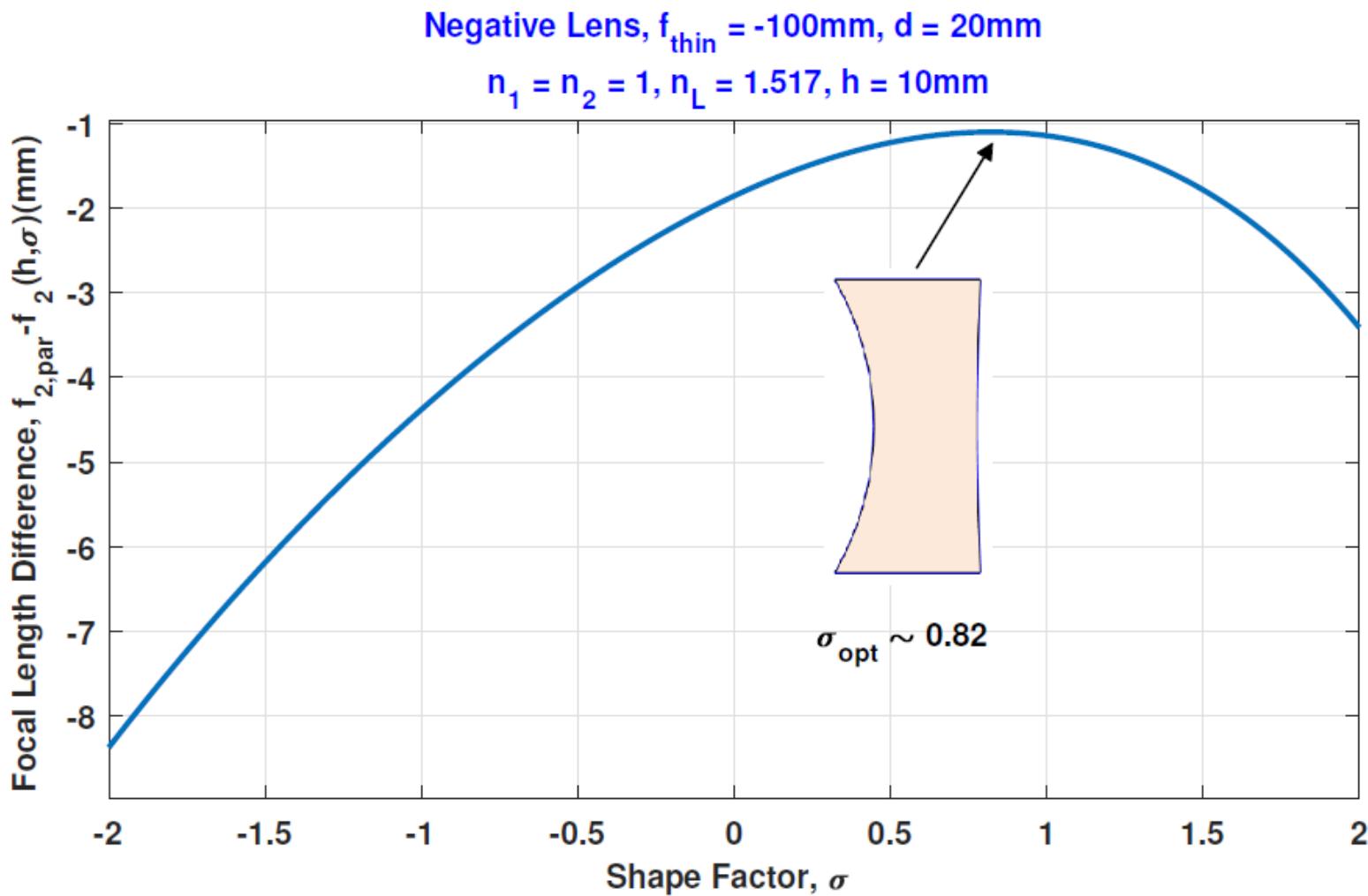
$$\sigma_{opt} = -\frac{2(n^2 - 1)}{n + 2} \frac{s' + s}{s' - s}$$



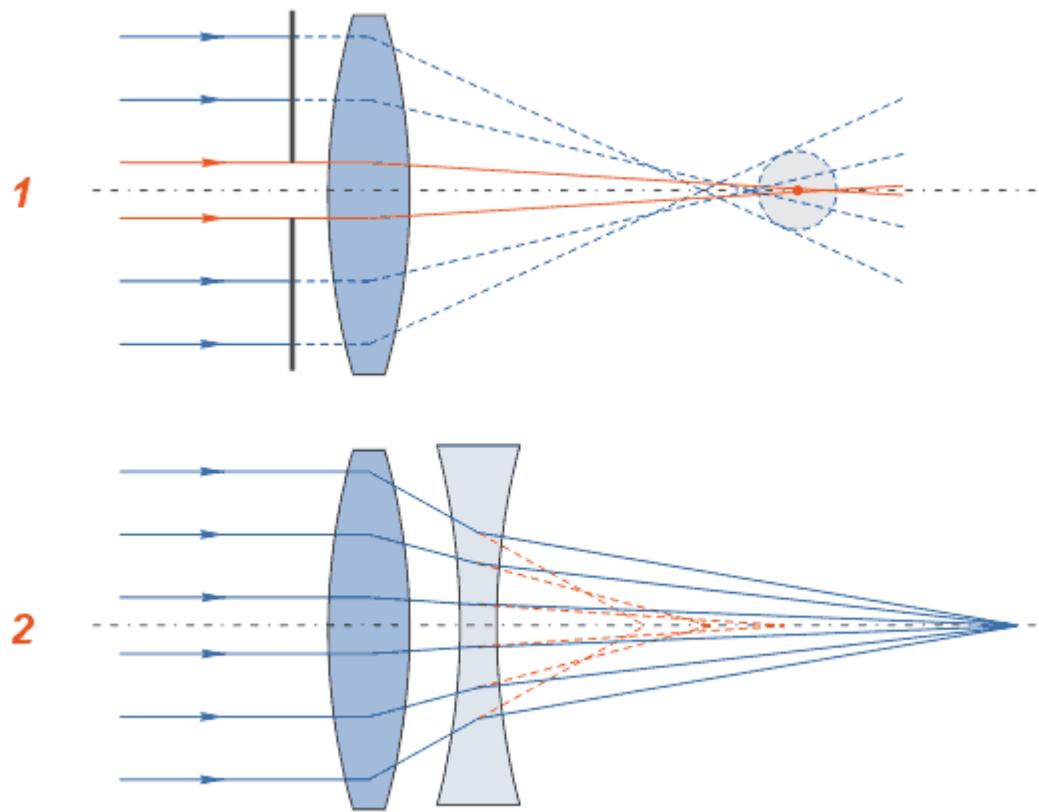
$$\sigma_{opt,3rd} = 0.74 \quad \sigma_{opt} = 0.655$$

Jenkins and White, "Fundamentals of Optics", 4th Ed., McGraw-Hill, 2001

Spherical Aberration for Negative Lenses



Spherical Aberration Correction



Astigmatism

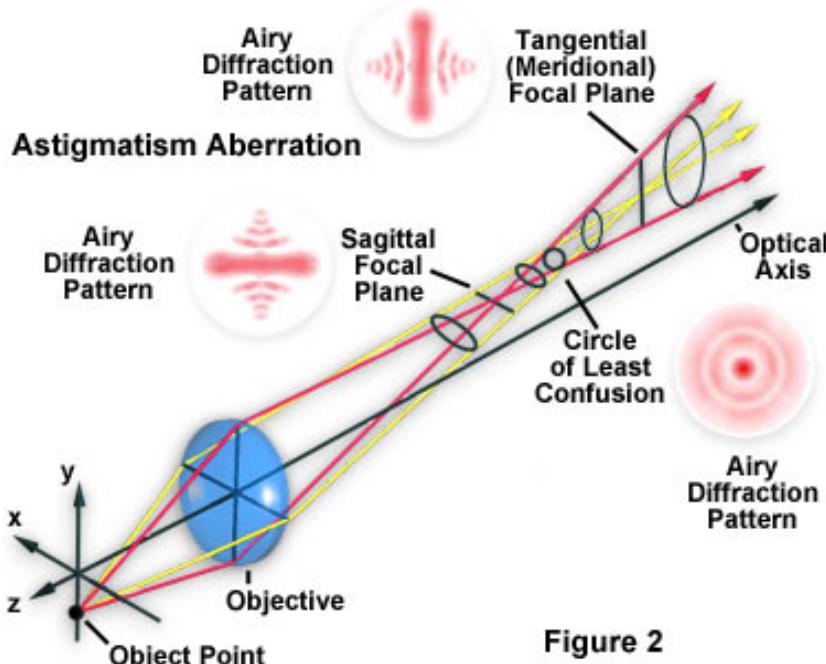
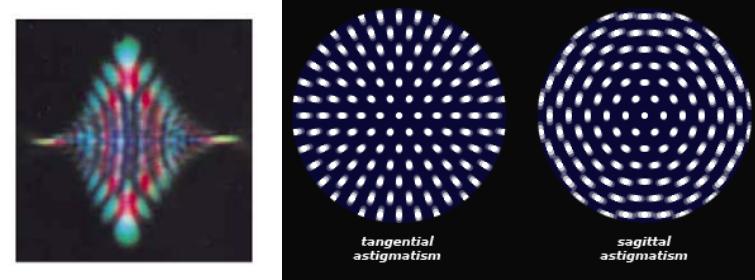
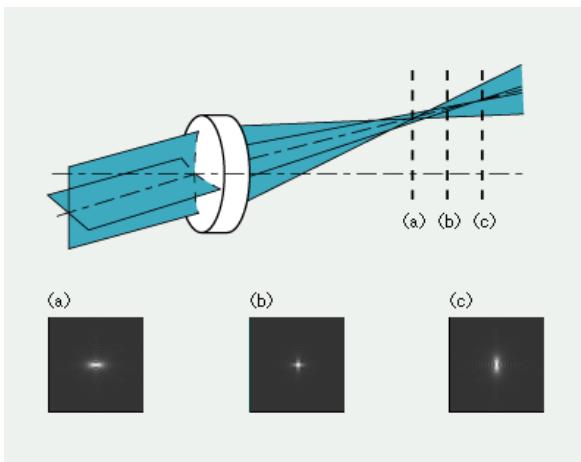


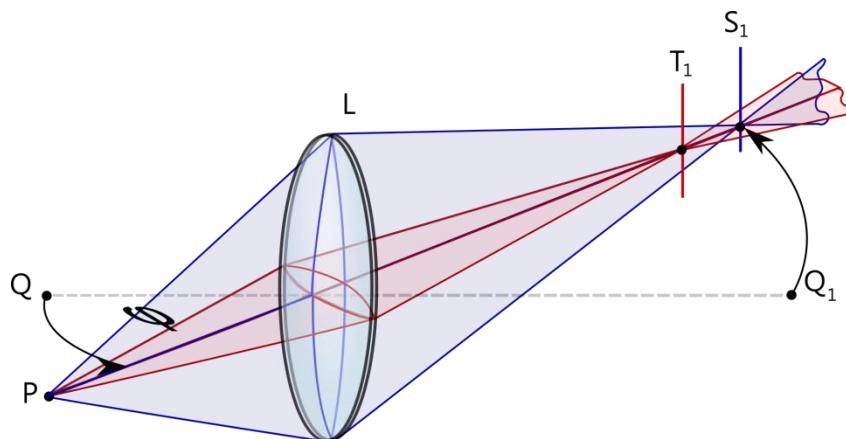
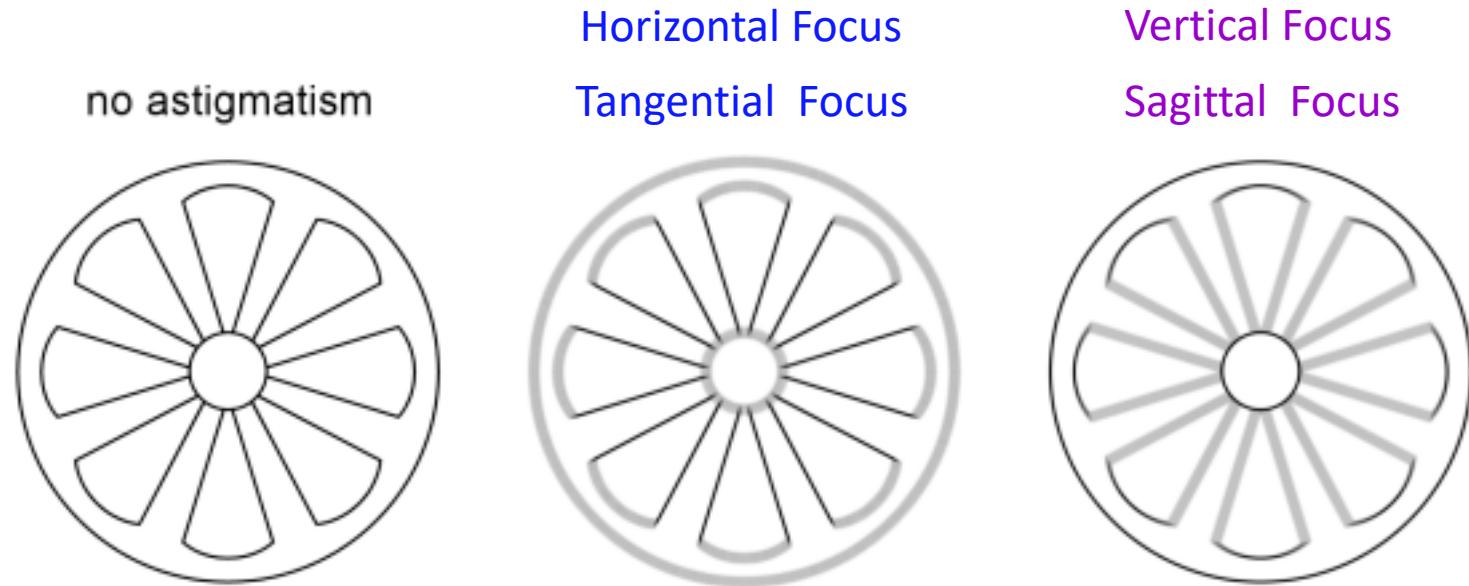
Figure 2

<https://www.olympus-lifescience.com/en/microscope-resource/primer/java/aberrations/astigmatism/#:~:text=Astigmatism%20aberrations%20are%20found%20at,location%20of%20the%20focal%20plane.>



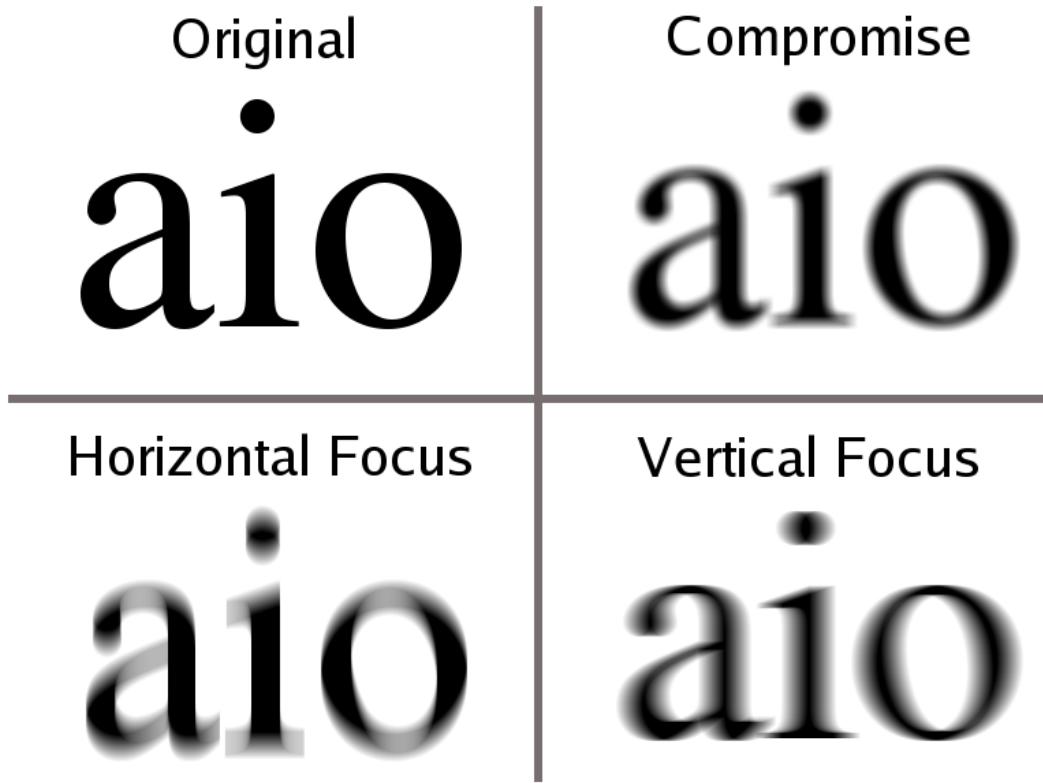
<http://www.handprint.com/ASTRO/ae4.html>

Astigmatism



[https://en.wikipedia.org/wiki/Astigmatism_\(optical_systems\)](https://en.wikipedia.org/wiki/Astigmatism_(optical_systems))

Astigmatism (Examples)



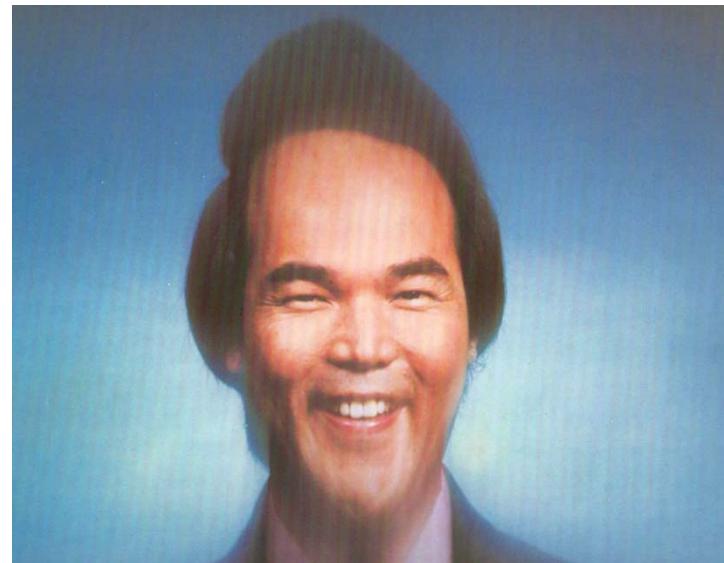
Astigmatism causes blur along one direction



<http://acuitylaservision.com/category/all-about-eyes/medical-blog-acuity/page/3/>

[https://en.wikipedia.org/wiki/Astigmatism_\(optical_systems\)](https://en.wikipedia.org/wiki/Astigmatism_(optical_systems))

Astigmatism Causes Blurring of the Image



Un-aberrated Image

Tangential Focus

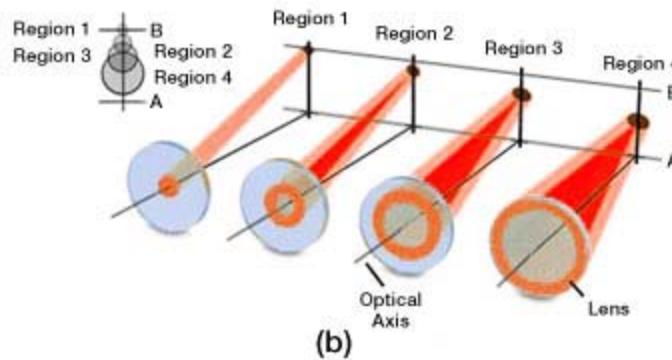
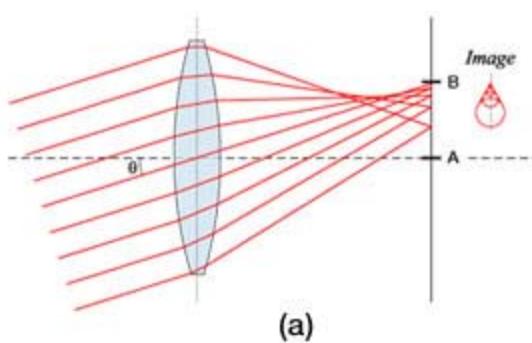
Medial Focus

Sagittal Focus

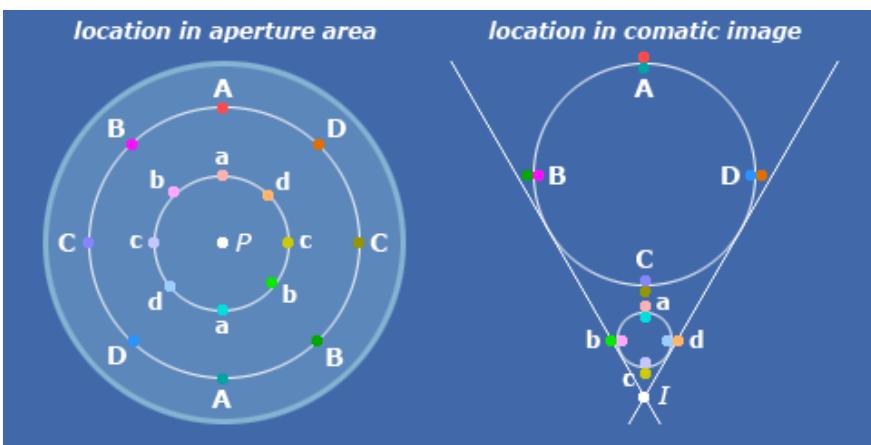


<http://eckop.com/wp-content/uploads/2017/05/Fig-1.14-Tangential-and-Sagittal-Foci.png>

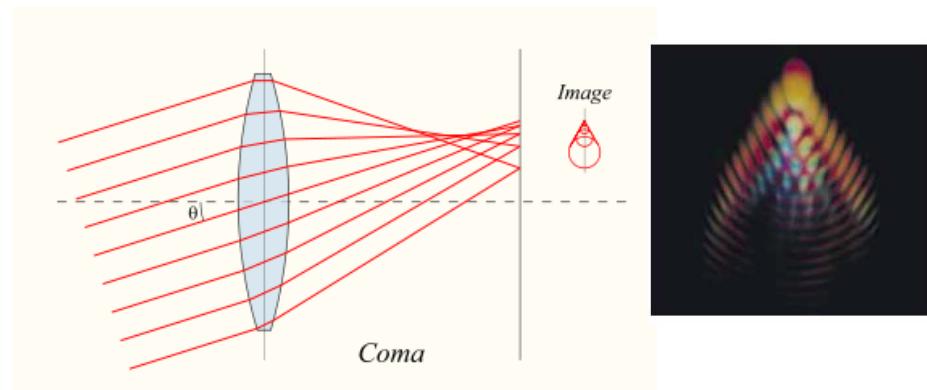
Coma



<http://www.cheyennezjphotographer.com/photography/lenses-2/>

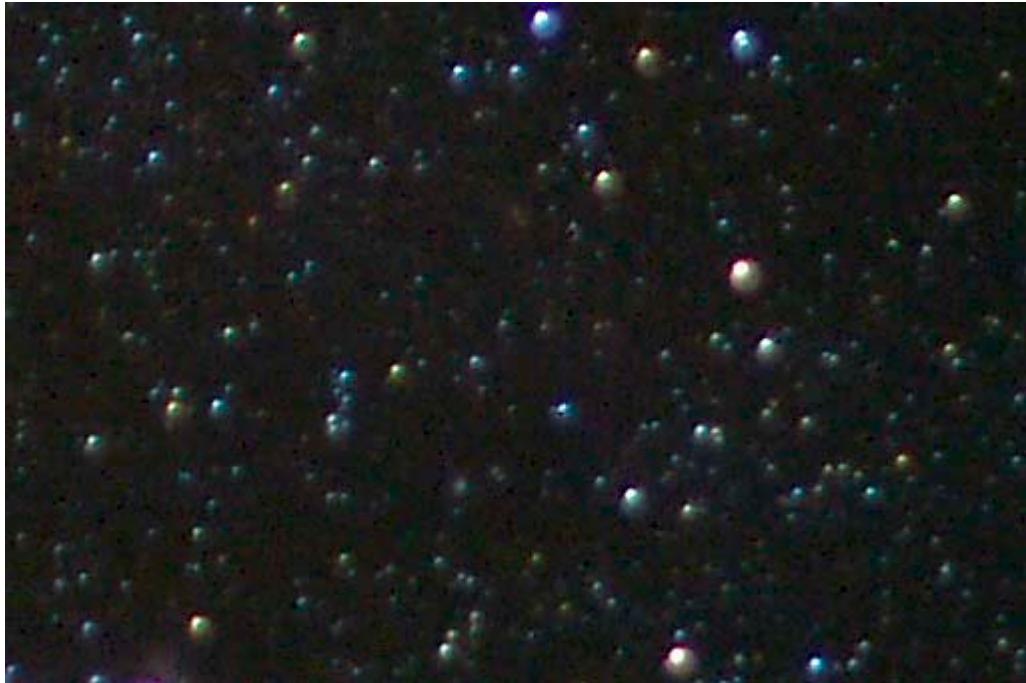


<https://www.handprint.com/ASTRO/ae4.html>

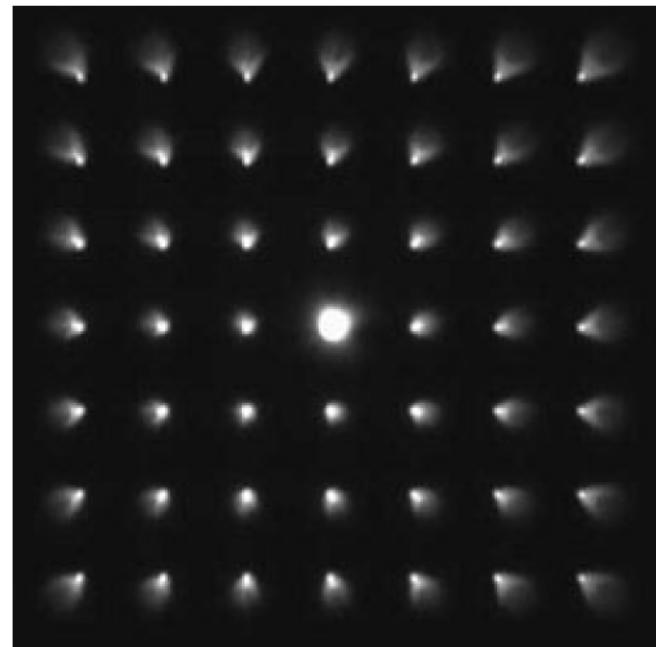
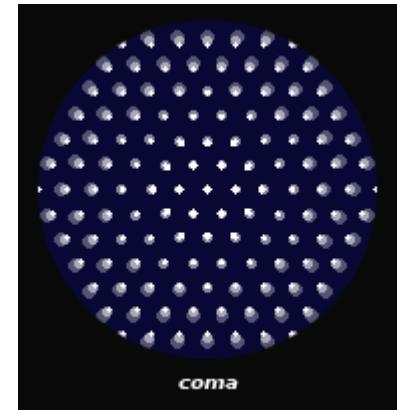


[http://en.wikipedia.org/wiki/Lens_\(optics\)](http://en.wikipedia.org/wiki/Lens_(optics))

Coma (Examples)

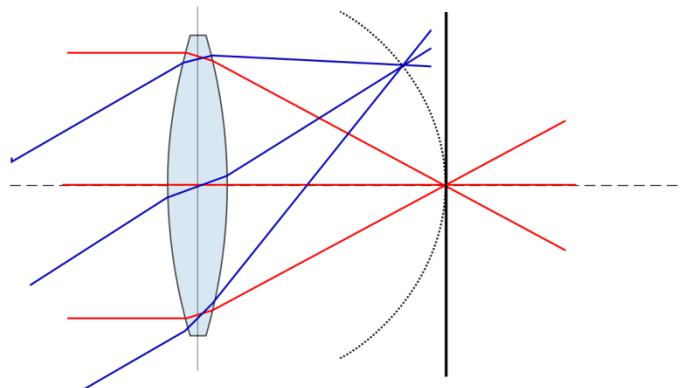


<http://www.handprint.com/ASTRO/ae4.html>



Field Curvature

Field curvature: the image "plane" (the arc) deviates from a flat surface (the vertical line).



https://en.wikipedia.org/wiki/Petzval_field_curvature

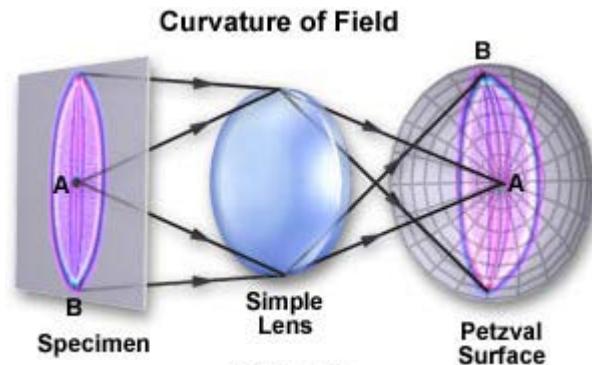
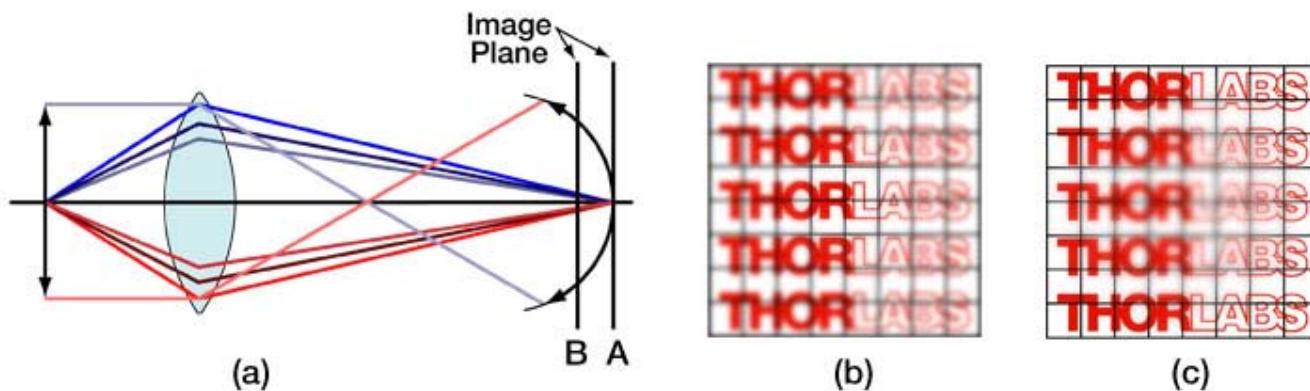


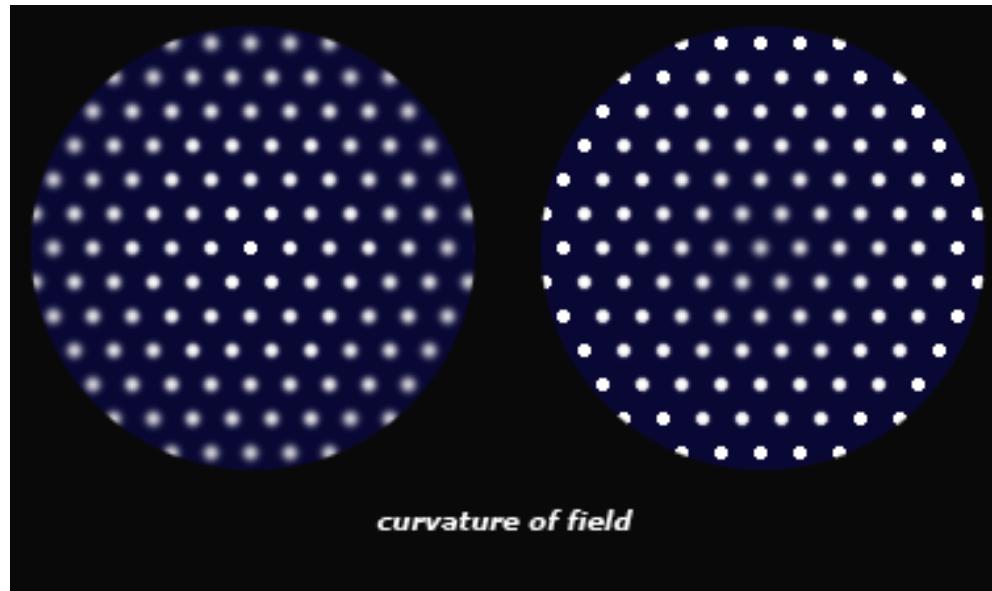
Figure 1

<http://www.microscopyu.com/tutorials/java/aberrations/curvatureoffield/>



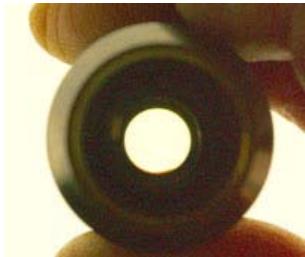
https://sites.astro.caltech.edu/~dmawet/teaching/2018-2019/ay105-lab-experiment_7-1.pdf

Field Curvature

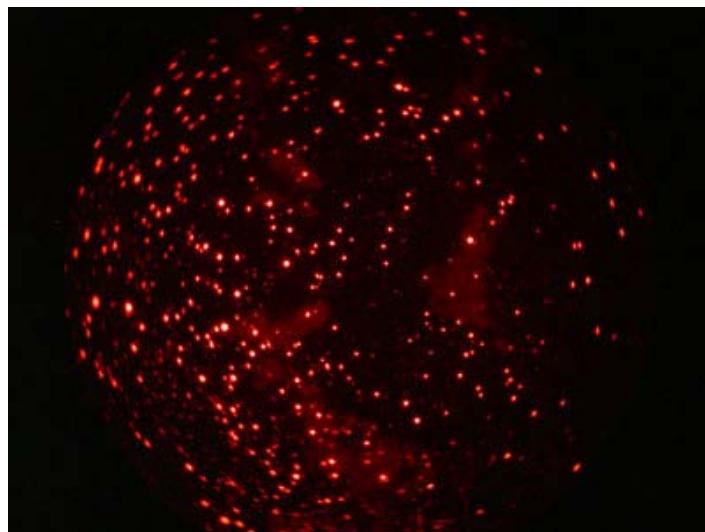
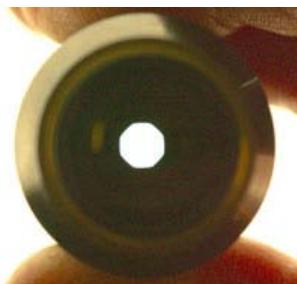


<http://www.handprint.com/ASTRO/ae4.html>

Field Curvature



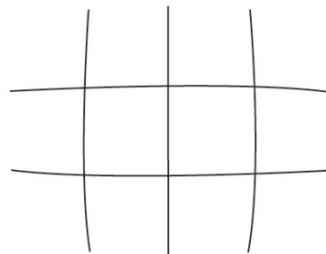
Notice that with a closed iris the distortion is greatly reduced, however the light gathering power of the lens is also reduced. Under dim fluorescence conditions the decrease in pixel intensity may be unacceptable.



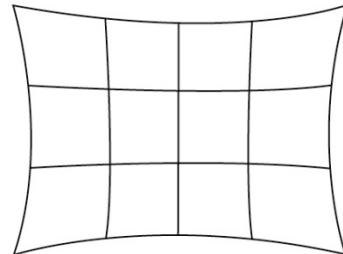
<https://microscopy.berkeley.edu/Resources/aberrations/curvature.html>

Distortion

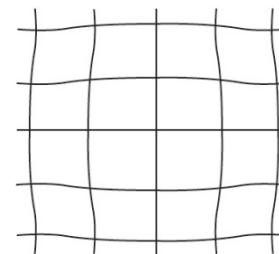
Barrel Distortion



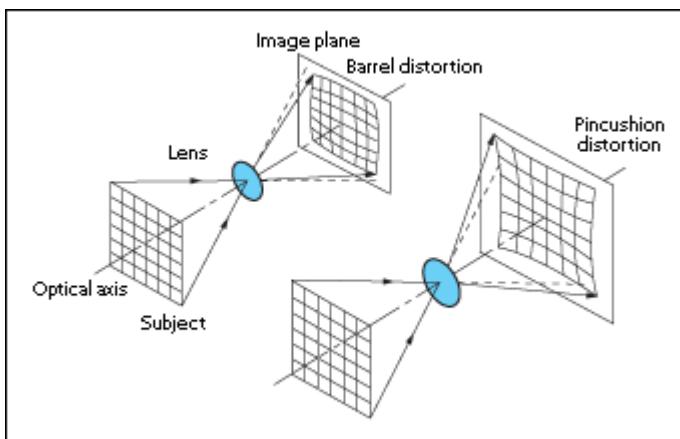
Pincushion Distortion



Moustache Distortion



<https://www.bhphotovideo.com/explora/photography/tips-and-solutions/optical-anomalies-and-lens-corrections-explained>



Distortion



Barrel Distortion



Pincushion Distortion

Pincushion Distortion Aberration

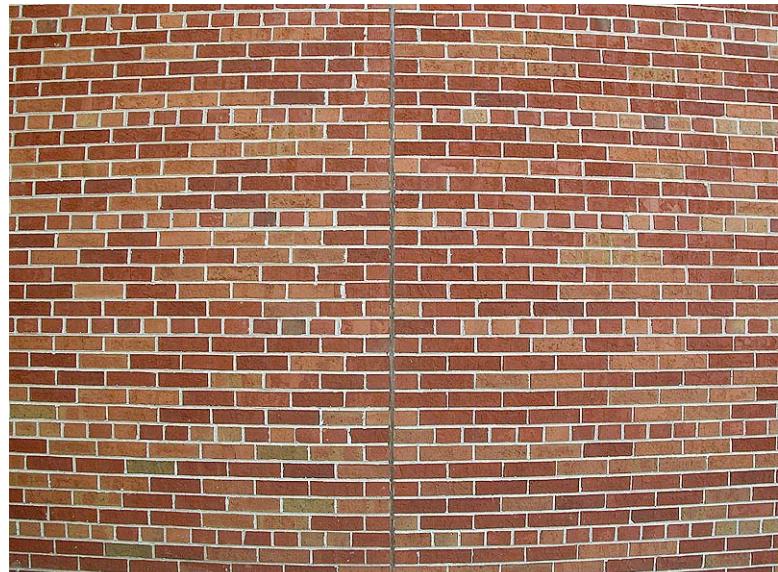


Barrel and Pincushion Distortion Aberrations



<https://www.bhphotovideo.com/explora/photography/tips-and-solutions/optical-anomalies-and-lens-corrections-explained>

Barrel Distortion Aberration



Distortion



Pincushion distortion
aberration

Barrel distortion
aberration

<http://www.azurephotonics.com/22.files/image010.jpg>

Distortion Aberrations

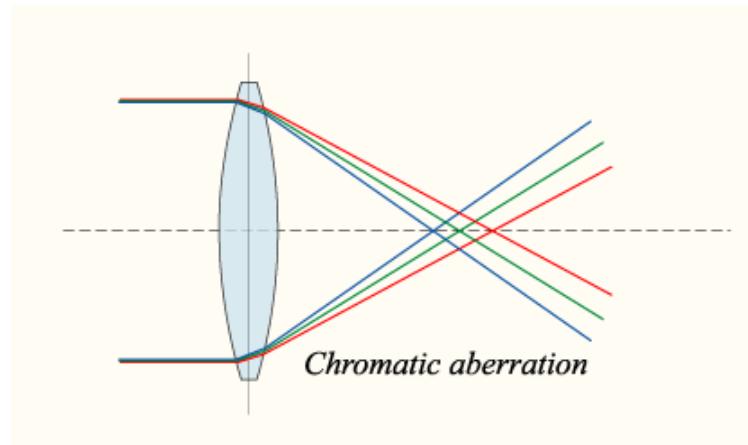
Barrel distortion
aberration



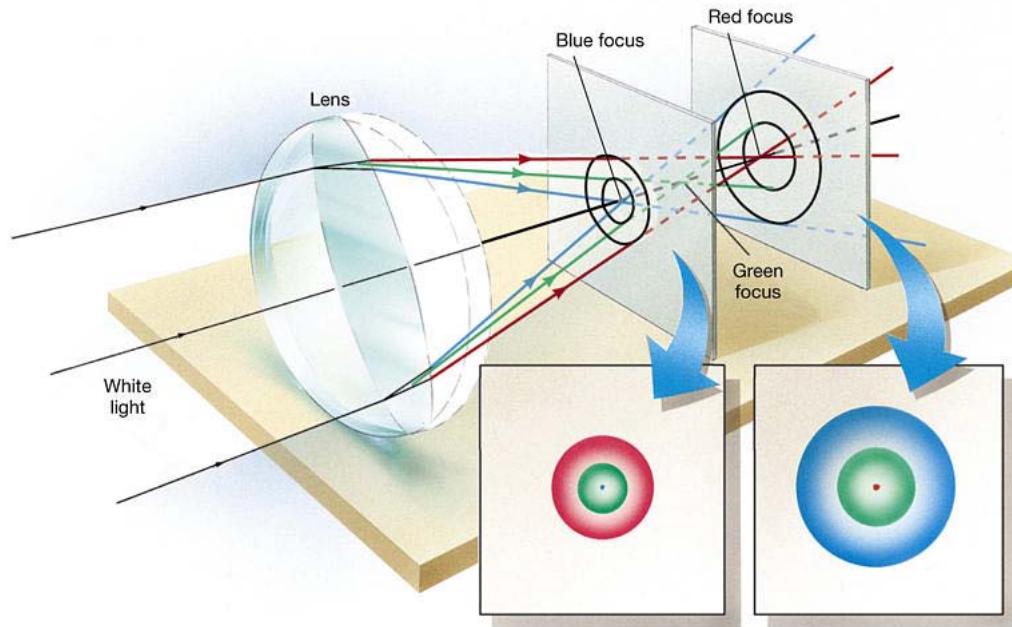
Pincushion distortion
aberration



Chromatic Aberration



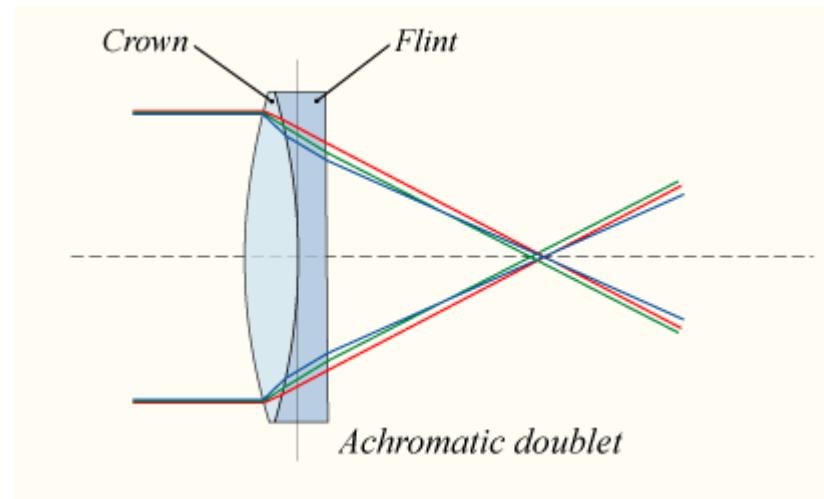
[http://en.wikipedia.org/wiki/Lens_\(optics\)](http://en.wikipedia.org/wiki/Lens_(optics))



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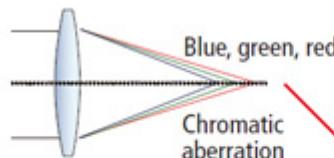
http://pages.uoregon.edu/jimbrau/BraulmNew/Chap05/FG05_05.jpg

Chromatic Aberration Correction



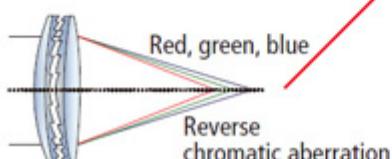
[http://en.wikipedia.org/wiki/Lens_\(optics\)](http://en.wikipedia.org/wiki/Lens_(optics))

①Refractive lens



Combination of ① and ②

②DO lens

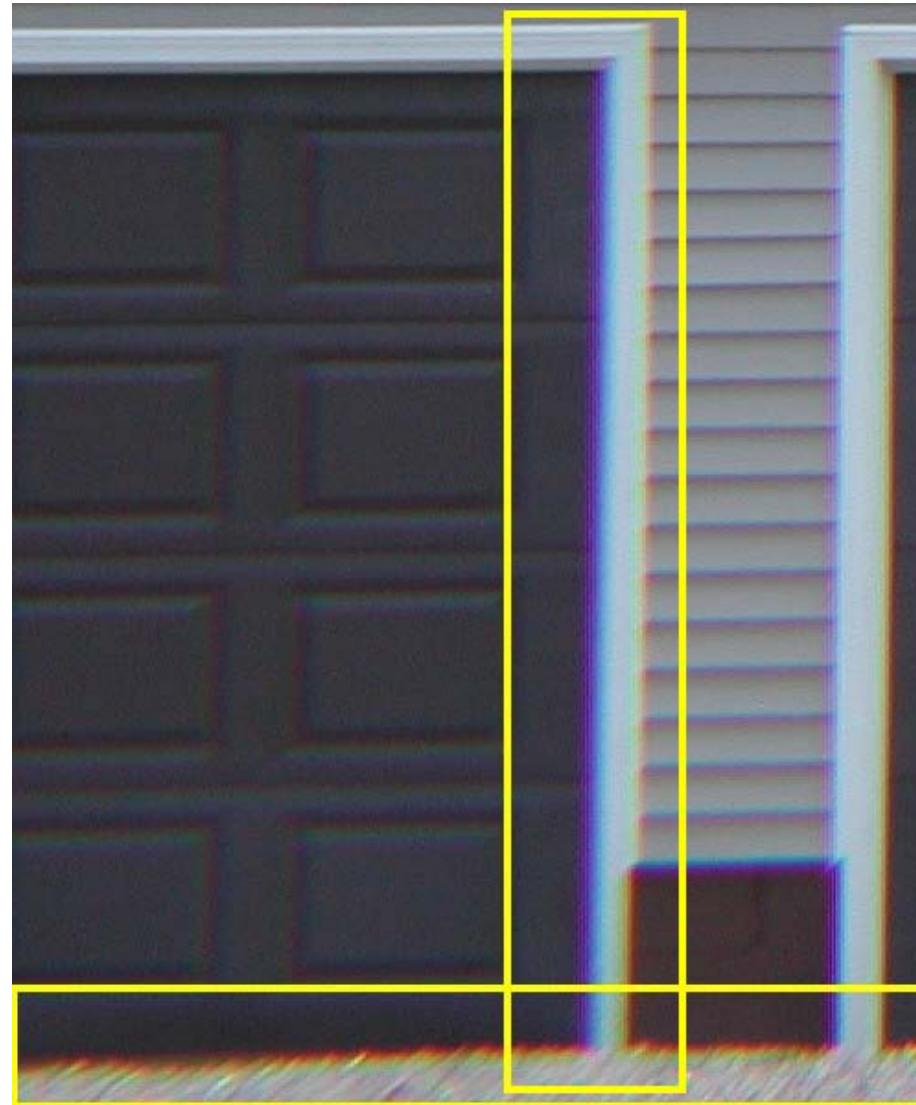


Cancels out chromatic aberration

Chromatic Aberration



Chromatic Aberration



Chromatic Aberration



https://en.wikipedia.org/wiki/Chromatic_aberration

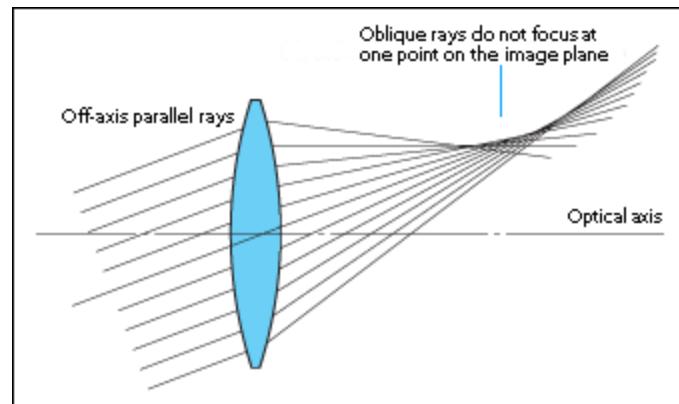
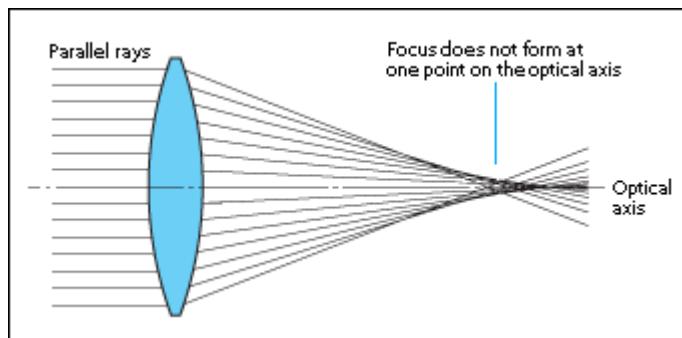
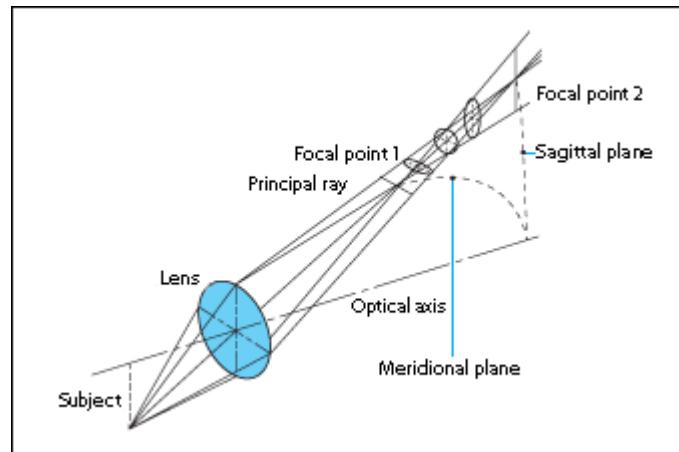
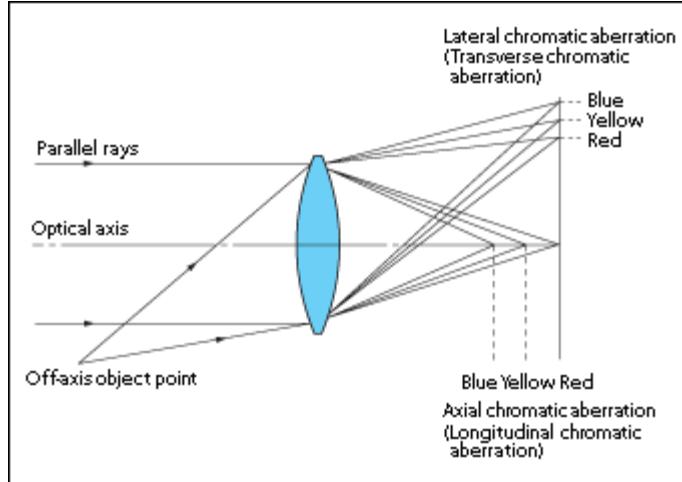


<https://photographylife.com/what-is-chromatic-aberration>

Chromatic Aberration



<https://digital-photography-school.com/chromatic-aberration-what-is-it-and-how-to-avoid-it/>



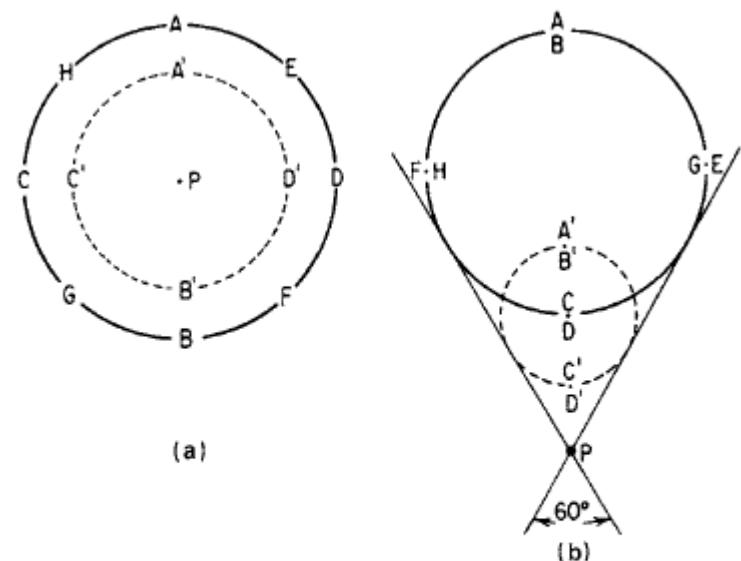
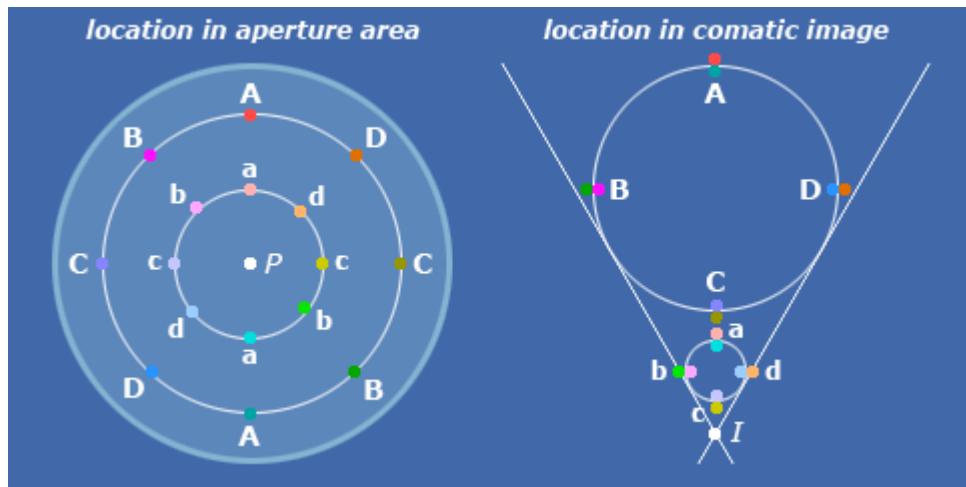
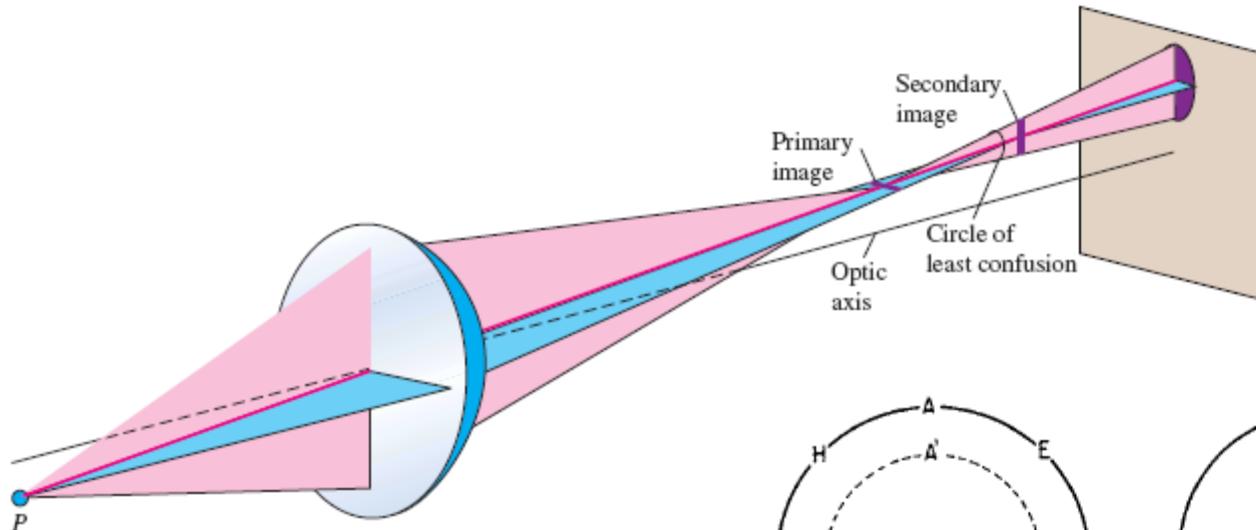


Figure 5.6 The relationship between the position of a ray in the lens aperture and its position in the coma patch.
 (a) View of the lens aperture with rays indicated by letters.
 (b) The letters indicate the positions of the corresponding rays in the image figure. Note that the diameters of the circles in the image are proportional to the square of the diameters in the aperture.

