

Gaussian Beams & Resonators

Electro-Optics & Applications

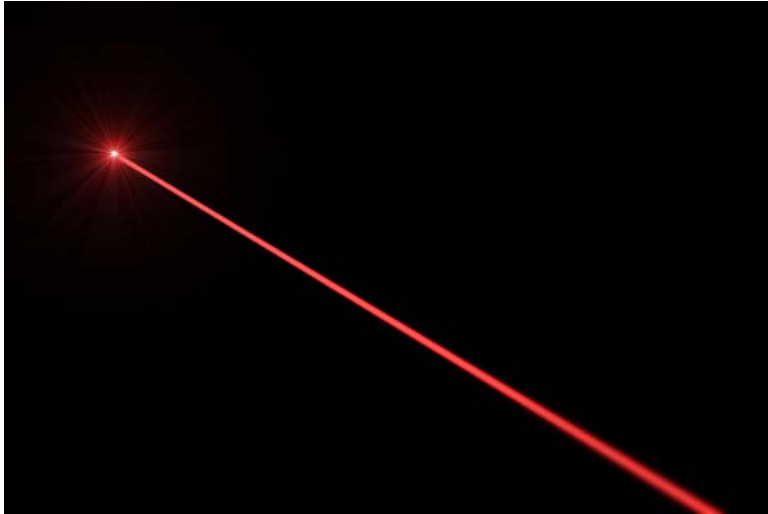
Prof. Elias N. Glytsis



*School of Electrical & Computer Engineering
National Technical University of Athens*

Gaussian Beams

He-Ne Laser



https://wtamu.edu/~cbaird/sq/images/laser_red.png

Green Laser Pointer



https://images-na.ssl-images-amazon.com/images/I/51CVh6BKpUL_SL1000_.jpg

Necessity for an expression of an electromagnetic field with finite cross-sectional area → Gaussian Beams

Gaussian Beams – TEM Solutions

Gauss' Law:

$$\vec{\nabla} \cdot \vec{D} = 0 \implies \vec{\nabla} \cdot \vec{E} = 0,$$

$$\vec{\nabla} \cdot \vec{E} = 0 \implies \vec{\nabla}_t \cdot \vec{E}_t + \frac{\partial E_z}{\partial z} = 0, \quad \vec{E} = \vec{E}_t + E_z \hat{z},$$

Approximations:

$$\frac{\partial E_z}{\partial z} \simeq -j \frac{2\pi}{\lambda_0} n E_z,$$

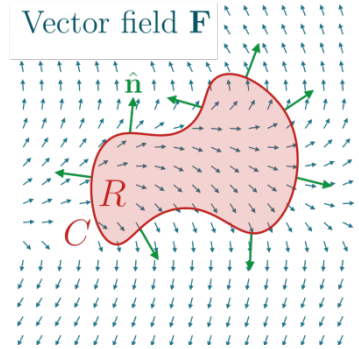
$$\vec{\nabla}_t \cdot \vec{E}_t = \lim_{\Delta S \rightarrow 0} \left\{ \frac{1}{\Delta S} \oint_{\Delta \ell} \vec{E}_t \cdot \hat{i}_{\perp \ell} d\ell \right\} \simeq \lim_{D \rightarrow 0} \left\{ \frac{4}{\pi D^2} |\vec{E}_t| \pi D \right\} \simeq \frac{|\vec{E}_t|}{D},$$

TEM Approximation:

$$|E_z| \simeq \frac{\lambda_0}{2\pi n D} |\vec{E}_t|$$

$$\frac{|E_z|}{|\vec{E}_t|} \simeq \frac{\lambda_0}{2\pi n D} < 10^{-3}$$

2D Divergence



<https://cdn.kastatic.org/ka-perseus-images/4054da358c8ceddef75ccf33cd9c6ae47367b003.svg>

Gaussian Beams – TEM Solutions

TEM Approximation:

$$\vec{E}(x, y, z) = \hat{t}E_0\psi(x, y, z) \exp(-jkz)$$

Helmholtz Scalar Equation

$$\nabla^2 E + k_0^2 n^2 E = 0 \qquad \nabla_t^2 \psi - j2k \frac{\partial \psi}{\partial z} + \frac{\partial^2 \psi}{\partial z^2} = 0$$

Paraxial Wave Equation

$$\nabla_t^2 \psi - j2k \frac{\partial \psi}{\partial z} \simeq 0, \quad \text{if} \quad \left| \frac{\partial^2 \psi}{\partial z^2} \right| \ll 2k \left| \frac{\partial \psi}{\partial z} \right|$$

Fundamental TEM Solution

$$\frac{1}{r_T} \frac{\partial}{\partial r_T} \left(r_T \frac{\partial \psi}{\partial r_T} \right) - j2k \frac{\partial \psi}{\partial z} = 0. \qquad \psi = \exp \left\{ -j \left[P(z) + \frac{kr_T^2}{2q(z)} \right] \right\}$$

Gaussian Beams – TEM Solutions

Fundamental TEM Solution

$$\left\{ \left[\frac{k^2}{q^2(z)} (q'(z) - 1) \right] r_T^2 - 2k \left[P'(z) + \frac{j}{q(z)} \right] r_T^0 \right\} \psi = 0, \quad \forall r_T$$

$$\frac{dq}{dz} = q'(z) = 1,$$
$$\frac{dP}{dz} = P'(z) = -\frac{j}{q(z)}.$$

$$q(z) = z + jz_0$$

$$|\psi(r_T, z = 0)|^2 = \exp(-kr_T^2/z_0)$$

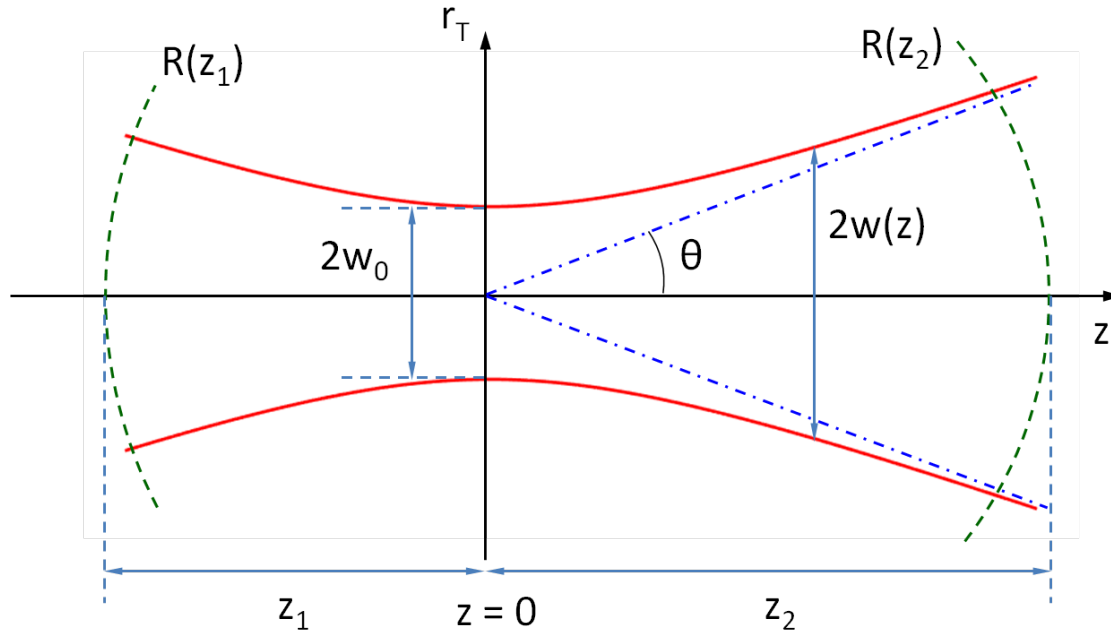
Minimum Beam Waist and Rayleigh Distance

$$w_0^2 = \frac{2z_0}{k} = \frac{\lambda_0 z_0}{n\pi} \implies z_0 = \frac{\pi n w_0^2}{\lambda_0}$$

$$\psi = \exp \left\{ -j \left[P(z) + \frac{kr_T^2}{2q(z)} \right] \right\}$$

$$jP(z) = \ln \left[1 - j \left(\frac{z}{z_0} \right) \right] = \ln \left[1 + \left(\frac{z}{z_0} \right)^2 \right]^{1/2} - j \tan^{-1} \left(\frac{z}{z_0} \right)$$

Gaussian Beams



$$E_{00}(r_T, z) = E_0 \underbrace{\frac{w_0}{w(z)} \exp\left[-\frac{r_T^2}{w^2(z)}\right]}_{\text{amplitude factor}} \underbrace{\exp\left\{-j\left[kz - \tan^{-1}\left(\frac{z}{z_0}\right)\right]\right\}}_{\text{longitudinal phase}} \underbrace{\exp\left[-j\frac{kr_T^2}{2R(z)}\right]}_{\text{radial phase}}$$

$$\frac{1}{q(z)} = \frac{z}{z^2 + z_0^2} - j\frac{z_0}{z^2 + z_0^2} = \frac{1}{R(z)} - j\frac{\lambda_0}{\pi n w^2(z)},$$

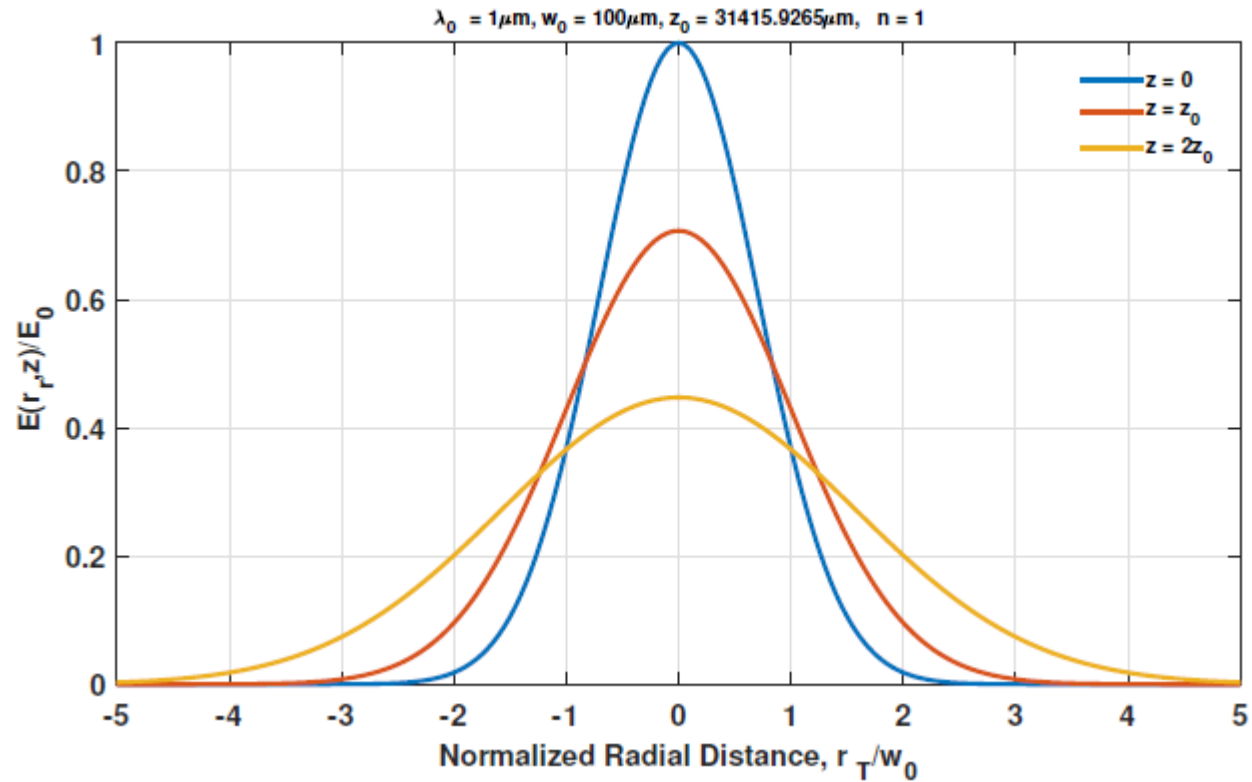
$$z_0 = \frac{\pi n w_0^2}{\lambda_0}$$

$$w^2(z) = w_0^2 \left[1 + \left(\frac{z}{z_0}\right)^2\right],$$

$$R(z) = z \left[1 + \left(\frac{z_0}{z}\right)^2\right].$$

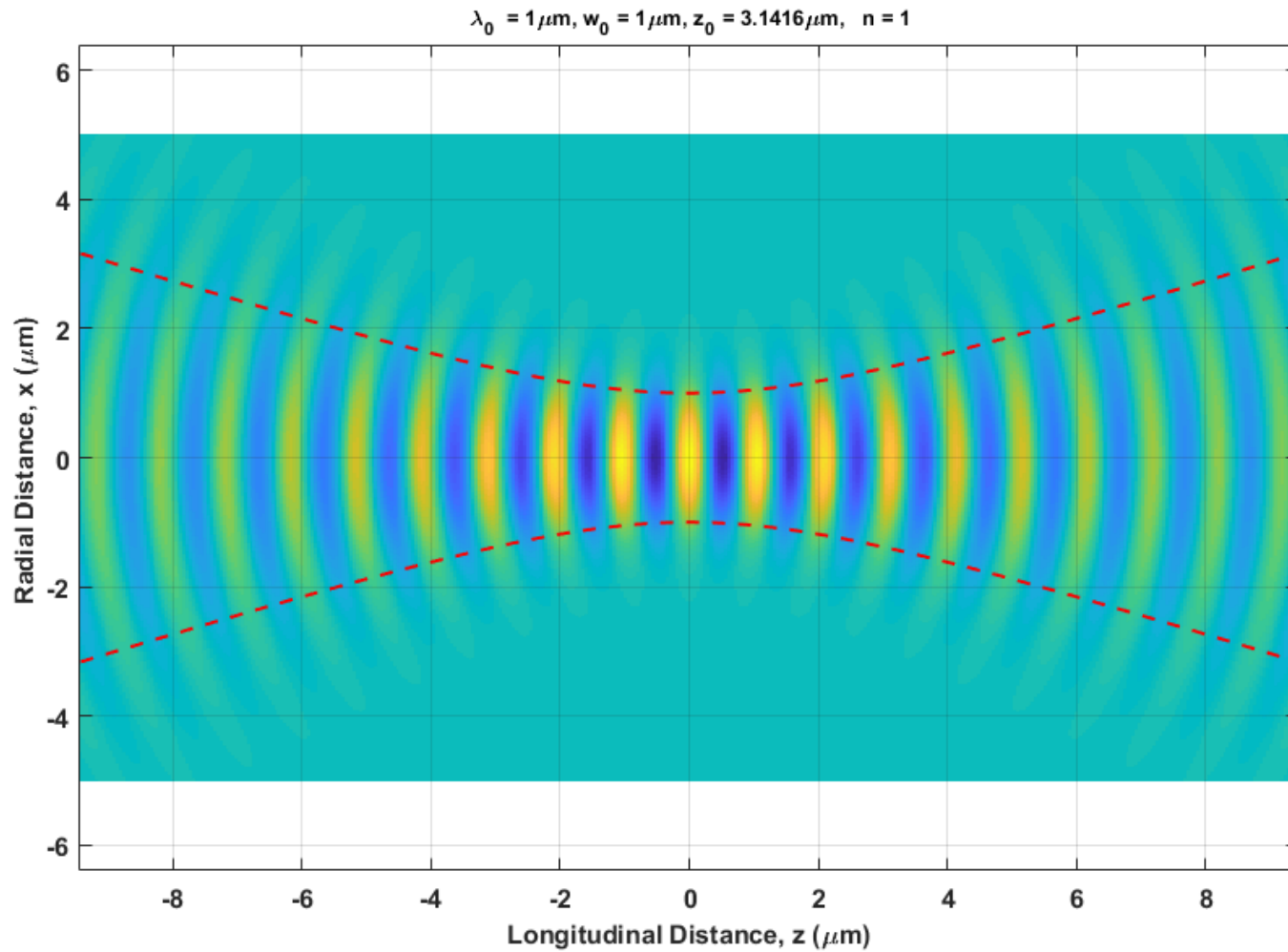
Gaussian Beams

Radial Profiles at various z Distances from Focal Plane



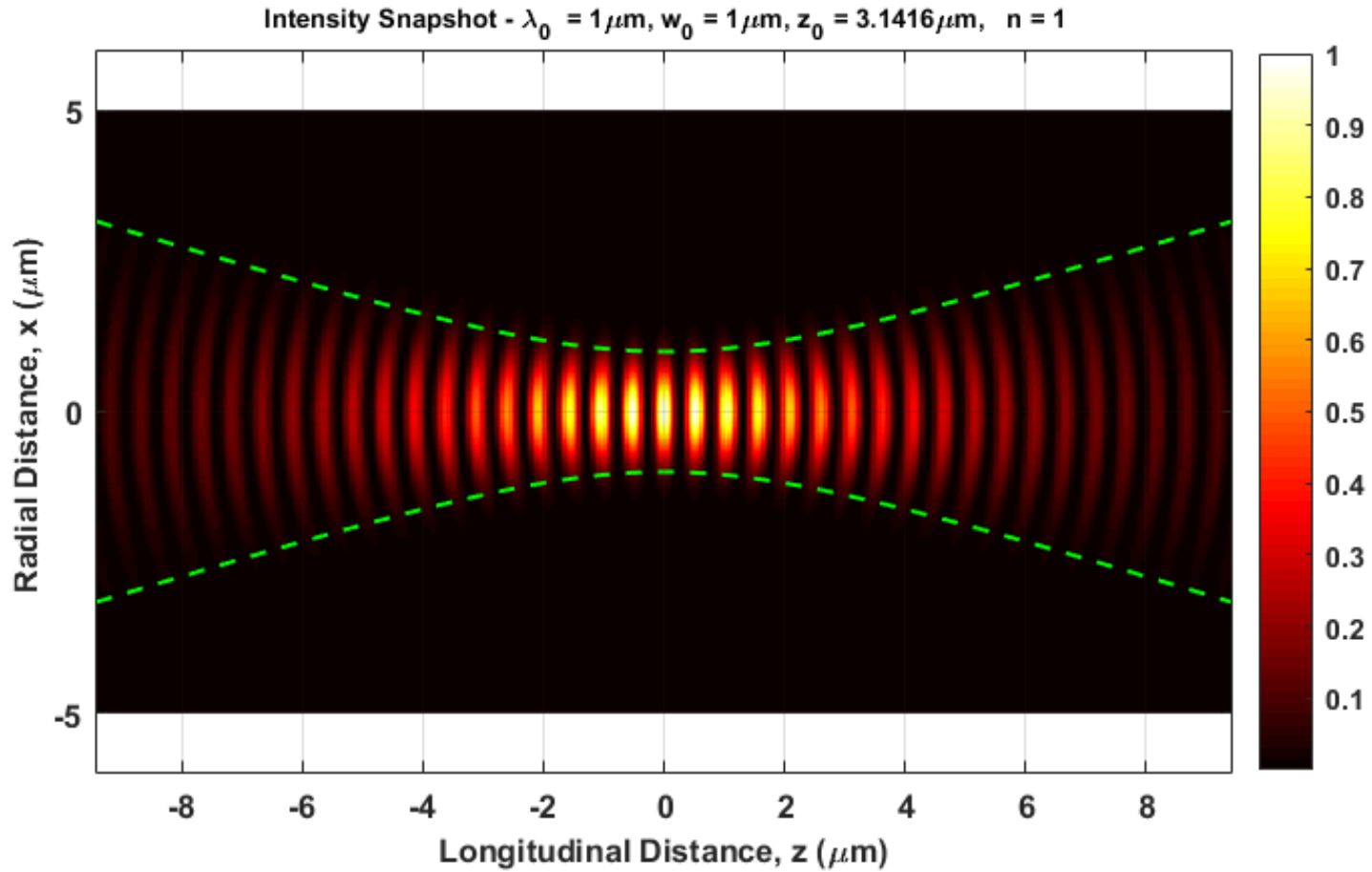
Gaussian Beams

Electric Field Snapshot in Time



Gaussian Beams

Intensity Snapshot in Time



Gaussian Beams

Gaussian Beam Divergence

$$w(z) \simeq \frac{w_0 z}{z_0} = \frac{\lambda_0 z}{\pi n w_0},$$

$$\tan \theta = \frac{dw(z)}{dz} = \frac{\lambda_0}{\pi n w_0} \implies \Delta\theta = 2\theta \simeq \frac{2\lambda_0}{\pi n w_0} = \frac{4}{\pi} \frac{\lambda_0/n}{D_0}$$

Gaussian Beam Power

$$P(z) = \frac{1}{2\eta} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} |E_{00}|^2 dx dy = \frac{1}{2\eta} \int_{-\infty}^{+\infty} \int_0^{2\pi} |E_{00}(r_T, z)|^2 r_T dr_T d\phi = \frac{1}{2\eta} |\mathcal{E}_0|^2 \left[\frac{\pi w_0^2}{2} \right]$$

Gaussian Beams

Gaussian Beam Radius of Curvature

Spherical Wave

$$E_{sph} = \frac{1}{r} \exp(-jkr), \quad \text{where}$$

$$r = \sqrt{x^2 + y^2 + z^2} = \sqrt{r_T^2 + z^2} = z \sqrt{1 + \frac{r_T^2}{z^2}}$$

$$r \simeq z + \frac{1}{2} \frac{r_T^2}{z} \simeq z + \frac{1}{2} \frac{r_T^2}{r}, \quad \text{and}$$

$$E_{sph} \simeq \frac{1}{r} \exp(-jkz) \exp\left(-j \frac{kr_T^2}{2r}\right).$$

Fundamental Gaussian Beam

$$E_{00}(r_T, z) = E_0 \underbrace{\frac{w_0}{w(z)} \exp\left[-\frac{r_T^2}{w^2(z)}\right]}_{\text{amplitude factor}} \underbrace{\exp\left\{-j \left[kz - \tan^{-1}\left(\frac{z}{z_0}\right) \right]\right\}}_{\text{longitudinal phase}} \underbrace{\exp\left[-j \frac{kr_T^2}{2R(z)}\right]}_{\text{radial phase}}$$

Gaussian Beams

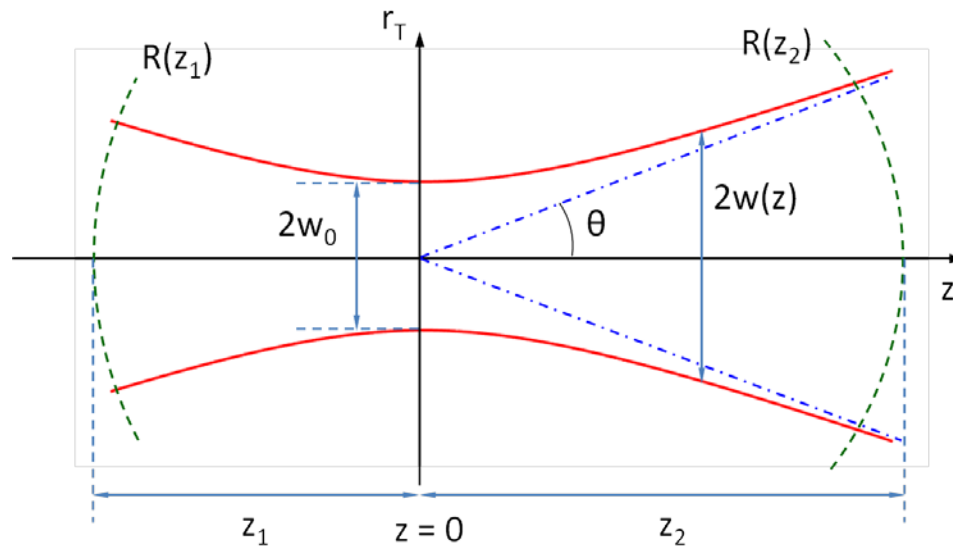
Fundamental Gaussian Beam

$$E_{00}(r_T, z) = E_0 \underbrace{\frac{w_0}{w(z)} \exp\left[-\frac{r_T^2}{w^2(z)}\right]}_{\text{amplitude factor}} \underbrace{\exp\left\{-j\left[kz - \tan^{-1}\left(\frac{z}{z_0}\right)\right]\right\}}_{\text{longitudinal phase}} \underbrace{\exp\left[-j\frac{kr_T^2}{2R(z)}\right]}_{\text{radial phase}}$$

Gaussian Beam Radius of Curvature

$$R(z) = z \left[1 + \left(\frac{z_0}{z}\right)^2 \right]$$

$$R(z) \simeq \begin{cases} +\infty, & \text{centered at } z_c = \mp\infty, & \text{for } |z| \ll z_0, \\ \mp 2z_0, & \text{centered at } z_c = \mp z_0 & \text{for } |z| = z_0, \\ z, & \text{centered at } z_c = 0, & \text{for } |z| \gg z_0. \end{cases}$$



Gaussian Beams

Gaussian Beam Radius of Curvature

$$R(z) \simeq \begin{cases} +\infty, & \text{centered at } z_c = \mp\infty, \text{ for } |z| \ll z_0, \\ \mp 2z_0, & \text{centered at } z_c = \mp z_0 \text{ for } |z| = z_0, \\ z, & \text{centered at } z_c = 0, \text{ for } |z| \gg z_0. \end{cases}$$

Gaussian Beam Longitudinal Phase Shift – *Gouy's* Shift

$$E_{00}(r_T, z) = E_0 \underbrace{\frac{w_0}{w(z)} \exp\left[-\frac{r_T^2}{w^2(z)}\right]}_{\text{amplitude factor}} \underbrace{\exp\left\{-j\left[kz - \tan^{-1}\left(\frac{z}{z_0}\right)\right]\right\}}_{\text{longitudinal phase}} \underbrace{\exp\left[-j\frac{kr_T^2}{2R(z)}\right]}_{\text{radial phase}}$$

$$\Phi(z) = kz - \tan^{-1}(z/z_0)$$

Phase Velocity (exact)

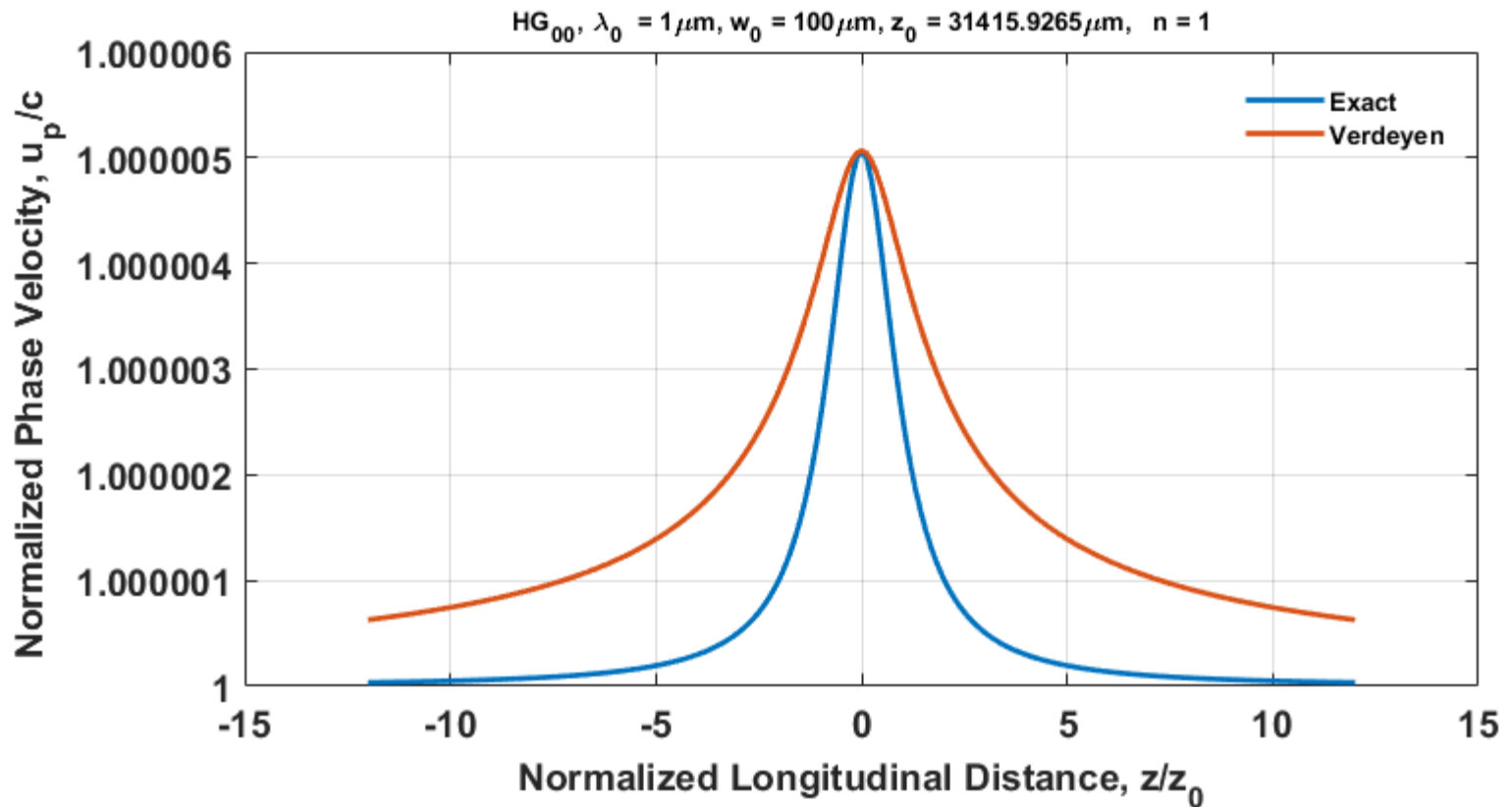
$$u_p = \frac{\omega}{d\Phi/dz} = \frac{\frac{c}{n}}{1 - \frac{\lambda_0 z_0}{2\pi n} \frac{1}{z^2 + z_0^2}}$$

Phase Velocity (approximate)

$$u_p = \frac{\omega}{\Phi/z} = \frac{\frac{c}{n}}{1 - \frac{\lambda_0}{2\pi n z} \tan^{-1}\left(\frac{z}{z_0}\right)}$$

Gaussian Beams

Gaussian Beam Longitudinal Phase Shift – *Gouy's* Shift



Hermite-Gaussian Beams

$$E_{mp}(x, y, z) = E_{mp}^{HG} H_m \left(\frac{\sqrt{2}x}{w(z)} \right) H_p \left(\frac{\sqrt{2}y}{w(z)} \right) \frac{w_0}{w(z)} \exp \left[-\frac{x^2 + y^2}{w^2(z)} \right] \exp \left\{ -j \left[kz - (1 + m + p) \tan^{-1} \left(\frac{z}{z_0} \right) \right] \right\} \exp \left[-j \frac{k(x^2 + y^2)}{2R(z)} \right]$$

where,

$$w^2(z) = w_0^2 \left(1 + \frac{z^2}{z_0^2} \right),$$

$$R(z) = z \left(1 + \frac{z_0^2}{z^2} \right),$$

$$H_m(u) = (-1)^m e^{u^2} \frac{d^m}{du^m} \left(e^{-u^2} \right),$$

$$H_{m+1}(u) = 2uH_m(u) - 2mH_{m-1}(u), \quad \text{with } H_0(u) = 1 \quad \text{and} \quad H_1(u) = u,$$

Some *Hermite* Polynomials

$$H_0(x) = 1$$

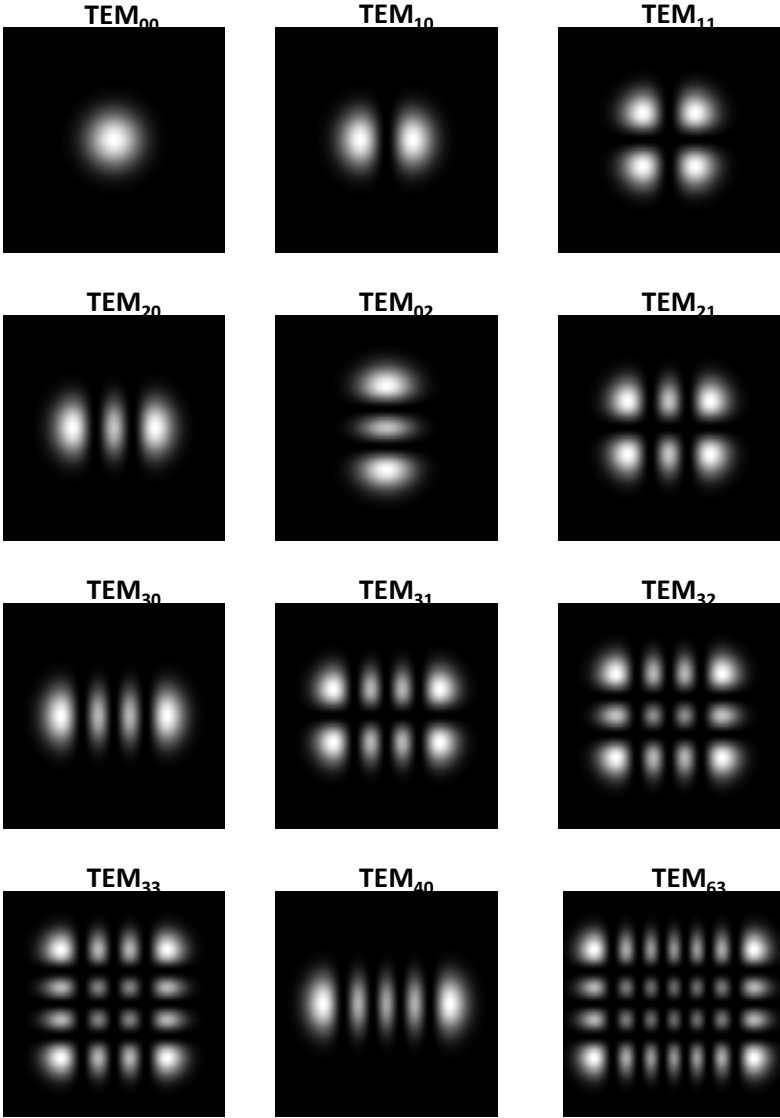
$$H_1(x) = 2x$$

$$H_2(x) = 4x^2 - 2$$

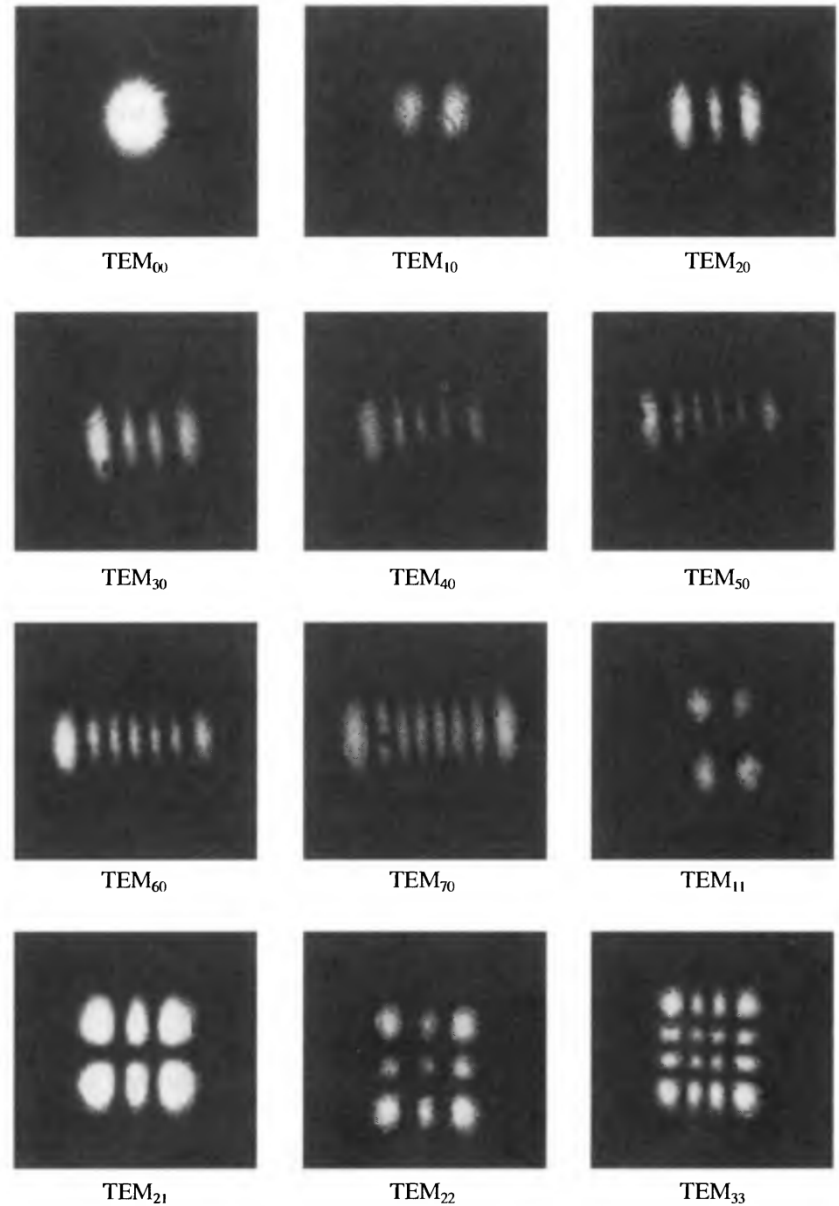
$$H_3(x) = 8x^3 - 12x$$

$$H_4(x) = 16x^4 - 48x^2 + 12$$

Hermite-Gaussian Beams Patterns



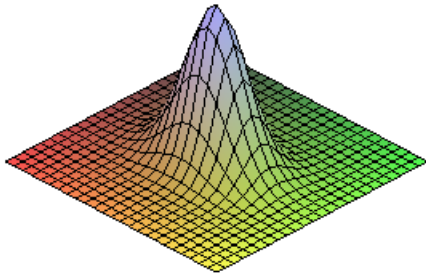
Experimental Patterns of Gaussian Beams



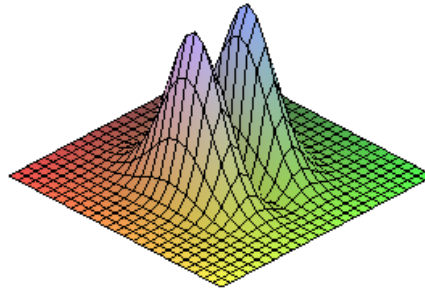
From A. Yariv and P. Yeh, "Photonics" 6th Ed. Oxford University Press, 2007

Hermite-Gaussian Beams Patterns

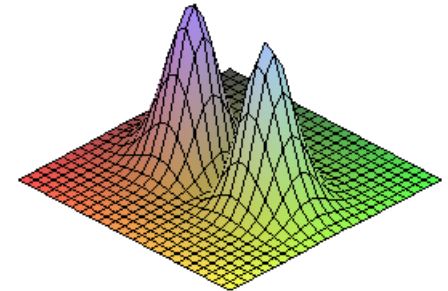
TEM₀₀



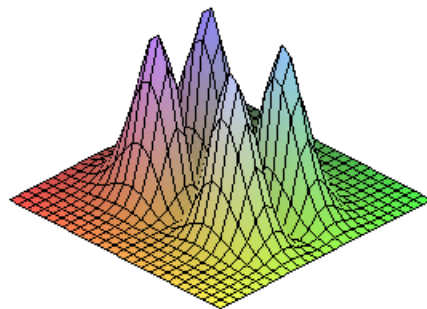
TEM₁₀



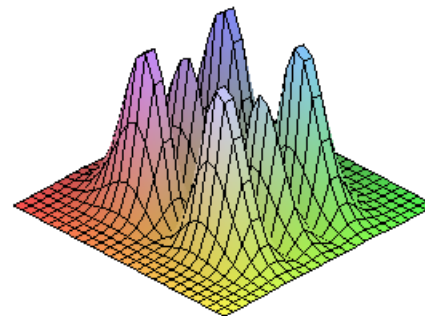
TEM₀₁



TEM₁₁



TEM₂₁



Laguerre-Gaussian Beams

$$E_{pm}(r_T, \phi, z) = E_{pm}^{LG} \frac{w_0}{w(z)} \left(\frac{\sqrt{2}r_T}{w(z)} \right)^{|m|} L_p^{|m|} \left(\frac{2r_T^2}{w^2(z)} \right) \exp \left[-\frac{r_T^2}{w^2(z)} \right] \\ \exp \left\{ -j \left[kz - (1 + |m| + 2p) \tan^{-1} \left(\frac{z}{z_0} \right) \right] \right\} \exp(jm\phi) \exp \left[-j \frac{kr_T^2}{2R(z)} \right]$$

where,

$$w^2(z) = w_0^2 \left(1 + \frac{z^2}{z_0^2} \right),$$

$$R(z) = z \left(1 + \frac{z_0^2}{z^2} \right),$$

$$L_p^m(u) = \frac{e^u}{p!} u^{-m} \frac{d^p}{du^p} (e^{-u} u^{p+m}),$$

$$(k+1)L_{k+1}^p(u) = (2k+1+p-u)L_k^p(u) - (k+p)L_{k-1}^p(u), \quad \text{with}$$

$$L_0^m(u) = 1 \quad \text{and} \quad L_1^m(u) = -u + (m+1),$$

Some Laguerre Polynomials

$$L_0^m(x) = 1$$

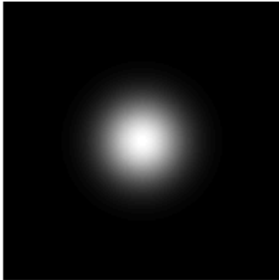
$$L_1^m(x) = -x + (m+1)$$

$$L_2^m(x) = \frac{1}{2}[x^2 - 2(m+2)x + (m+1)(m+2)]$$

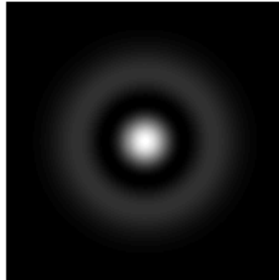
$$L_3^m(x) = \frac{1}{6}[-x^3 + 3(m+3)x^2 - 3(m+2)(m+3)x + (m+1)(m+2)(m+3)]$$

Laguerre-Gaussian Beams Patterns

TEM(0,0) - $\cos(m\phi)$



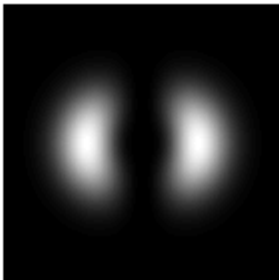
TEM(1,0) - $\cos(m\phi)$



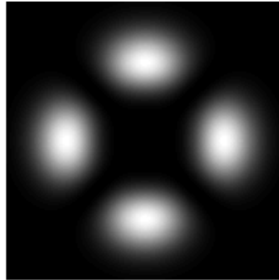
TEM(2,0) - $\cos(m\phi)$



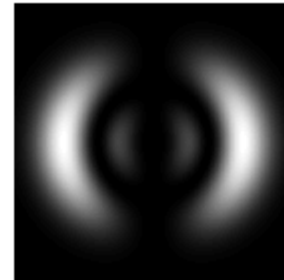
TEM(0,1) - $\cos(m\phi)$



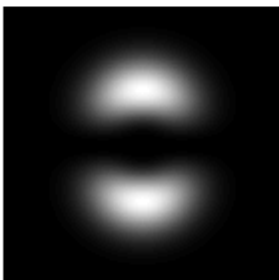
TEM(0,2) - $\cos(m\phi)$



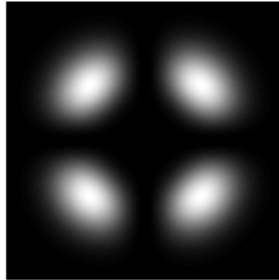
TEM(1,1) - $\cos(m\phi)$



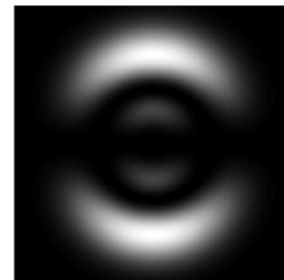
TEM(0,1) - $\sin(m\phi)$



TEM(0,2) - $\sin(m\phi)$



TEM(1,1) - $\sin(m\phi)$



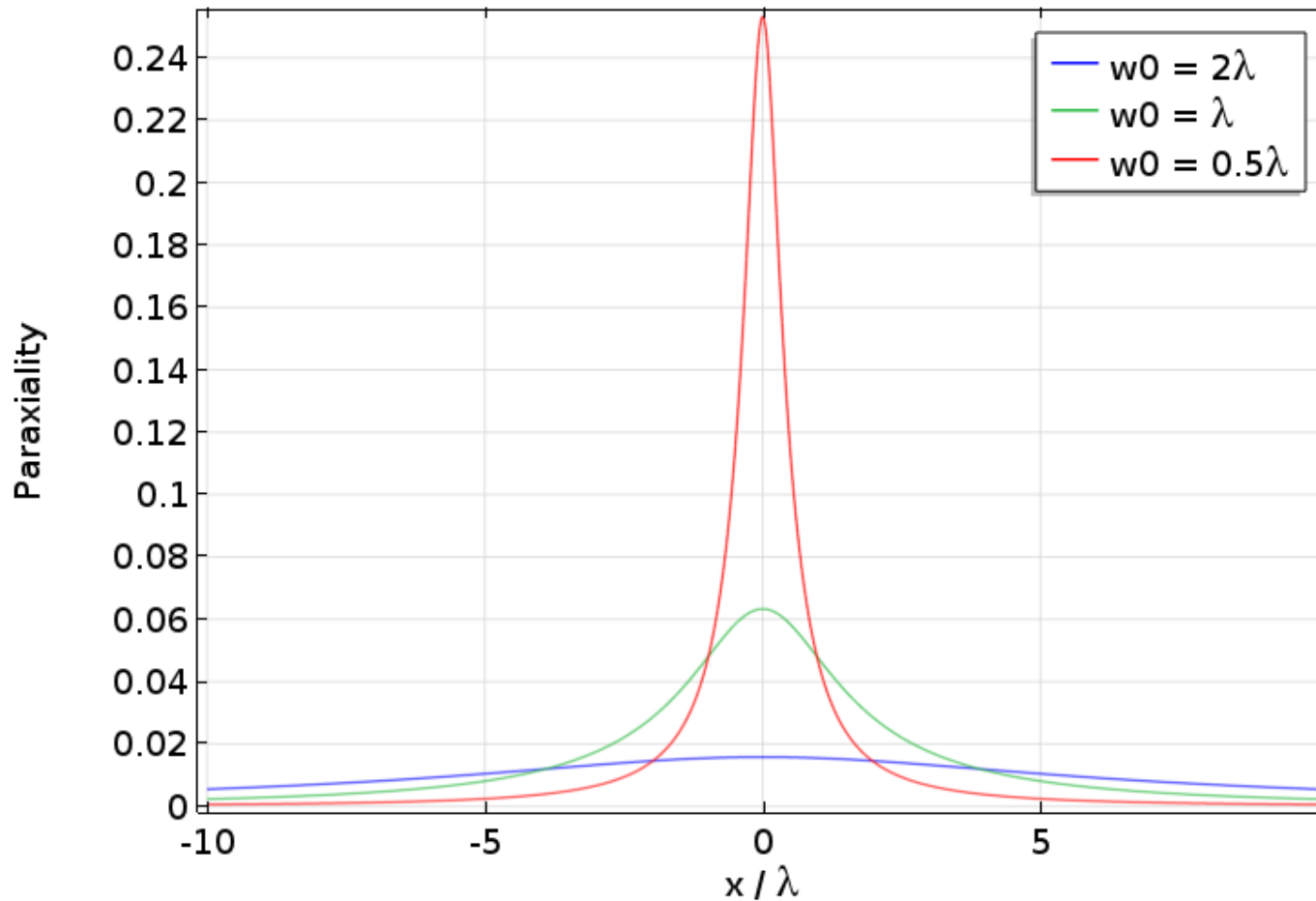
Validity of Paraxial Approximation

$$\mathcal{P} = 1 - \frac{N + 1}{k_0^2 n^2 w_0^2}, \quad \text{where}$$
$$N = m + p, \quad \text{for Hermite-Gaussian beams,}$$
$$N = 2p + |m|, \quad \text{for Laguerre-Gaussian beams.}$$

$\mathcal{P} \simeq 1$ (the closer to 1 the better the paraxial approximation)

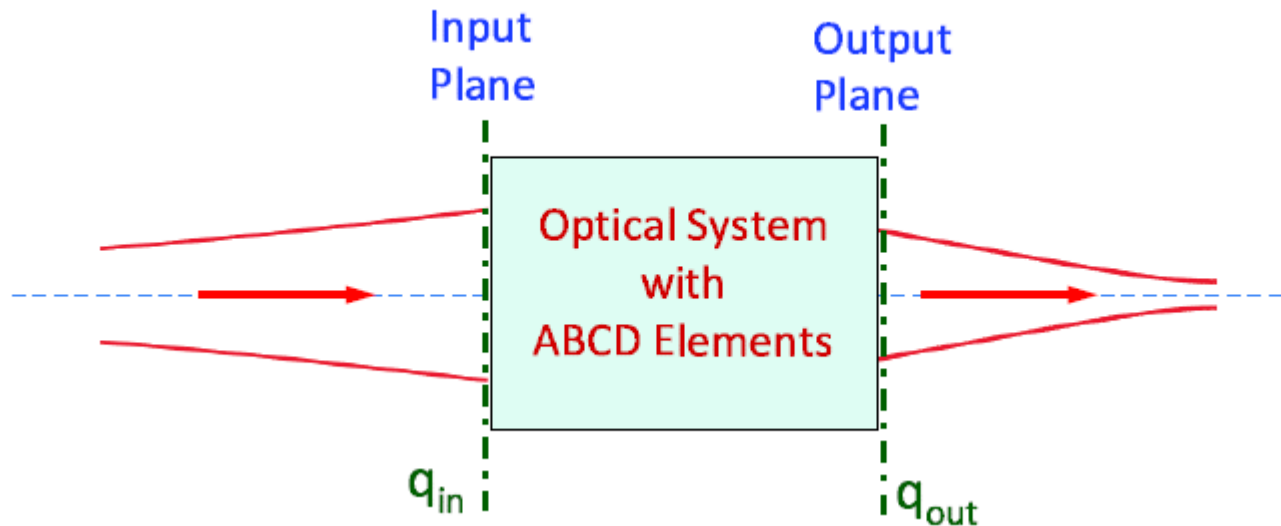
Validity of Paraxial Approximation

$$\text{Paraxiality} = \left| \frac{\frac{\partial^2 \psi}{\partial z^2}}{2jk \frac{\partial \psi}{\partial z}} \right|$$



<https://www.comsol.com/blogs/understanding-the-paraxial-gaussian-beam-formula/>

Gaussian Beams and ABCD Law

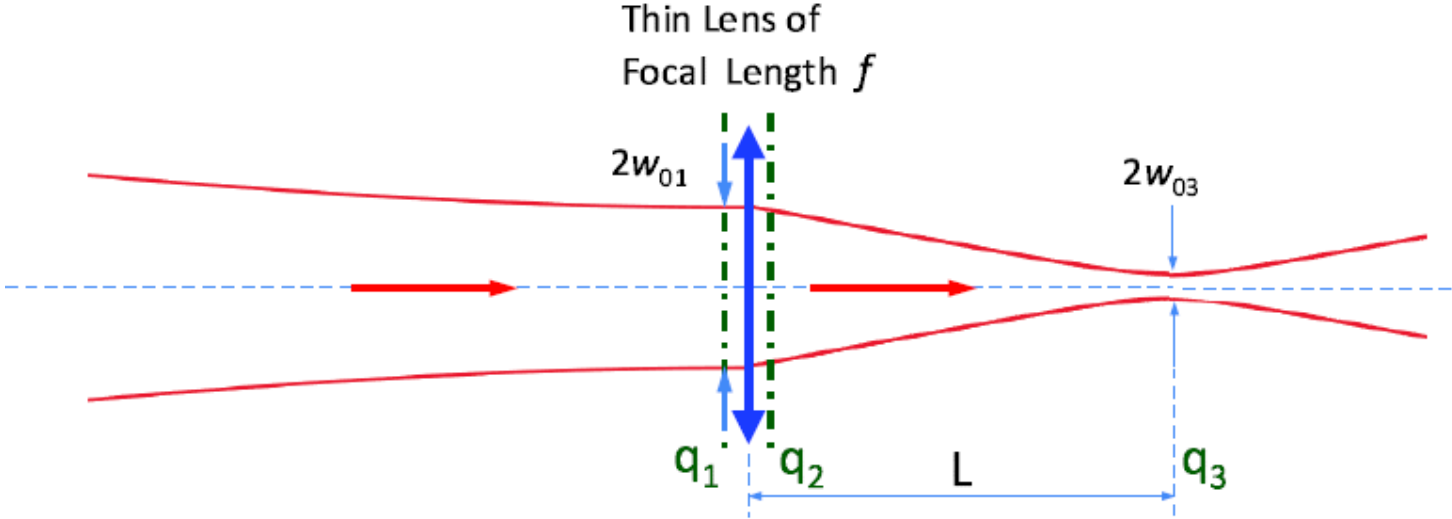
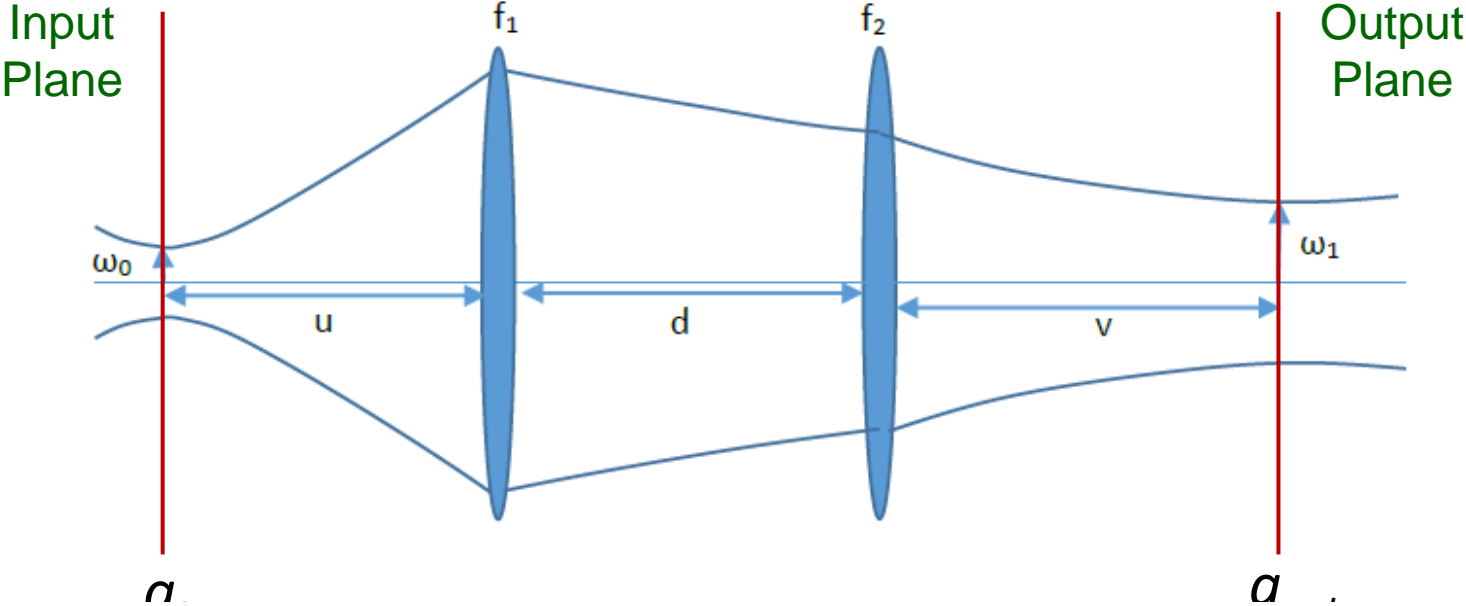


$$q_{out} = \frac{Aq_{in} + B}{Cq_{in} + D}$$

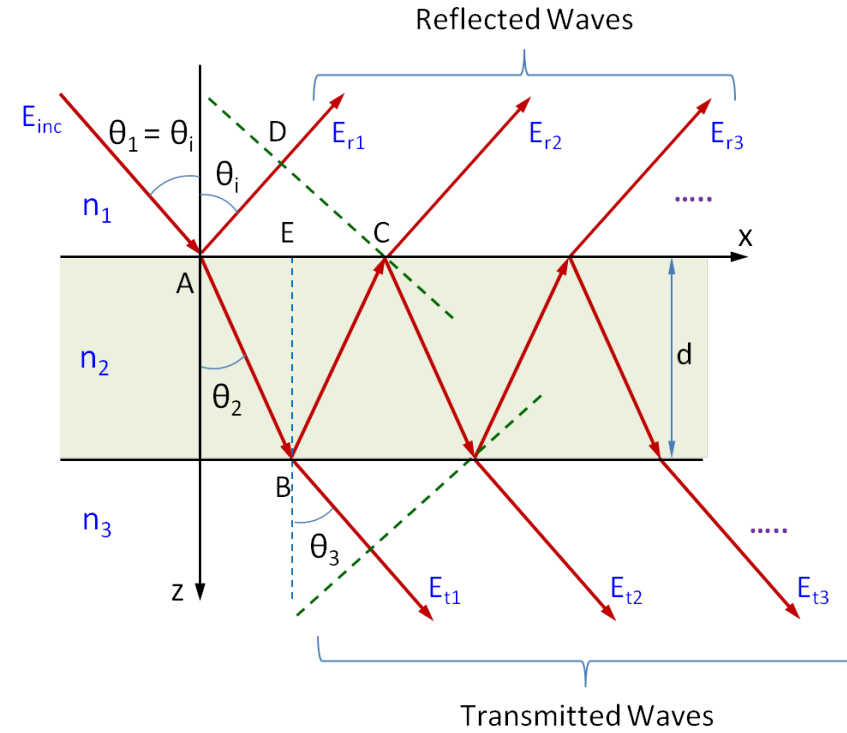
$$\frac{1}{q_{out}} = \frac{C + D(1/q_{in})}{A + B(1/q_{in})}$$

$$\frac{1}{q(z)} = \frac{z}{z^2 + z_0^2} - j \frac{z_0}{z^2 + z_0^2} = \frac{1}{R(z)} - j \frac{\lambda_0}{\pi n \omega^2(z)}$$

Gaussian Beams and ABCD Law Examples



Fabry-Perot Interferometer



$$\delta = k_0 n_2 [(AB) + (BC)] - k_0 n_1 (AD), \quad \text{where,}$$

$$(AB) = (BC) = \frac{d}{\cos \theta_2},$$

$$(AD) = (AC) \sin \theta_1 = 2(AE) \sin \theta_1 = 2d \tan \theta_2 \sin \theta_1,$$

$$\delta = 2k_0 n_2 d \cos \theta_2,$$

Reflected Waves

$$E_{r1} = r_{12} E_i,$$

$$E_{r2} = t_{12} t_{21} r_{23} e^{-j\delta} E_i,$$

$$E_{r3} = t_{12} t_{21} r_{21} r_{23}^2 e^{-j2\delta} E_i,$$

$$\vdots = \vdots,$$

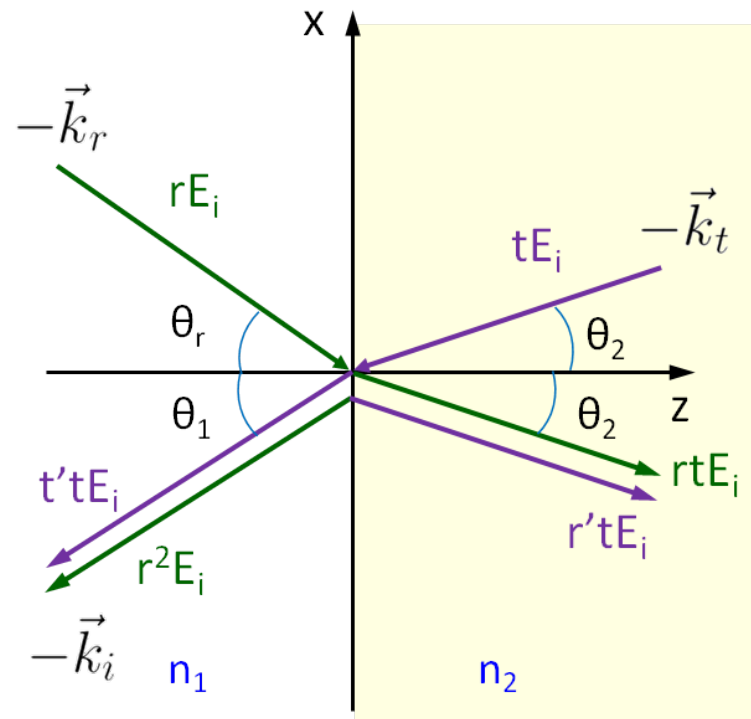
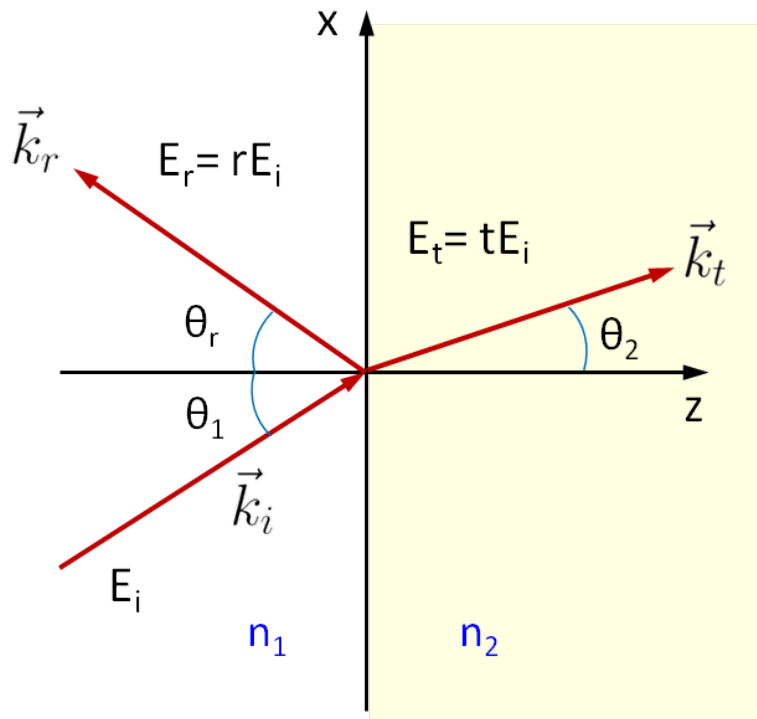
$$E_{rN} = t_{12} t_{21} r_{21}^{N-2} r_{23}^{N-1} e^{-j(N-1)\delta} E_i,$$

$$\vdots = \vdots.$$

$$\begin{aligned} E_r &= \sum_{m=1}^{\infty} E_{rm} = r_{12} E_i + t_{12} t_{21} r_{23} e^{-j\delta} E_i \left[1 + r_{21} r_{23} e^{-j\delta} + r_{21}^2 r_{23}^2 e^{-j2\delta} + \dots \right] = \\ &= r_{12} E_i + t_{12} t_{21} r_{23} e^{-j\delta} E_i \frac{1}{1 - r_{21} r_{23} e^{-j\delta}} = r_{12} E_i - (1 - r_{12}^2) E_i \frac{r_{32} e^{-j\delta}}{1 - r_{12} r_{32} e^{-j\delta}} \end{aligned}$$

$$\frac{E_r}{E_i} = \frac{r_{12} - r_{32} e^{-j\delta}}{1 - r_{12} r_{32} e^{-j\delta}}.$$

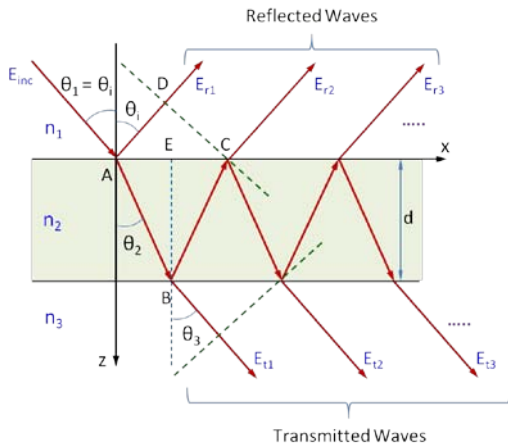
Stokes Relations



$$rt + r't = 0 \implies r' = -r,$$

$$tt' + r^2 = 1.$$

Fabry-Perot Interferometer



Transmitted Waves

$$E_t = \sum_{m=1}^{\infty} E_{tm} = t_{12}t_{23}E_i \left[1 + r_{21}r_{23}e^{-j\delta} + r_{21}^2r_{23}^2e^{-j2\delta} + \dots \right]$$

$$\frac{E_t}{E_i} = \frac{t_{12}t_{23}}{1 - r_{12}r_{32}e^{-j\delta}}$$

$$\begin{aligned} \frac{I_r}{I_i} = \frac{P_r}{P_i} = \frac{|E_r|^2}{|E_i|^2} &= \frac{|r_{12}|^2 + |r_{32}|^2 - 2|r_{12}||r_{32}|\cos\delta}{1 + |r_{12}|^2|r_{32}|^2 - 2|r_{12}||r_{32}|\cos\delta} = \\ &= \frac{(|r_{12}| - |r_{32}|)^2 + 4|r_{12}||r_{32}|\sin^2(\delta/2)}{(1 - |r_{12}||r_{32}|)^2 + 4|r_{12}||r_{32}|\sin^2(\delta/2)} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2 + 4\sqrt{R_1R_2}\sin^2(\delta/2)}{(1 - \sqrt{R_1R_2})^2 + 4\sqrt{R_1R_2}\sin^2(\delta/2)}, \end{aligned}$$

$$\frac{I_t}{I_i} = \frac{P_t}{P_i} = \frac{n_3 \cos\theta_3 |E_t|^2}{n_1 \cos\theta_1 |E_i|^2} = \frac{|t_{12}|^2 |t_{23}|^2}{1 + |r_{12}|^2|r_{32}|^2 - 2|r_{12}||r_{32}|\cos\delta},$$

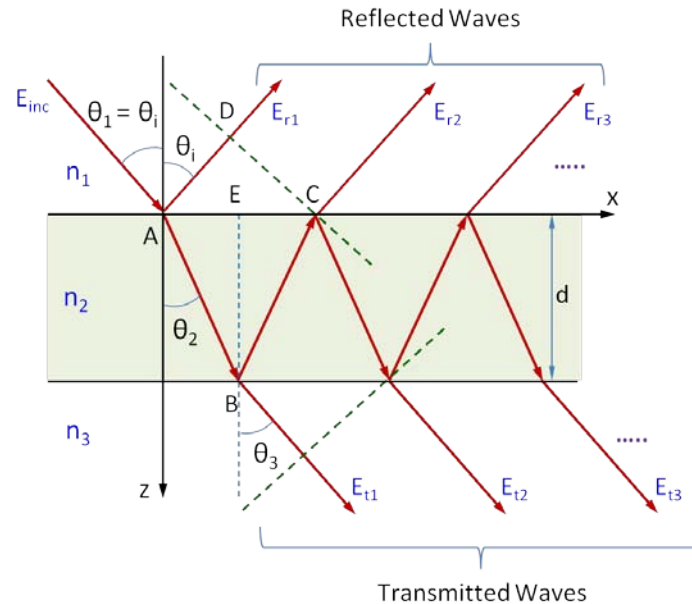
using Eqs. (118) or (119)

$$|t_{12}|^2 = \frac{n_1 \cos\theta_1}{n_2 \cos\theta_2} (1 - |r_{12}|^2),$$

$$|t_{23}|^2 = \frac{n_2 \cos\theta_2}{n_3 \cos\theta_3} (1 - |r_{32}|^2), \quad \text{results in,}$$

$$\begin{aligned} \frac{I_t}{I_i} &= \frac{(1 - |r_{12}|^2)(1 - |r_{32}|^2)}{1 + |r_{12}|^2|r_{32}|^2 - 2|r_{12}||r_{32}|\cos\delta} = \\ &= \frac{(1 - |r_{12}|^2)(1 - |r_{32}|^2)}{(1 - |r_{12}||r_{32}|)^2 + 4|r_{12}||r_{32}|\sin^2(\delta/2)} = \frac{(1 - R_1)(1 - R_2)}{(1 - \sqrt{R_1R_2})^2 + 4\sqrt{R_1R_2}\sin^2(\delta/2)} \end{aligned}$$

Fabry-Perot Interferometer



$$R_1 = |r_{12}|^2 \text{ and } R_2 = |r_{32}|^2$$

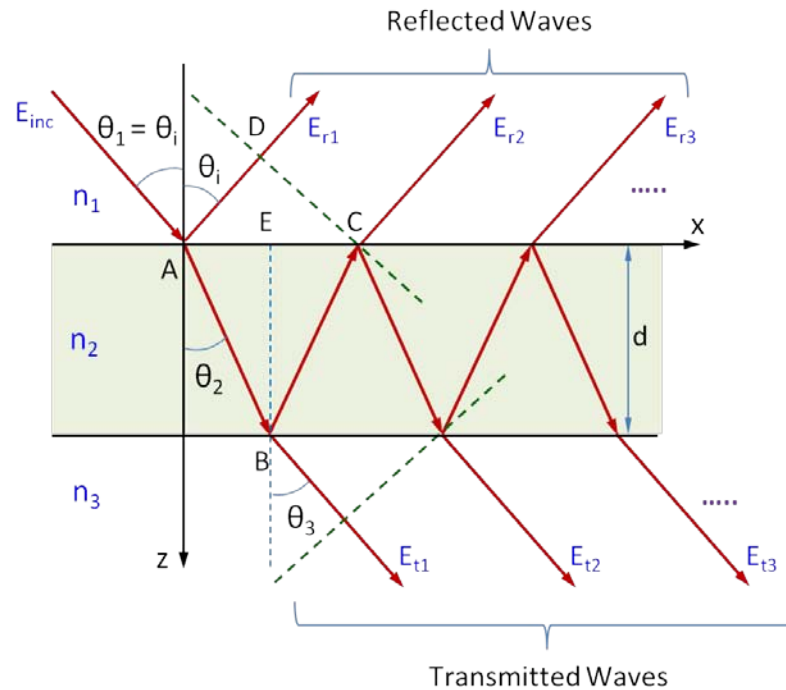
$$\left(\frac{I_t}{I_i}\right)_{max} = \frac{(1 - R_1)(1 - R_2)}{(1 - \sqrt{R_1 R_2})^2}, \quad \text{for } \delta = 2m\pi,$$

$$\left(\frac{I_t}{I_i}\right)_{min} = \frac{(1 - R_1)(1 - R_2)}{(1 + \sqrt{R_1 R_2})^2}, \quad \text{for } \delta = (2m + 1)\pi,$$

$$\left(\frac{I_r}{I_i}\right)_{max} = \frac{(\sqrt{R_1} + \sqrt{R_2})^2}{(1 + \sqrt{R_1 R_2})^2}, \quad \text{for } \delta = (2m + 1)\pi,$$

$$\left(\frac{I_r}{I_i}\right)_{min} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2}{(1 - \sqrt{R_1 R_2})^2}, \quad \text{for } \delta = 2m\pi.$$

Symmetric Fabry-Perot Interferometer



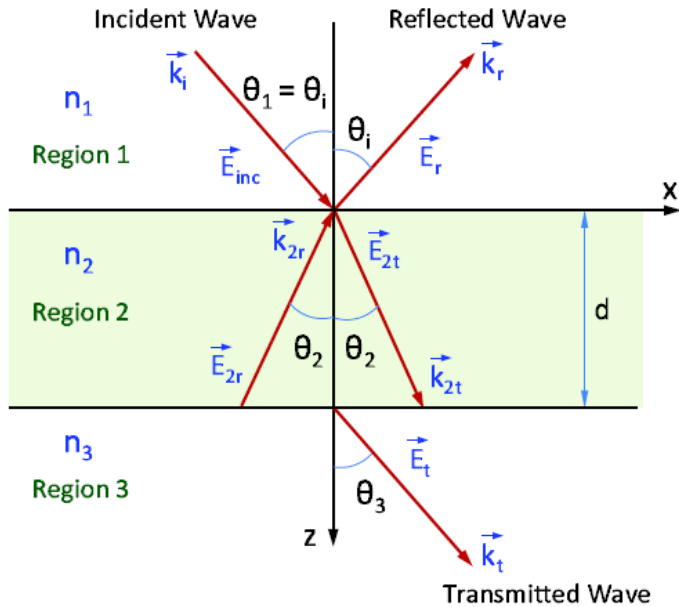
$$n_1 = n_3 = n_0 \text{ and } n_2 = n_f \quad r_{12} = r_{32} = r \quad (\phi_{12} = \phi_{32} = 0) \quad R_1 = R_2 = R = r^2$$

$$\delta = k_0 \Delta, \quad \Delta = 2dn_2 \cos \theta_2, \quad R = r^2$$

$$\frac{I_t}{I_i} = \frac{(1 - r^2)^2}{1 + r^4 - 2r^2 \cos \delta} = \frac{(1 - R)^2}{(1 - R)^2 + 4R \sin^2(\delta/2)}$$

$$\frac{I_r}{I_i} = \frac{2r^2(1 - \cos \delta)}{1 + r^4 - 2r^2 \cos \delta} = \frac{4R \sin^2(\delta/2)}{(1 - R)^2 + 4R \sin^2(\delta/2)}$$

Electromagnetic Analysis of Fabry-Perot Interferometer



$$\vec{E}_1 = \vec{E}_i + \vec{E}_r = \hat{y} \left[E_i e^{-j\vec{k}_i \cdot \vec{r}} + E_r e^{-j\vec{k}_r \cdot \vec{r}} \right], \quad \text{where}$$

$$\vec{k}_i = k_0 n_1 (\hat{i}_x \sin \theta_1 + \hat{i}_z \cos \theta_1), \quad \vec{k}_r = k_0 n_1 (\hat{i}_x \sin \theta_1 - \hat{i}_z \cos \theta_1),$$

$$\vec{E}_2 = \vec{E}_{2t} + \vec{E}_{2r} = \hat{y} \left[E_{2t} e^{-j\vec{k}_{2t} \cdot \vec{r}} + E_{2r} e^{-j\vec{k}_{2r} \cdot \vec{r}} \right], \quad \text{where}$$

$$\vec{k}_{2t} = k_0 n_2 (\hat{i}_x \sin \theta_2 + \hat{i}_z \cos \theta_2), \quad \vec{k}_{2r} = k_0 n_2 (\hat{i}_x \sin \theta_2 - \hat{i}_z \cos \theta_2),$$

$$\vec{E}_3 = \vec{E}_t = \hat{y} E_t e^{-j\vec{k}_t \cdot (\vec{r} - d\hat{i}_z)}, \quad \text{where}$$

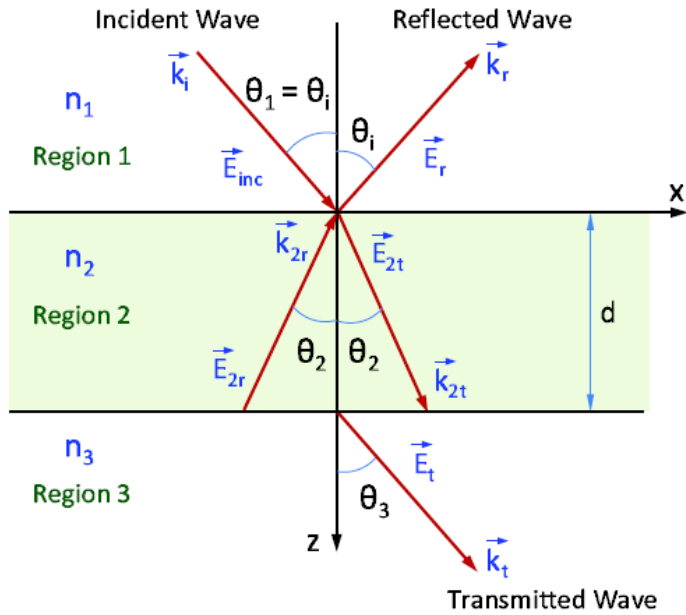
$$\vec{k}_t = k_0 n_3 (\hat{i}_x \sin \theta_3 + \hat{i}_z \cos \theta_3).$$

$$H_{1x} = \frac{1}{Z_1} \left[-E_i \cos \theta_1 e^{-jk_0 n_1 (x \sin \theta_1 + z \cos \theta_1)} + E_r \cos \theta_1 e^{-jk_0 n_1 (x \sin \theta_1 - z \cos \theta_1)} \right],$$

$$H_{2x} = \frac{1}{Z_2} \left[-E_{2t} \cos \theta_2 e^{-jk_0 n_2 (x \sin \theta_2 + z \cos \theta_2)} + E_{2r} \cos \theta_2 e^{-jk_0 n_2 (x \sin \theta_2 - z \cos \theta_2)} \right],$$

$$H_{3x} = -\frac{1}{Z_3} E_t \cos \theta_3 e^{-jk_0 n_3 (x \sin \theta_3 + (z-d) \cos \theta_3)}.$$

Electromagnetic Analysis of Fabry-Perot Interferometer



Οριακές Συνθήκες

$$\beta_2 = k_0 n_2 \cos \theta_2$$

$$\begin{bmatrix} E_{2t} \\ E_{2r} \end{bmatrix} = \underbrace{\begin{bmatrix} \frac{1}{2} \left(1 + \frac{n_1 \cos \theta_1}{n_2 \cos \theta_2} \right) & \frac{1}{2} \left(1 - \frac{n_1 \cos \theta_1}{n_2 \cos \theta_2} \right) \\ \frac{1}{2} \left(1 - \frac{n_1 \cos \theta_1}{n_2 \cos \theta_2} \right) & \frac{1}{2} \left(1 + \frac{n_1 \cos \theta_1}{n_2 \cos \theta_2} \right) \end{bmatrix}}_{\tilde{M}_{2,1}} \begin{bmatrix} E_i \\ E_r \end{bmatrix},$$

$$\begin{bmatrix} E_t \\ 0 \end{bmatrix} = \underbrace{\begin{bmatrix} \frac{1}{2} \left(1 + \frac{n_2 \cos \theta_2}{n_3 \cos \theta_3} \right) e^{-j\beta_2 d} & \frac{1}{2} \left(1 - \frac{n_2 \cos \theta_2}{n_3 \cos \theta_3} \right) e^{+j\beta_2 d} \\ \frac{1}{2} \left(1 - \frac{n_2 \cos \theta_2}{n_3 \cos \theta_3} \right) e^{-j\beta_2 d} & \frac{1}{2} \left(1 + \frac{n_2 \cos \theta_2}{n_3 \cos \theta_3} \right) e^{+j\beta_2 d} \end{bmatrix}}_{\tilde{M}_{3,2}} \begin{bmatrix} E_{2t} \\ E_{2r} \end{bmatrix},$$

$$\begin{bmatrix} E_t \\ 0 \end{bmatrix} = \tilde{M}_{3,2} \tilde{M}_{2,1} \begin{bmatrix} E_i \\ E_r \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} E_i \\ E_r \end{bmatrix} \Rightarrow$$

$$K_{12} = \frac{n_1 \cos \theta_1}{n_2 \cos \theta_2},$$

$$K_{23} = \frac{n_2 \cos \theta_2}{n_3 \cos \theta_3},$$

$$m_{11} = \frac{1}{4} \left[(1 + K_{12})(1 + K_{23})e^{-j\beta_2 d} + (1 - K_{12})(1 - K_{23})e^{+j\beta_2 d} \right],$$

$$m_{12} = \frac{1}{4} \left[(1 - K_{12})(1 + K_{23})e^{-j\beta_2 d} + (1 + K_{12})(1 - K_{23})e^{+j\beta_2 d} \right],$$

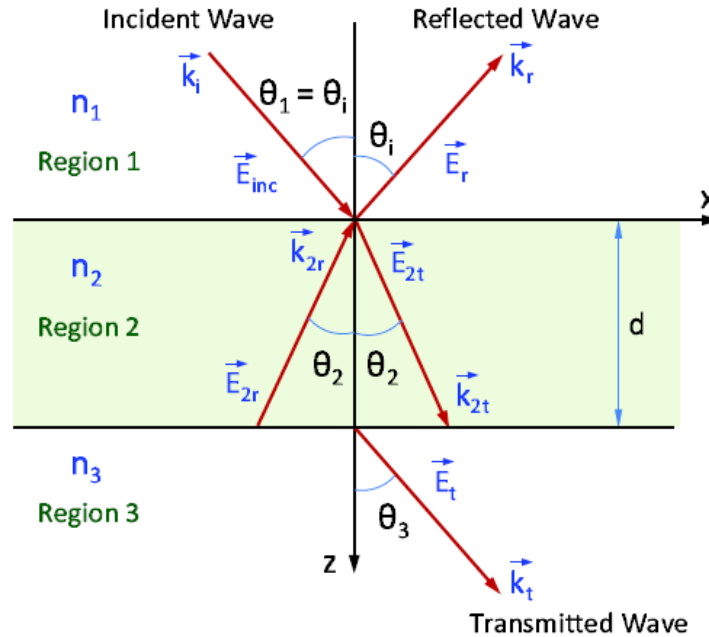
$$m_{21} = \frac{1}{4} \left[(1 + K_{12})(1 - K_{23})e^{-j\beta_2 d} + (1 - K_{12})(1 + K_{23})e^{+j\beta_2 d} \right],$$

$$m_{22} = \frac{1}{4} \left[(1 - K_{12})(1 - K_{23})e^{-j\beta_2 d} + (1 + K_{12})(1 + K_{23})e^{+j\beta_2 d} \right].$$

$$\frac{E_r}{E_i} = r = -\frac{m_{21}}{m_{22}},$$

$$\frac{E_t}{E_i} = t = m_{11} - \frac{m_{12}m_{21}}{m_{22}}, \quad \text{where,}$$

Electromagnetic Analysis of Fabry-Perot Interferometer

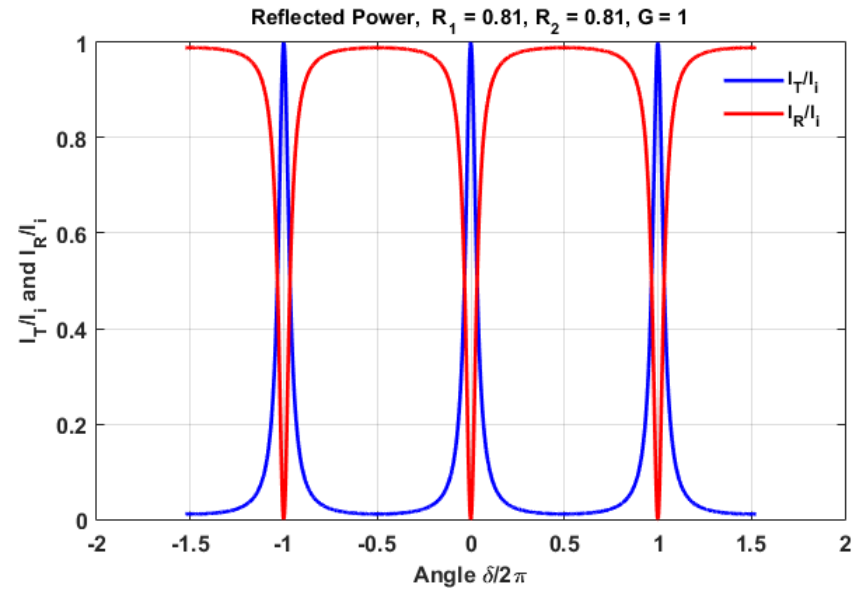
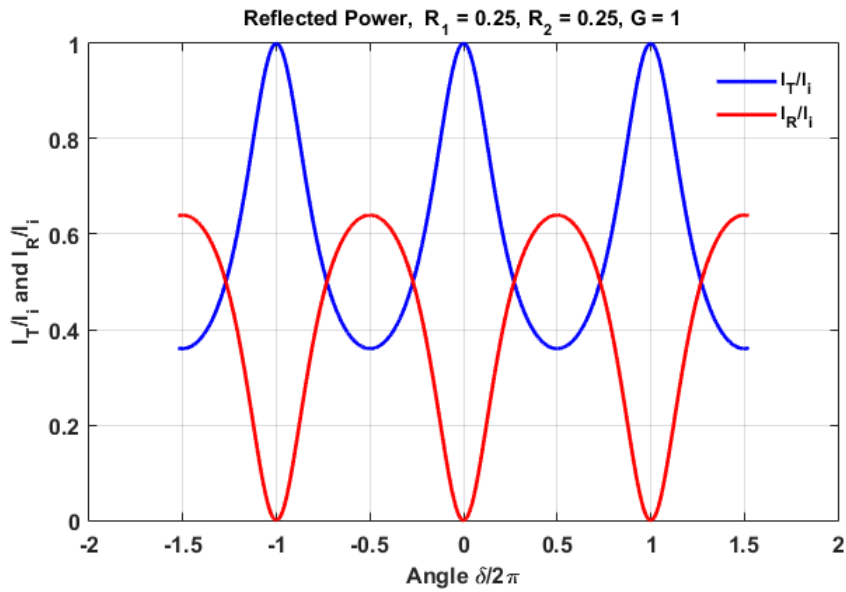


$$\frac{I_r}{I_i} = |r|^2 = \frac{|m_{21}|^2}{|m_{22}|^2},$$

$$\frac{I_t}{I_i} = \frac{n_3 \cos \theta_3}{n_1 \cos \theta_1} |t|^2 = \frac{n_3 \cos \theta_3}{n_1 \cos \theta_1} \left[|m_{11}|^2 + \frac{|m_{12}|^2 |m_{21}|^2}{|m_{22}|^2} - 2 \operatorname{Re} \left\{ \frac{m_{11}^* m_{12} m_{21}}{m_{22}} \right\} \right]$$

Fabry-Perot Interferometer

$$\delta = 2k_0 n_2 d \cos \theta_2$$



Asymmetric Fabry-Perot Interferometer with Gain or Loss

$$G = e^{\gamma d}$$

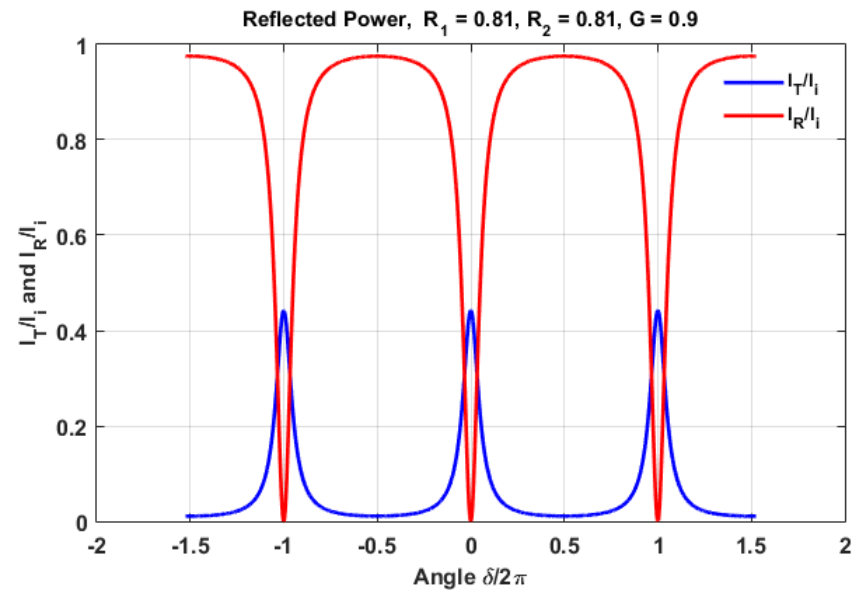
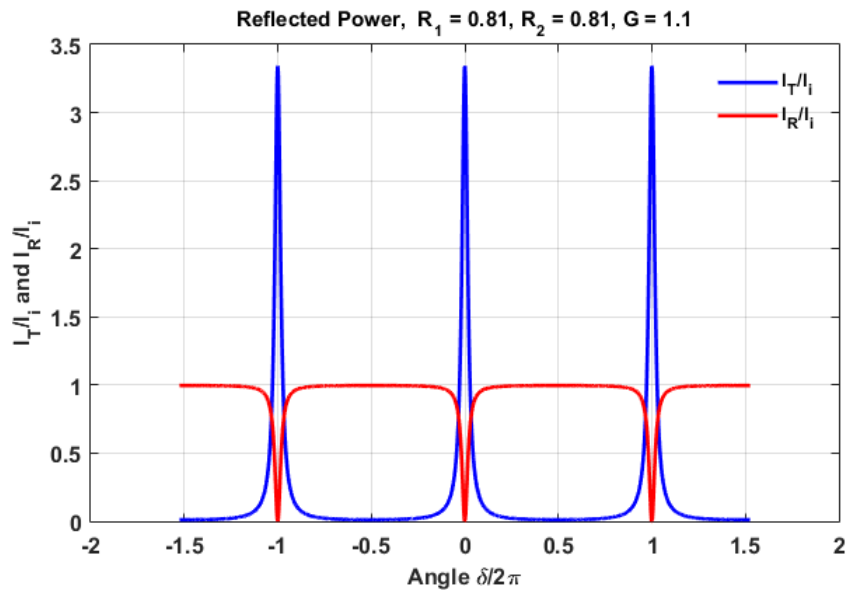
$$\frac{I_t}{I_i} = \frac{G(1 - R_1)(1 - R_2)}{(1 - G\sqrt{R_1R_2})^2 + 4G\sqrt{R_1R_2}\sin^2(\delta/2)}$$

$$\frac{I_r}{I_i} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2 + 4G\sqrt{R_1R_2}\sin^2(\delta/2)}{(1 - G\sqrt{R_1R_2})^2 + 4G\sqrt{R_1R_2}\sin^2(\delta/2)}$$

$$\delta = 2k_0n_2d \cos \theta_2$$

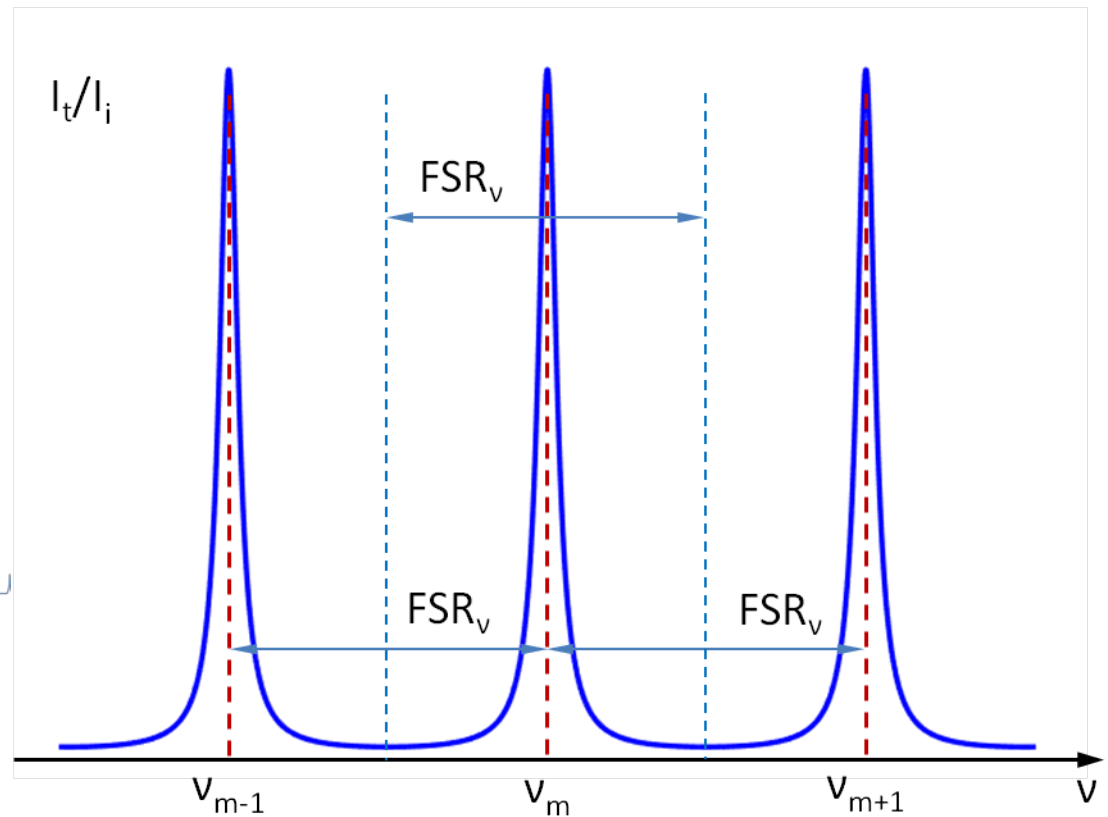
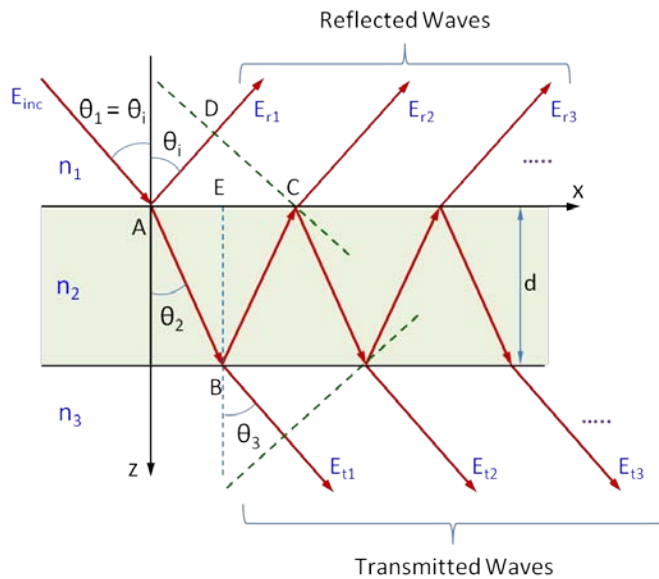
Gain

Loss



Symmetric Fabry-Perot Interferometer

Resonant Frequencies



$$\delta = 2k_0 n_2 d \cos \theta_2$$

$$FSR_\nu = \Delta\nu = \nu_{m+1} - \nu_m = \frac{c}{2dn_2 \cos \theta_2}$$

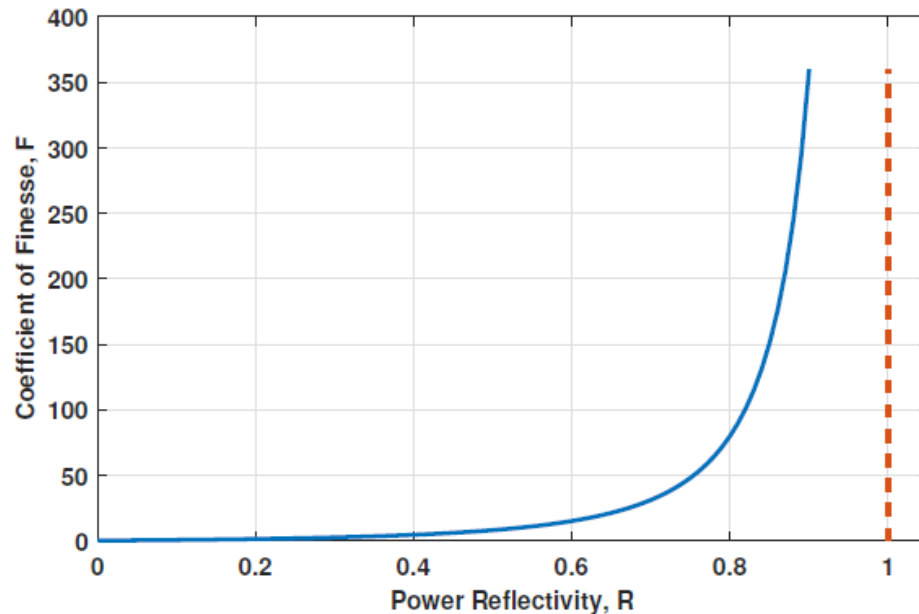
Symmetric Fabry-Perot Interferometer

$$\delta = 2k_0 n_2 d \cos \theta_2$$

$$\frac{I_t}{I_i} = \frac{(1 - R)^2}{(1 - R)^2 + 4R \sin^2(\delta/2 - \phi)} = \frac{1}{1 + F \sin^2(\delta/2 - \phi)},$$

$$F = \frac{4R}{(1 - R)^2}, \quad \text{Symmetric Fabry-Perot Case.}$$

Coefficient of Finesse

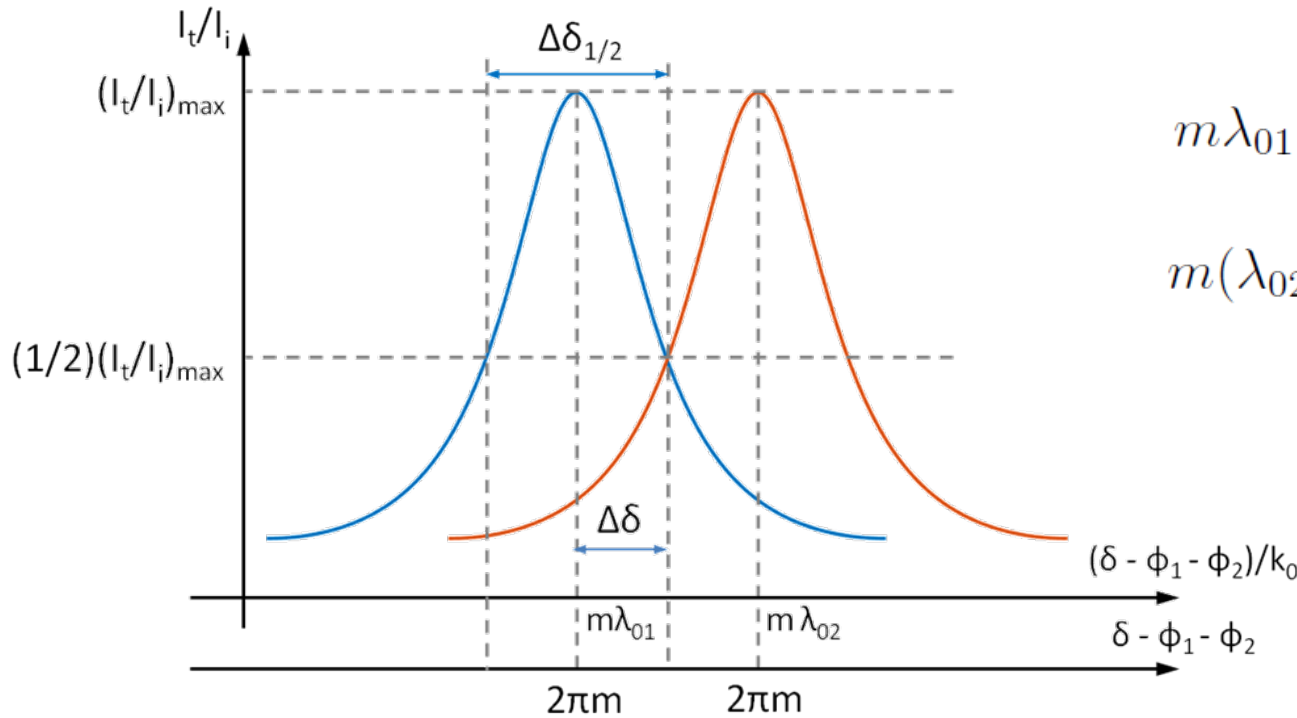


Coefficient of Finesse

$$F = \frac{4R}{(1 - R)^2}$$

Symmetric Fabry-Perot Interferometer

Minimum Wavelength Separation



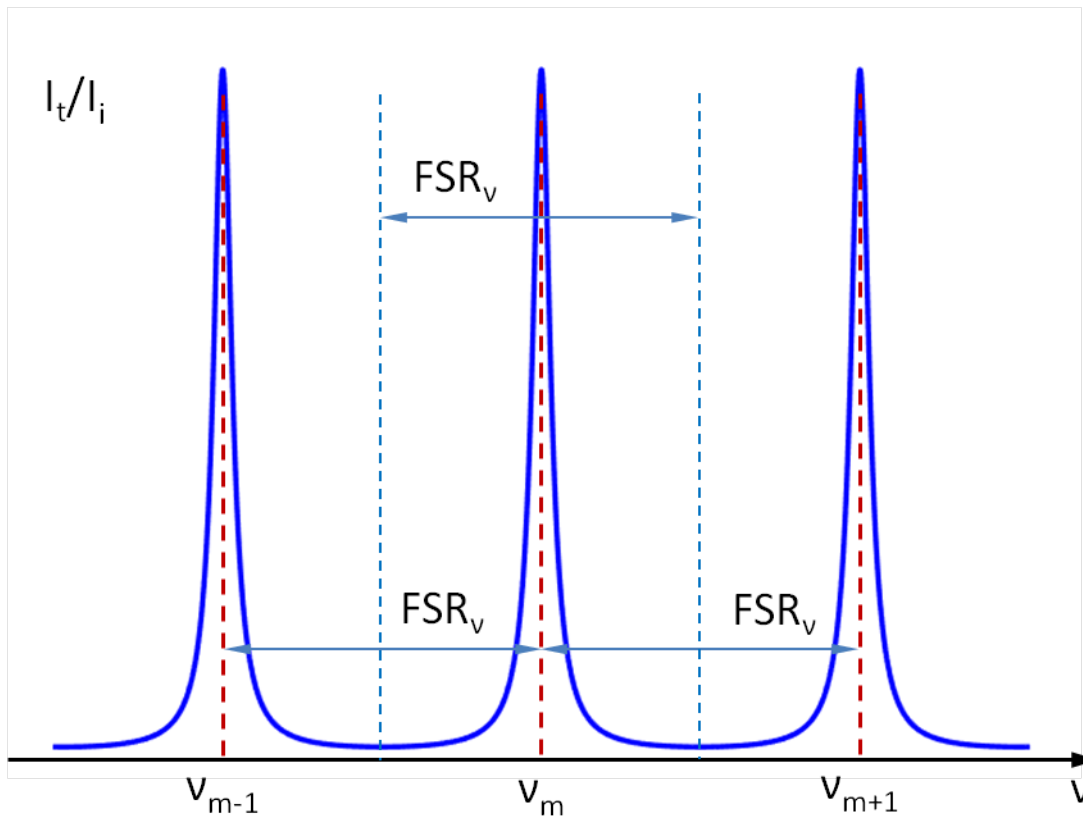
$$m\lambda_{01} + \frac{2\Delta\delta}{k_1} = m\lambda_{02} \implies$$

$$m(\lambda_{02} - \lambda_{01}) = \frac{2\lambda_{01}}{\pi\sqrt{F}} \implies$$

$$\Delta\lambda_{min} = \frac{2\lambda_{01}}{\pi m\sqrt{F}}$$

$$\frac{I_t}{I_i} = \frac{1}{1 + F \sin^2 \left(\frac{2\pi m + \Delta\delta}{2} \right)} = \frac{1}{2} \implies \Delta\delta \simeq \frac{2}{\sqrt{F}}$$

Symmetric Fabry-Perot Interferometer



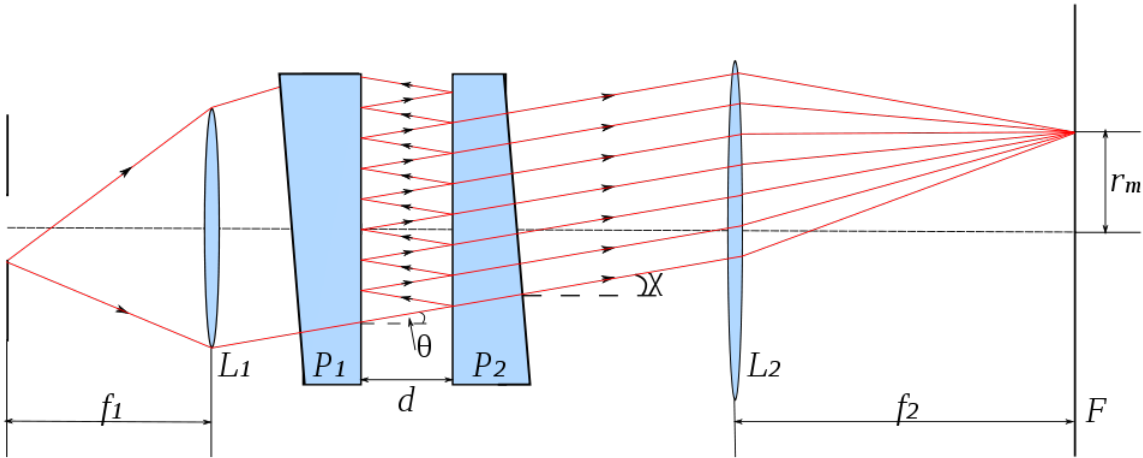
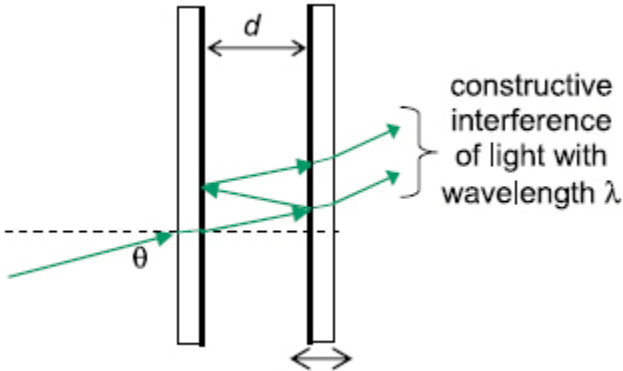
Resolving Power

$$\mathcal{R} = \frac{\lambda_0}{\Delta\lambda_{min}} = \frac{\pi m \sqrt{F}}{2}$$

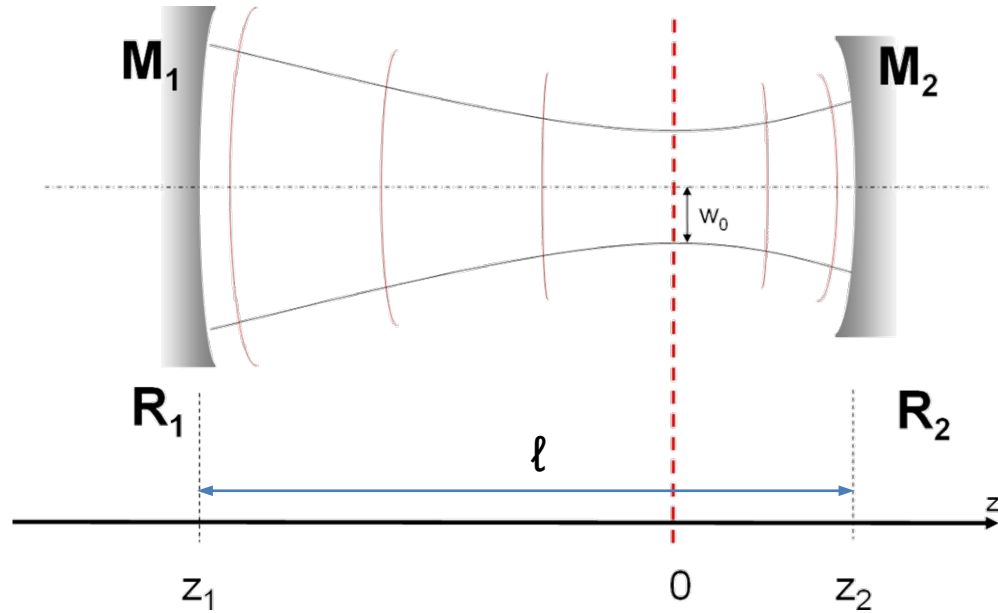
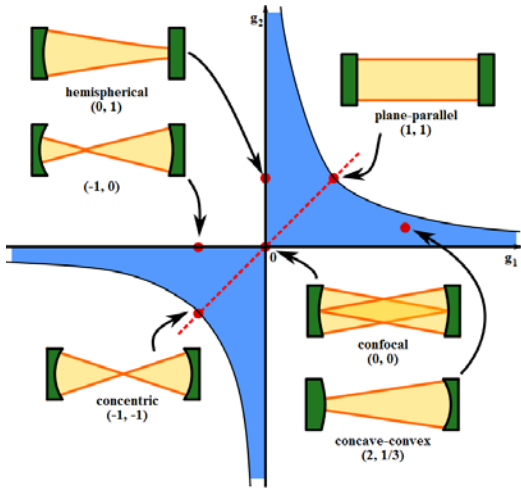
Finesse

$$\mathcal{F} = \frac{\Delta\lambda_{FSR}}{\Delta\lambda_{min}} = \frac{\pi}{2} \sqrt{F}$$

Fabry-Perot Interferometer



Two-Mirror Laser Resonator



$$z_1 = -\frac{\ell(R_2 - \ell)}{R_1 + R_2 - 2\ell}$$

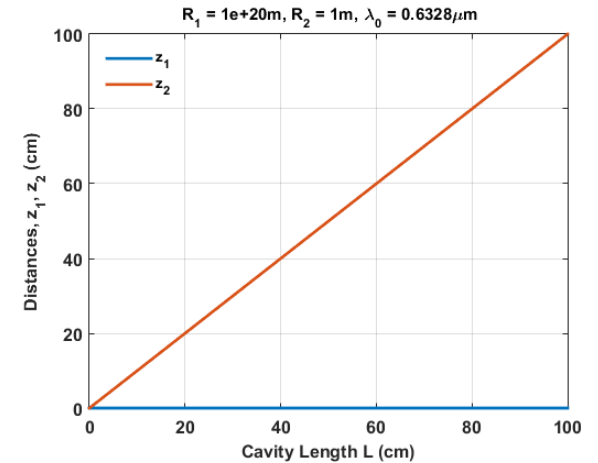
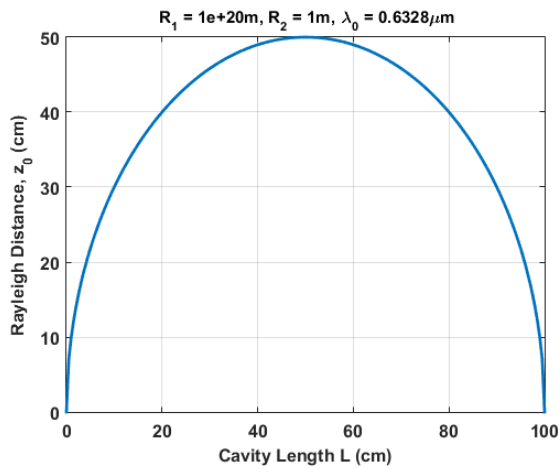
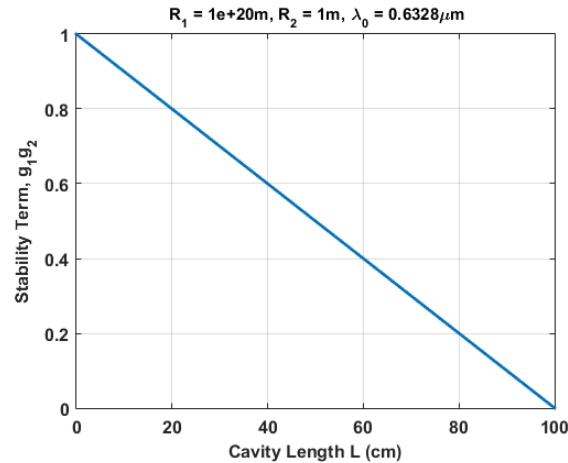
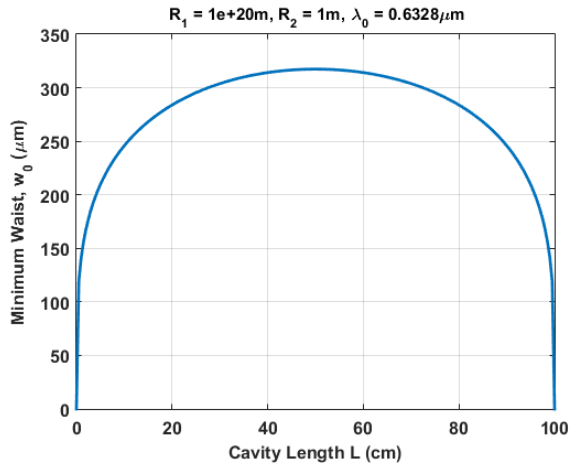
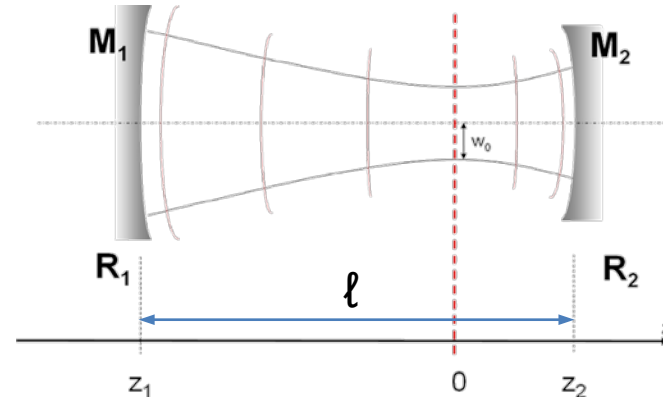
$$z_2 = +\frac{\ell(R_1 - \ell)}{R_1 + R_2 - 2\ell}$$

$$z_0^2 = \frac{\ell(R_1 - \ell)(R_2 - \ell)(R_1 + R_2 - \ell)}{(R_1 + R_2 - 2\ell)^2}$$

Two-Mirror Laser Resonator Example

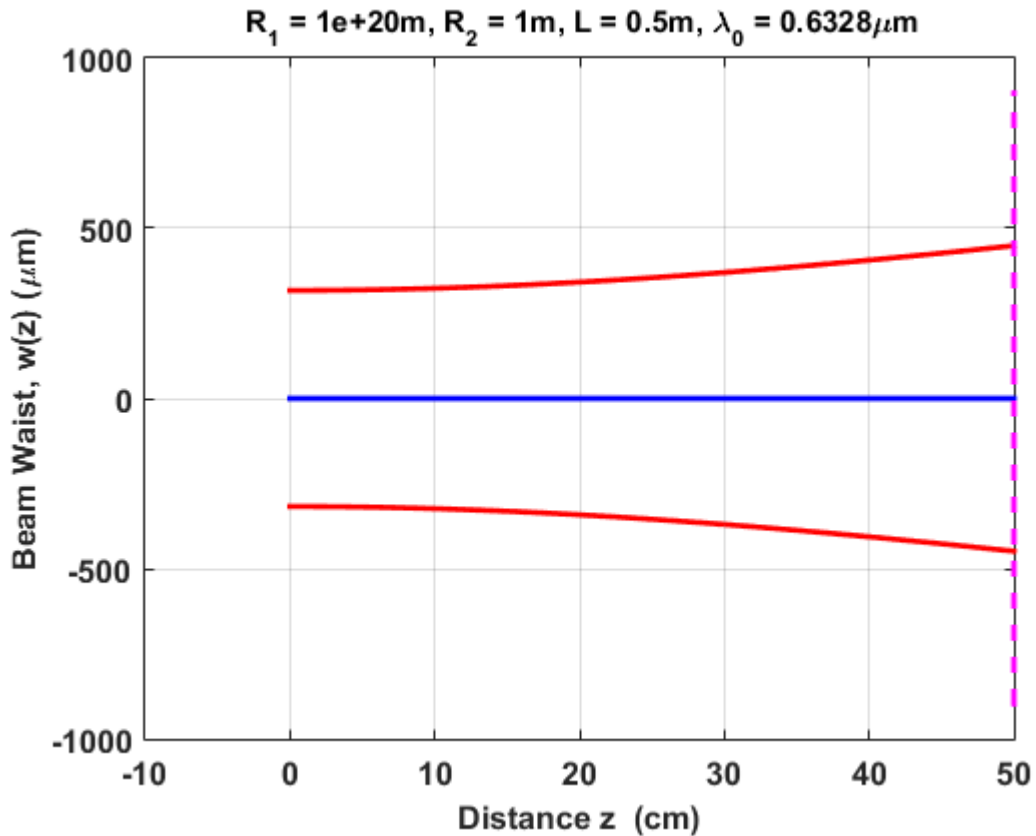
$R_1 = \text{Infinite}$

$R_2 = 1\text{m}$ ($R_2 > 0$)



Two-Mirror Laser Resonator Example

$R_1 = \text{Infinite}$, $R_2 = 1\text{m} (>0)$, $L = R_2/2 = 0.5\text{m}$

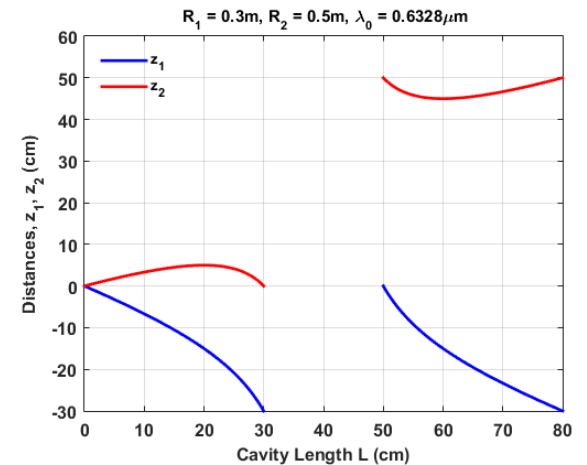
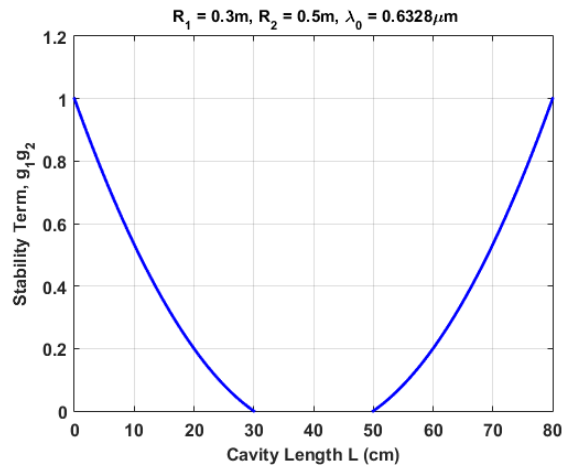
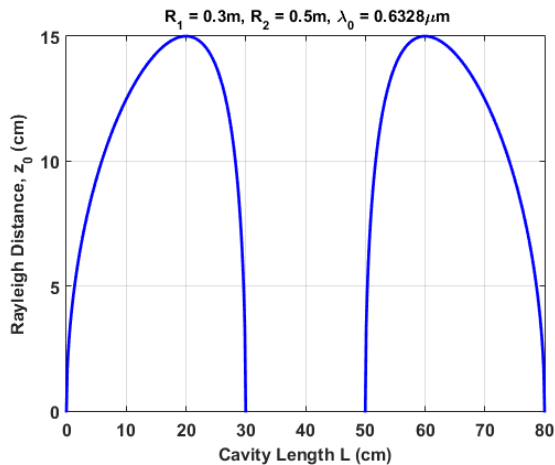
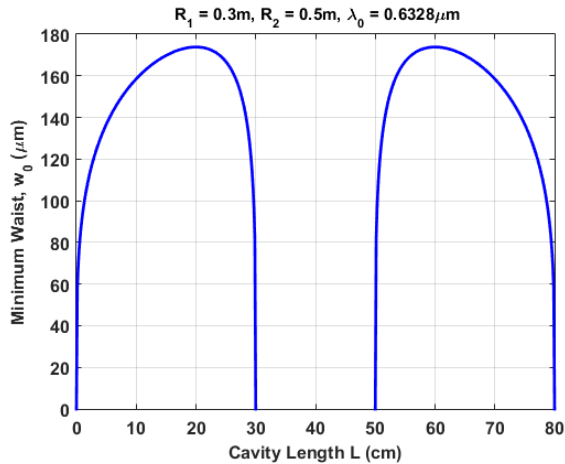
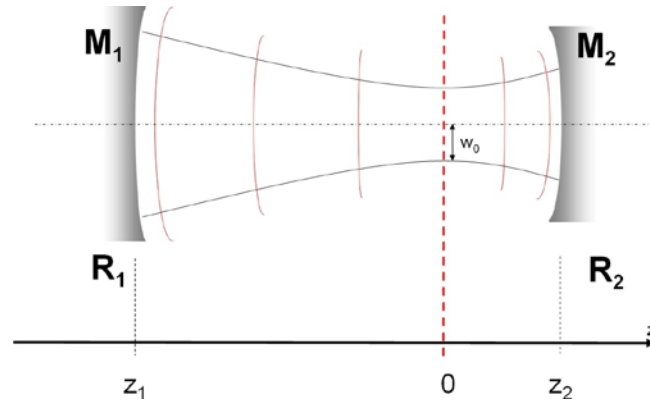


$z_0 = 0.5\text{m}$, $w_0 = 317.35\mu\text{m}$, $z_1 = 0$, $z_2 = 0.5\text{m}$

Two-Mirror Laser Resonator Example

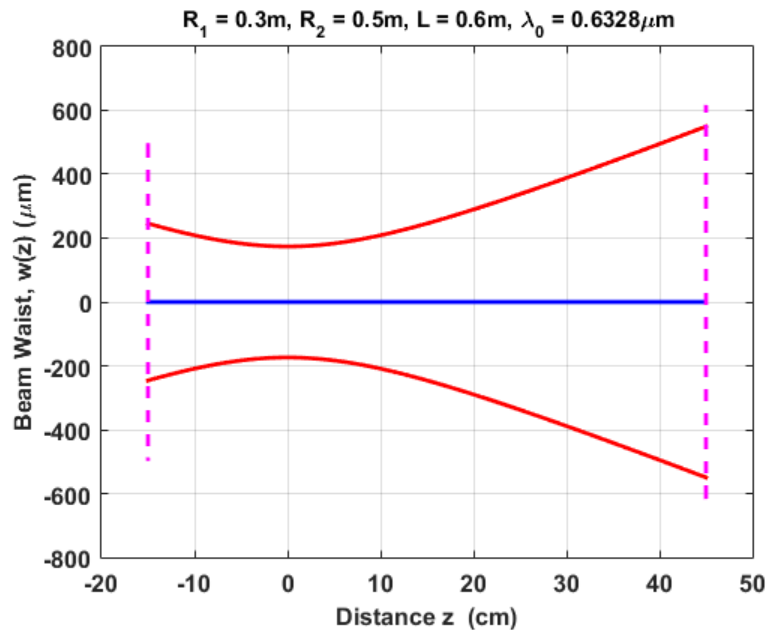
$R_1 = 0.3\text{m}$ ($R_1 > 0$)

$R_2 = 0.5\text{m}$ ($R_2 > 0$)



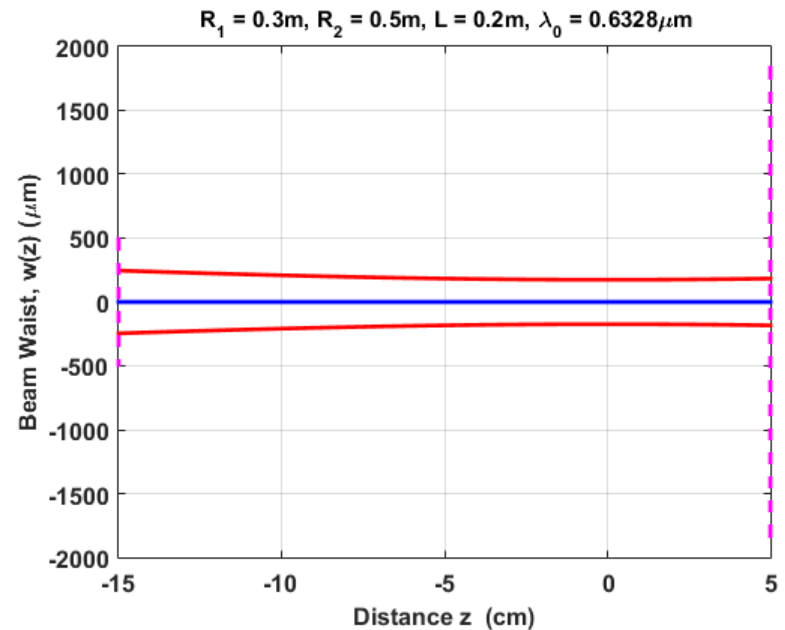
Two-Mirror Laser Resonator Example

$R_1 = 0.3\text{m} (>0)$, $R_2 = 0.5\text{m} (>0)$, $L = 0.6\text{m}$



$z_0 = 0.15\text{m}$, $w_0 = 173.82\mu\text{m}$,
 $z_1 = -0.15\text{m}$, $z_2 = 0.45\text{m}$

$R_1 = 0.3\text{m} (>0)$, $R_2 = 0.5\text{m} (>0)$, $L = 0.2\text{m}$

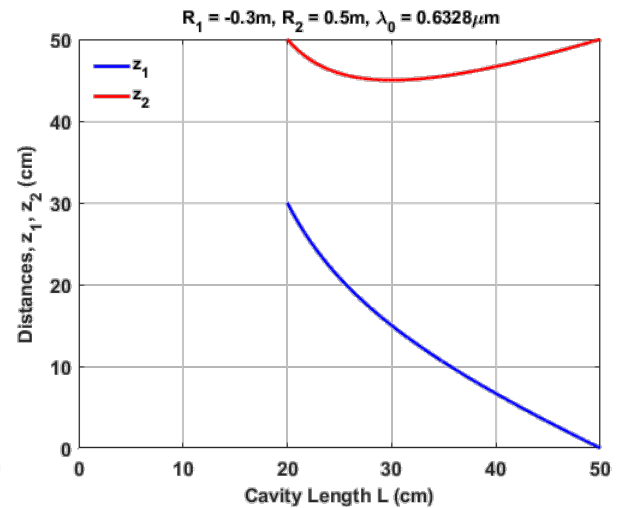
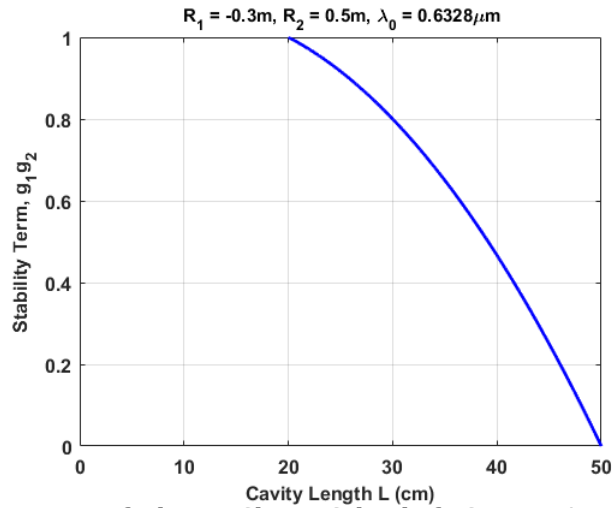
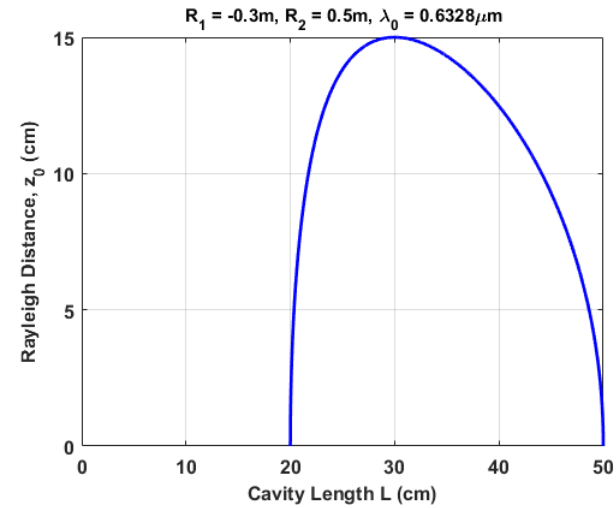
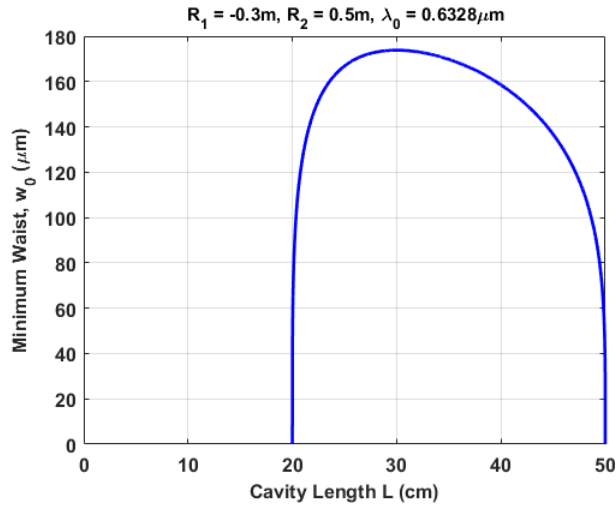
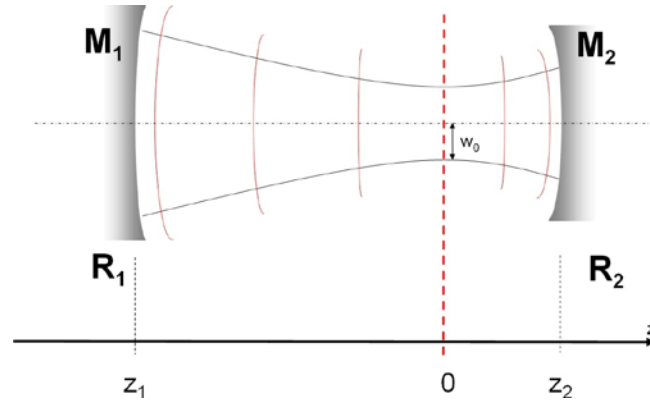


$z_0 = 0.15\text{m}$, $w_0 = 173.82\mu\text{m}$,
 $z_1 = -0.15\text{m}$, $z_2 = 0.05\text{m}$

Two-Mirror Laser Resonator Example

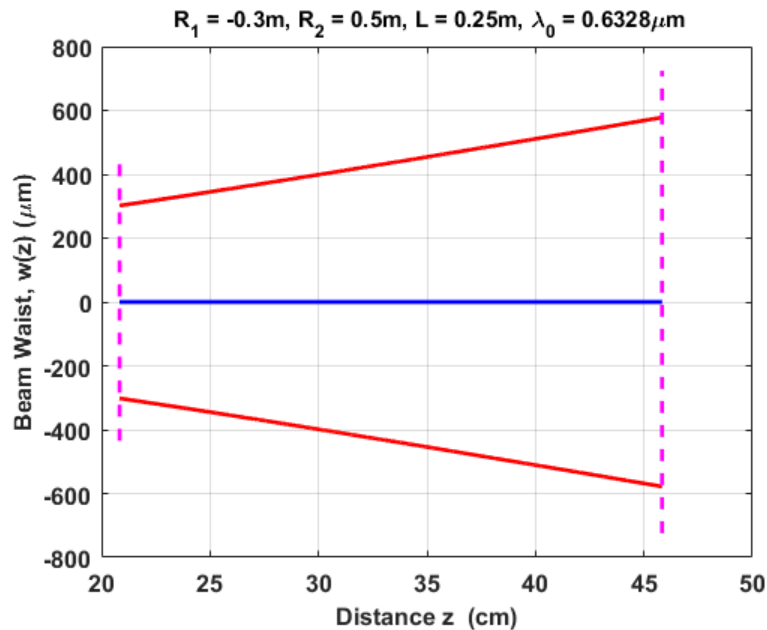
$R_1 = -0.3\text{m}$ ($R_1 < 0$)

$R_2 = 0.5\text{m}$ ($R_2 > 0$)



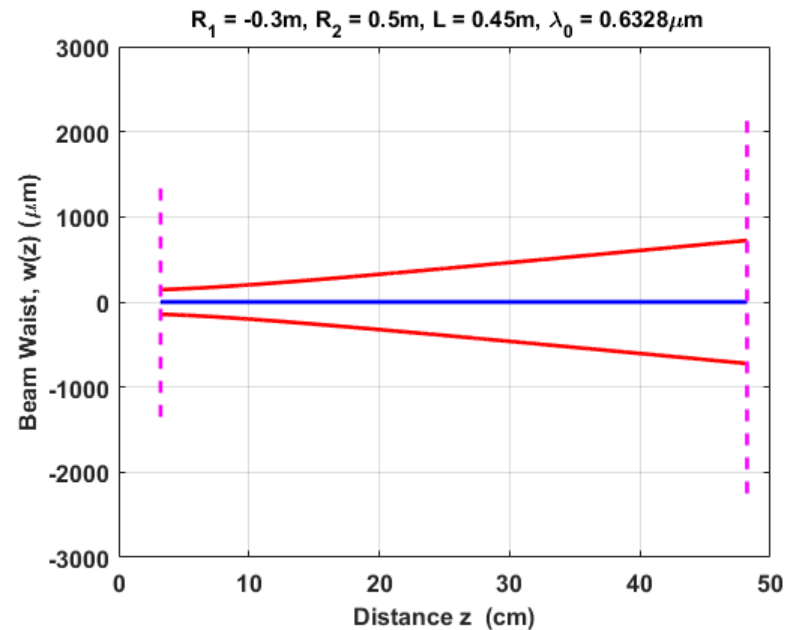
Two-Mirror Laser Resonator Example

$R_1 = -0.3\text{m} (<0)$, $R_2 = 0.5\text{m} (>0)$, $L = 0.25\text{m}$



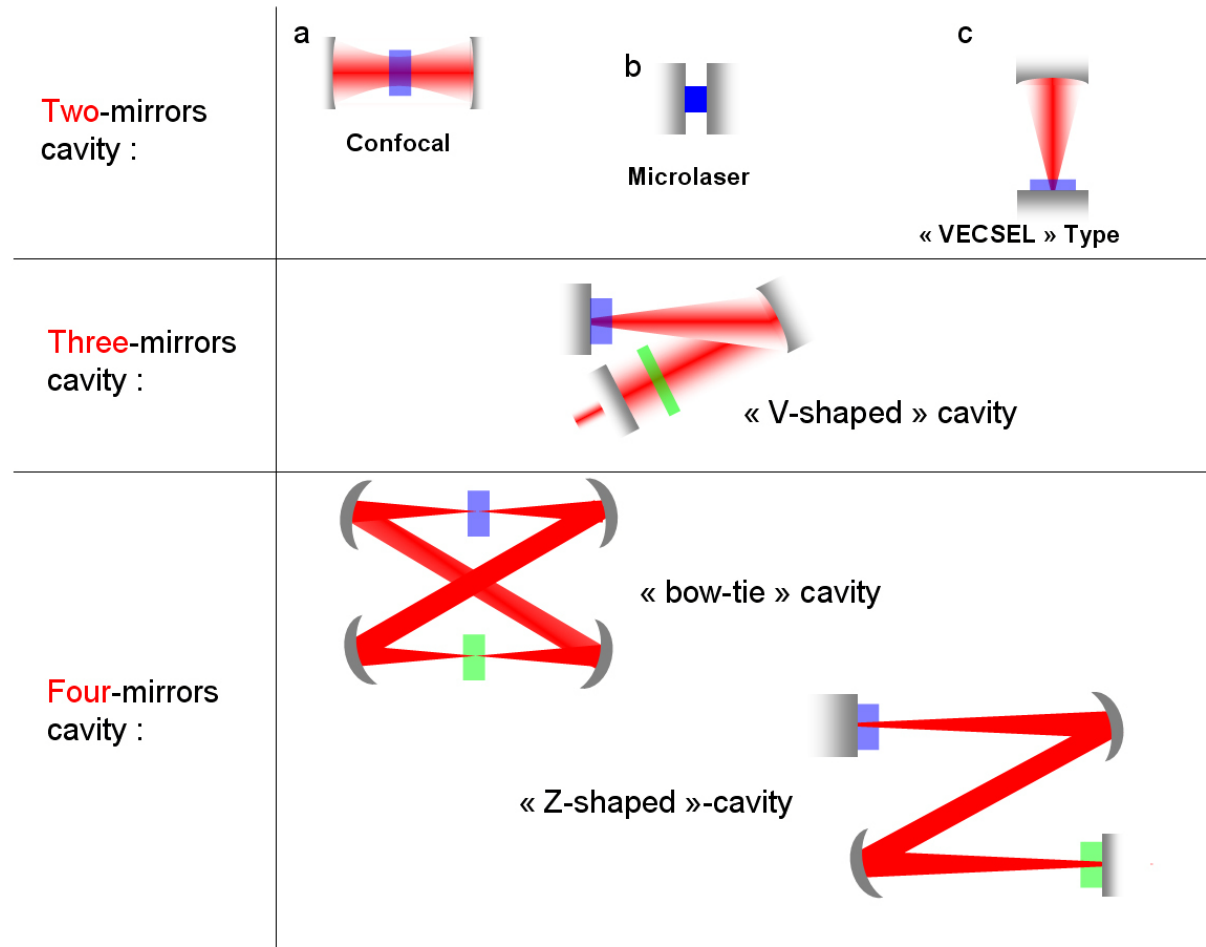
$z_0 = 0.1382\text{m}$, $w_0 = 166.84\mu\text{m}$,
 $z_1 = 0.2083\text{m}$, $z_2 = 0.4583\text{m}$

$R_1 = -0.3\text{m} (<0)$, $R_2 = 0.5\text{m} (>0)$, $L = 0.5\text{m}$

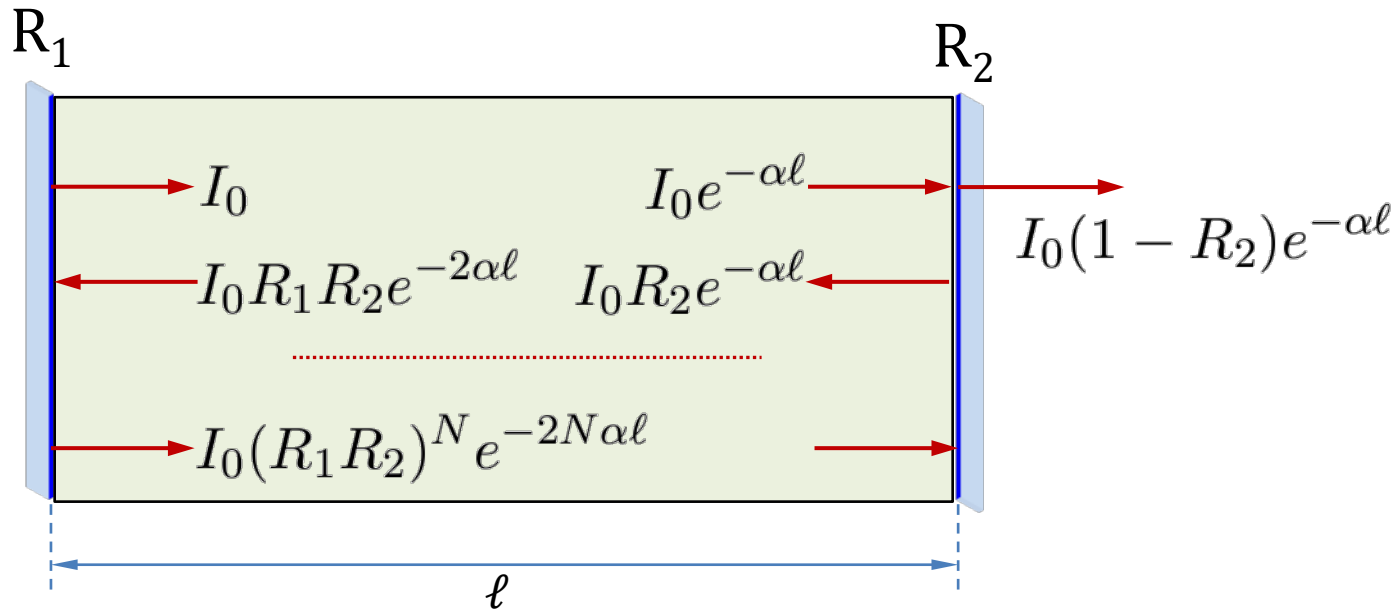


$z_0 = 0.0928\text{m}$, $w_0 = 136.71\mu\text{m}$,
 $z_1 = 0.0321\text{m}$, $z_2 = 0.4821\text{m}$

Different Laser Resonator Geometries



Cavity Lifetime – Approximate Approach

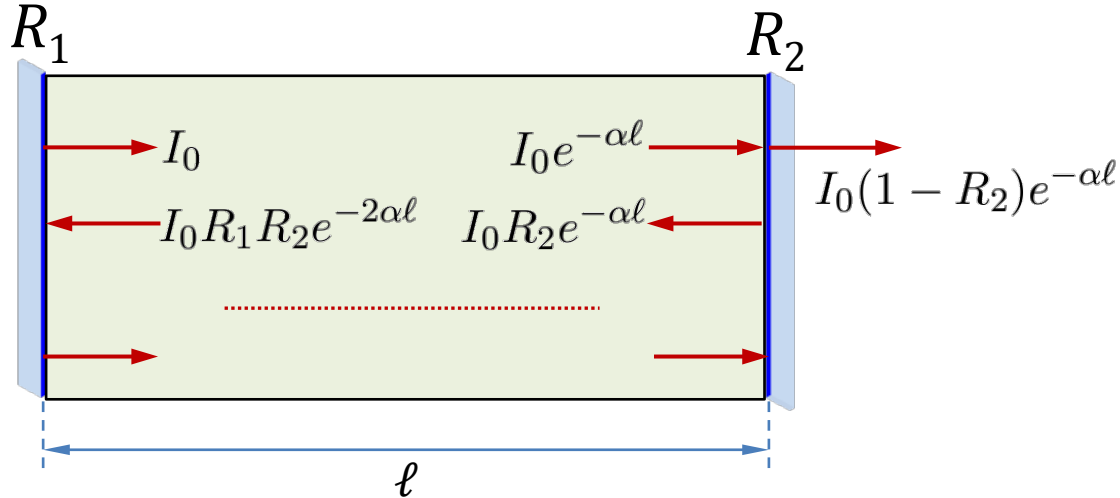


Assume N round-trips in the cavity:

$$\frac{I_0 (R_1 R_2)^N e^{-2N\alpha \ell}}{I_0} = e^{-1} \rightarrow t_N = \frac{2\ell N}{c/n} = t_c$$

$$t_c = \frac{n/c}{\alpha - \frac{1}{\ell} \ln(\sqrt{R_1 R_2})}$$

Cavity Lifetime – Accurate Approach



Rate of decrease in intensity (or number of photons) in the cavity:

$$\frac{dI}{dt} = -\frac{1 - R_1 R_2 e^{-2\alpha l}}{\tau_{RT}} I = -\frac{1}{t_c} I$$

$$I(t) = I_0 e^{t/t_c} \longrightarrow t_c = \frac{\tau_{RT}}{1 - R_1 R_2 e^{-2\alpha l}} = \frac{\tau_{RT}}{1 - S}$$

Survival Ratio: $S = R_1 R_2 e^{-2\alpha l}$

Round-Trip Time: $\tau_{RT} = \frac{2l}{c/n}$