



on the safety of high-speed trains running on bridges during earthquakes

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outline

motivation

proposed model

results – frequent earthquakes

results – rare earthquakes

conclusions



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motivation

contemporary high-speed railways (HSR's)



China's HSR

- operational speed: **300-350** km/h
- total HSR length: **16,000** km (to 28/12/2014)
- longest bridge : **164** km (over 4000 bridges)
- bridge/line ratio :

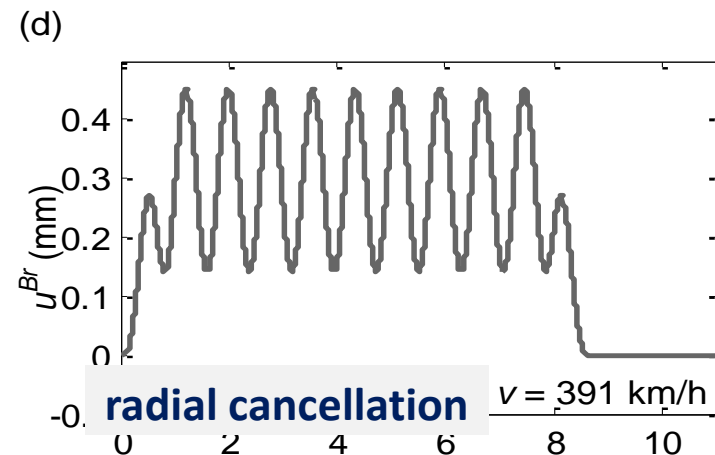
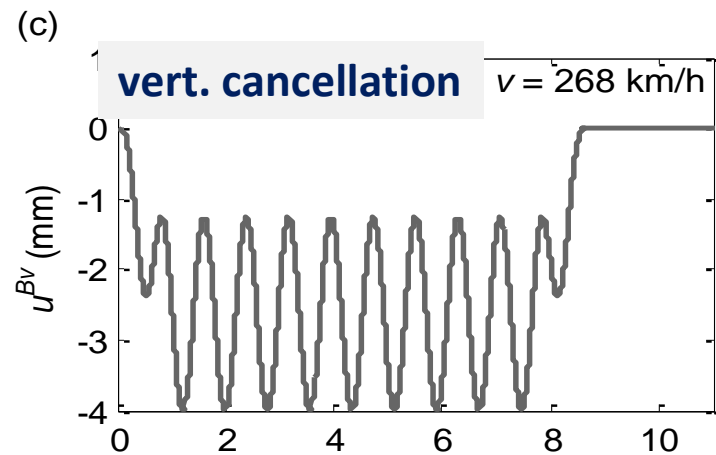
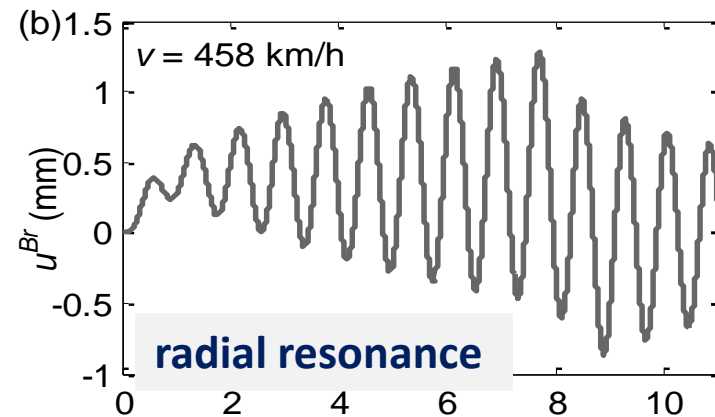
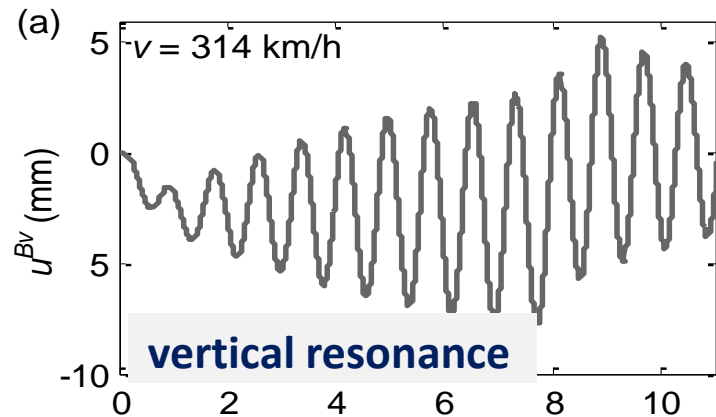
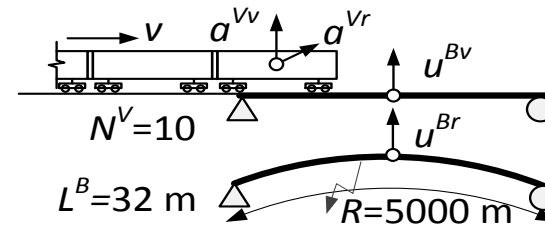
Beijing-Shanghai, China	80.5%
Taipei-Kaohsiung, Taiwan	73%
Beijing-Tianjin, China	86.6%



motivation

VBI: bridge resonance and cancellation

- ten identical 3D vehicles
- single span curved simple bridge
- u : displacement; a : acceleration
- V : vehicle, B : bridge
- v : vertical, r : radial





motivation

accidents: derailment of trains during earthquakes

Chūetsu Earthquake, Japan
($M_w = 6.8$ 23 Oct 2004)



- Shinkansen railway, 200 km/h
- broke the 48-year safety record

Jiashian earthquake, southern Taiwan
($M_w = 6.4$ 04 Mar 2010)



- 300 km/h high-speed train

from VBI to SVBI: Seismic Vehicle-Bridge Interaction



outline

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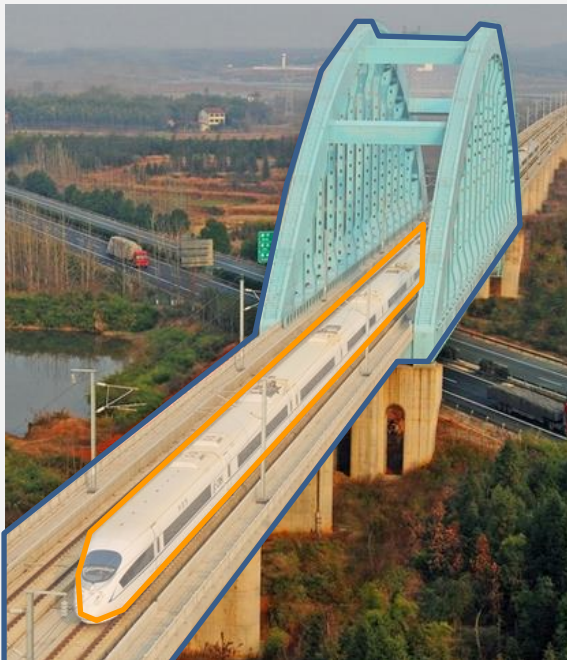
results – rare earthquakes

conclusions



proposed SVBI model

railway bridges



http://blog.sina.com.cn/s/blog_4d4c5f2b01014f60.html (2014)

modelling

vehicle

bridge

interaction

approach

multibody dynamics

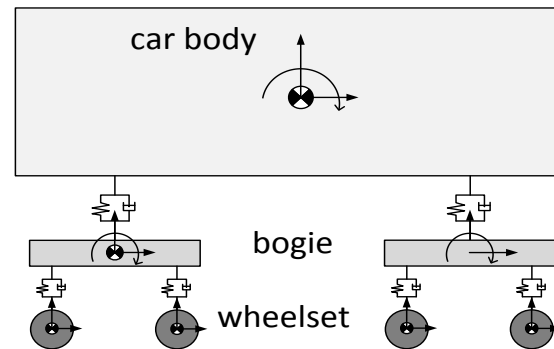
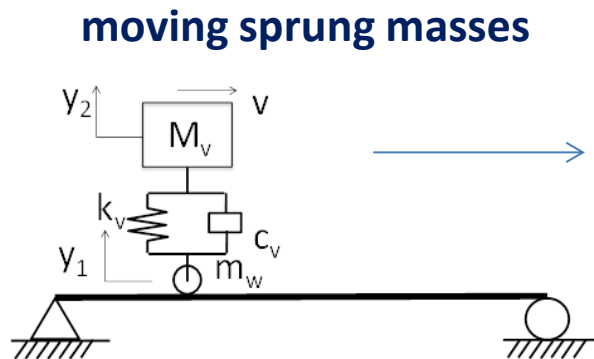
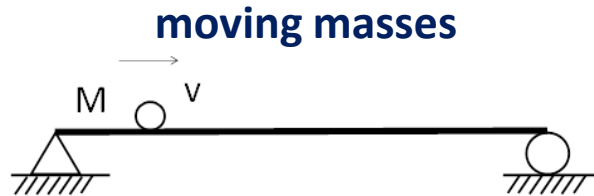
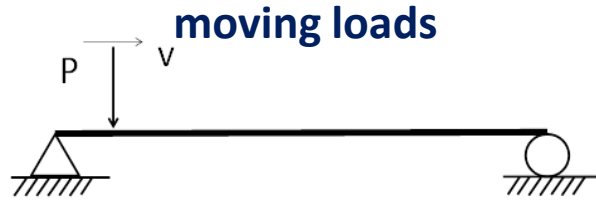
finite element method

nonsmooth dynamics



vehicle modelling

brief history



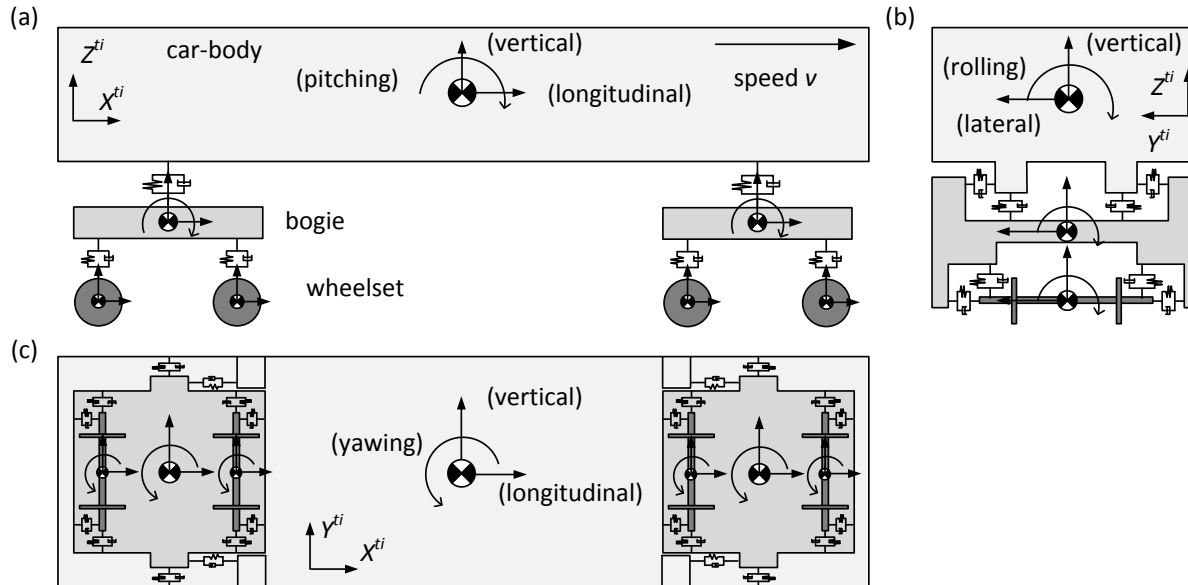
current trend

- beyond moving load analysis
- vehicle-bridge interaction analysis YB Yang (1995)
- **interdisciplinary**
civil + mechanical engineering



vehicle modelling

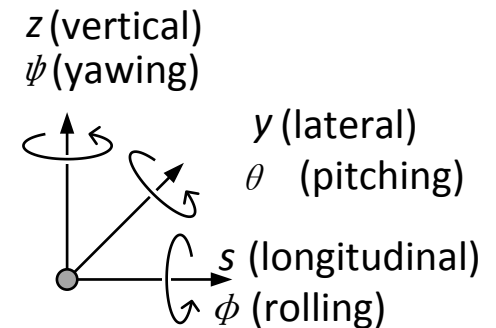
railway train vehicle



multibody assembly

- wheelsets, bogies, car-body → **rigid bodies**
- suspension → springs + dashpots
- e.g. 38 total DOF's

terminology



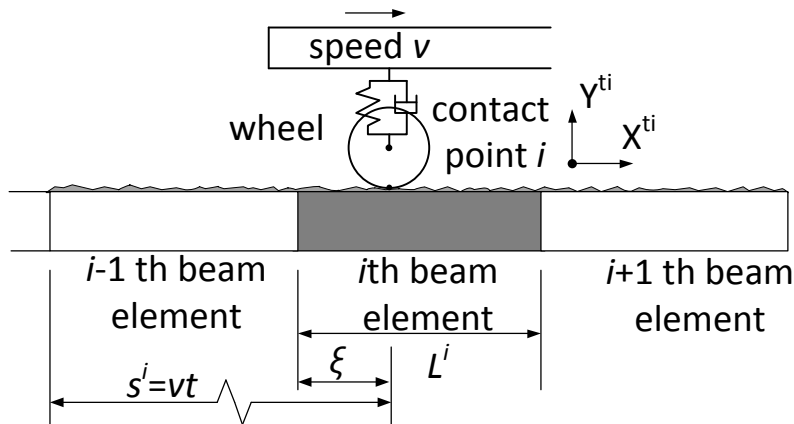
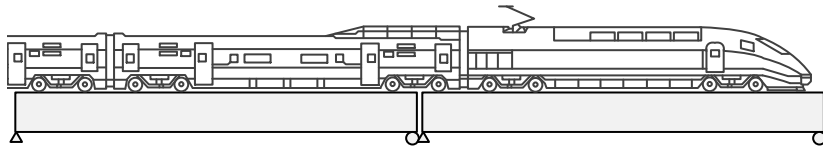


bridge subsystem

equation of motion



$$\mathbf{M}^B \ddot{\mathbf{u}}^B + \mathbf{C}^B \dot{\mathbf{u}}^B + \mathbf{K}^B \mathbf{u}^B + \boxed{\mathbf{W}_N^B \lambda_N + \mathbf{W}_T^B \lambda_T} = \mathbf{F}^B$$



- expressed in the inertia global system
- direction matrices \mathbf{W}_N^B and \mathbf{W}_T^B

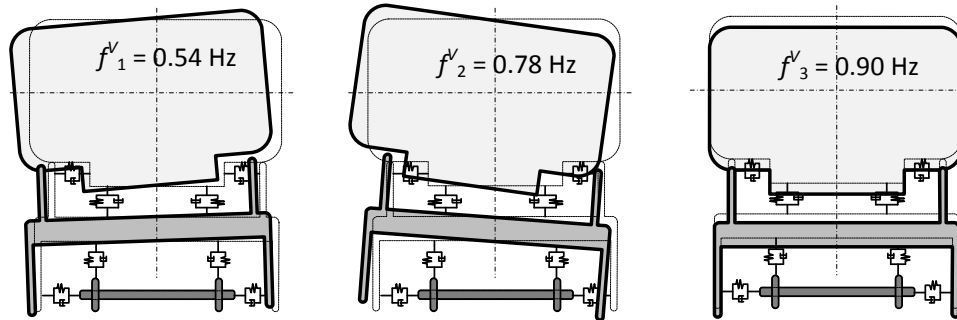
e.g. for a beam element

- **linear shape functions** for the axial (longitudinal) and torsional DOF's
- **cubic (Hermitian) shape functions** for the flexural DOF's
- the only **non-zero** entries in \mathbf{W}_N^B and \mathbf{W}_T^B → elements in **contact** with the wheel
- as vehicle wheel moves, different bridge element contact with wheel
- \mathbf{W}_N^B and \mathbf{W}_T^B : **time-dependent**

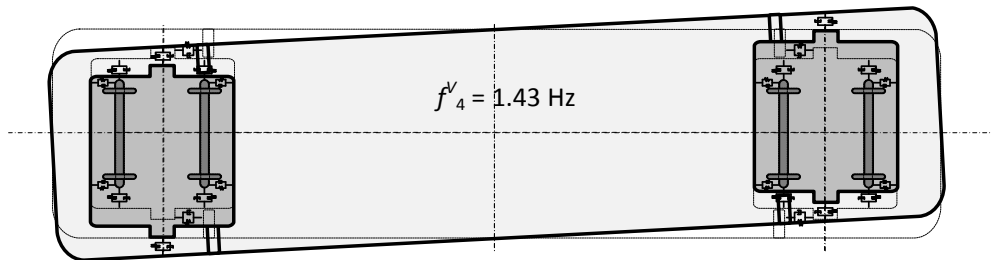


vehicle modelling

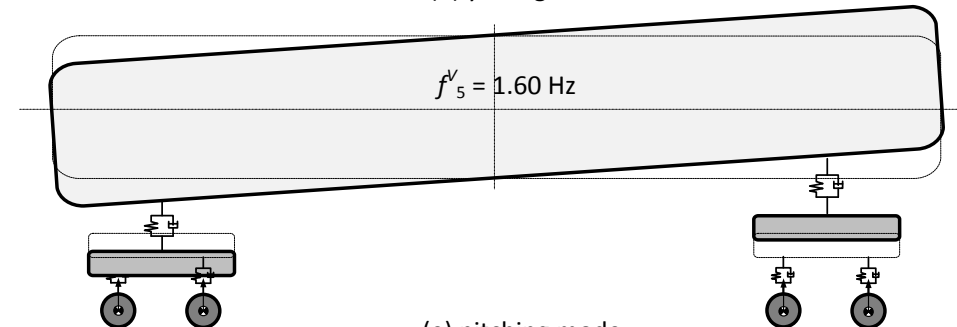
railway train vehicle



(a) first lateral-rolling mode (b) second lateral-rolling mode (c) vertical mode



(d) yawing mode



(e) pitching mode

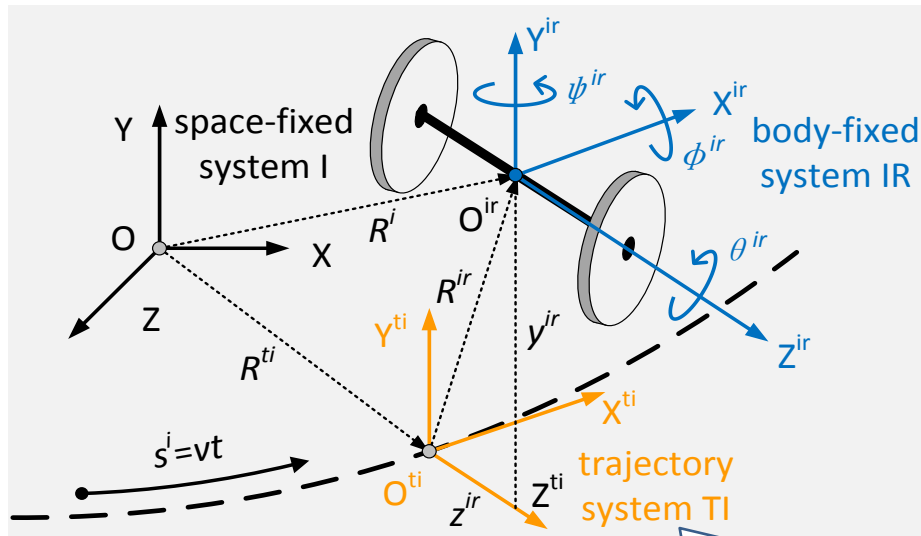
multibody assembly

- wheelsets, bogies, car-body → **rigid bodies**
- suspension → springs + dashpots



vehicle modelling

vehicle-dynamics



3 systems of reference

(Shabana 2010)

- inertial (space-fixed) system I
- body-fixed system IR
- **moving trajectory system TI**

moving trajectory system TI (for curved paths)

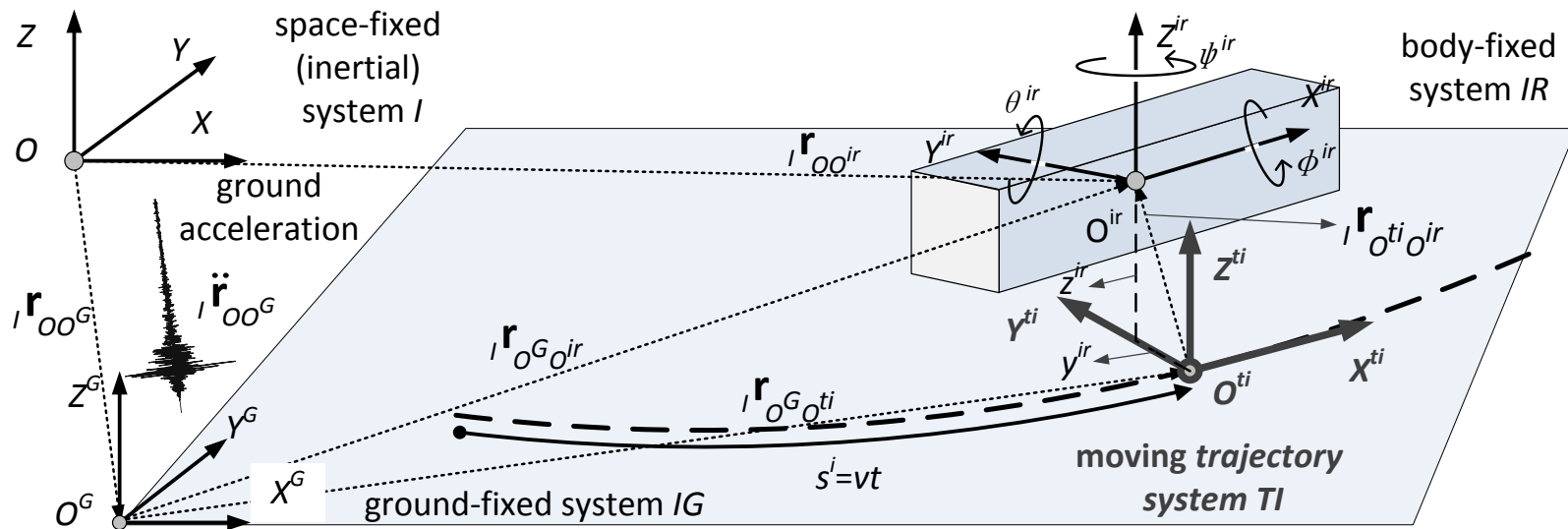
- moves along the curve
- longitudinal direction $O^{ti}X^{ti}$: tangent to the curve
- origin and orientation : defined by the arc length, s^i



vehicle subsystem

equation of motion on a curved path

$${}^I \ddot{\mathbf{r}}_{O^i O^i r} = {}^I \ddot{\mathbf{r}}_{O^i O^i G} + {}^I \mathbf{L}^i T I \ddot{\mathbf{u}}^i + {}^I \boldsymbol{\gamma}^i R$$



$$\mathbf{M}^i(t) = {}^I \mathbf{L}^i(t)^T m^i {}^I \mathbf{L}^i(t) + {}_{IR} \mathbf{H}^i(t)^T {}_{IR} \mathbf{I}_{\theta\theta IR}^i \mathbf{H}^i(t)$$

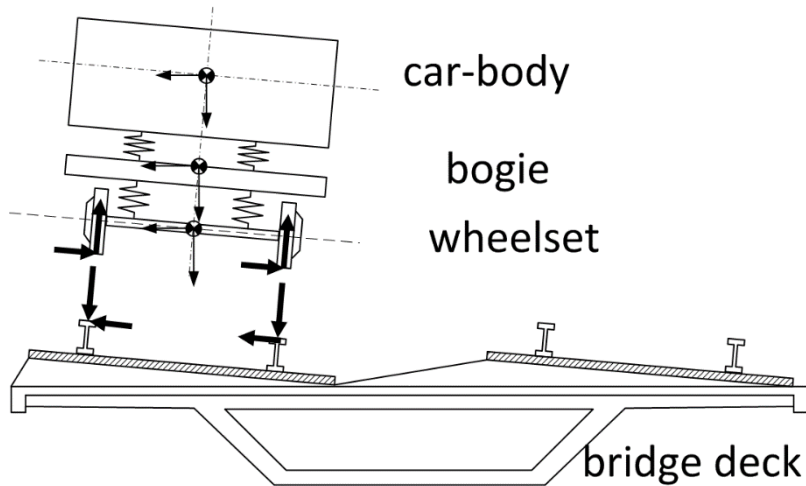
$$\mathbf{F}_v^i = -m^i {}^I \mathbf{L}^i(t)^T {}^I \boldsymbol{\gamma}^i R - {}_{IR} \mathbf{H}^i(t)^T \left({}_{IR} \mathbf{I}_{\theta\theta IR}^i \boldsymbol{\gamma}_\alpha^i + {}_{IR} \boldsymbol{\omega}^i \times \left({}_{IR} \mathbf{I}_{\theta\theta IR}^i \boldsymbol{\omega}^i \right) \right)$$

$$\mathbf{F}_G^i = -m^i {}^I \mathbf{L}^i(t)^T {}^I \ddot{\mathbf{r}}_{O^i O^i G}$$



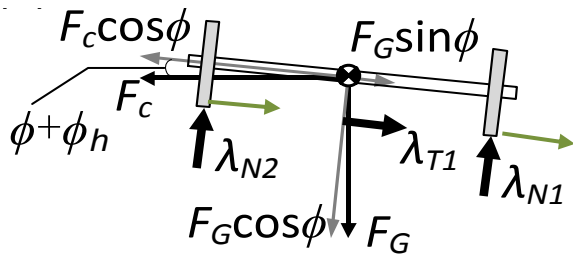
vehicle subsystem

equation of motion



$$\mathbf{M}^V(t)\ddot{\mathbf{u}}^V + \mathbf{C}^V\dot{\mathbf{u}}^V + \mathbf{K}^V\mathbf{u}^V - \mathbf{W}_N^V\lambda_N - \mathbf{W}_T^V\lambda_T = \mathbf{F}^V$$

- expressed in the moving **trajectory system**
- $\mathbf{M}^V(t) \rightarrow$ time varying for curved path
- λ_N and λ_T = **normal** and **tangential** contact force vector
- \mathbf{W}_N^V and \mathbf{W}_T^V = **direction matrices** of λ_N and λ_T
- \mathbf{F}^V = gravity, **inertia (centrifugal and coriolis forces)** due to the **curved path** **seismic** loads if considered





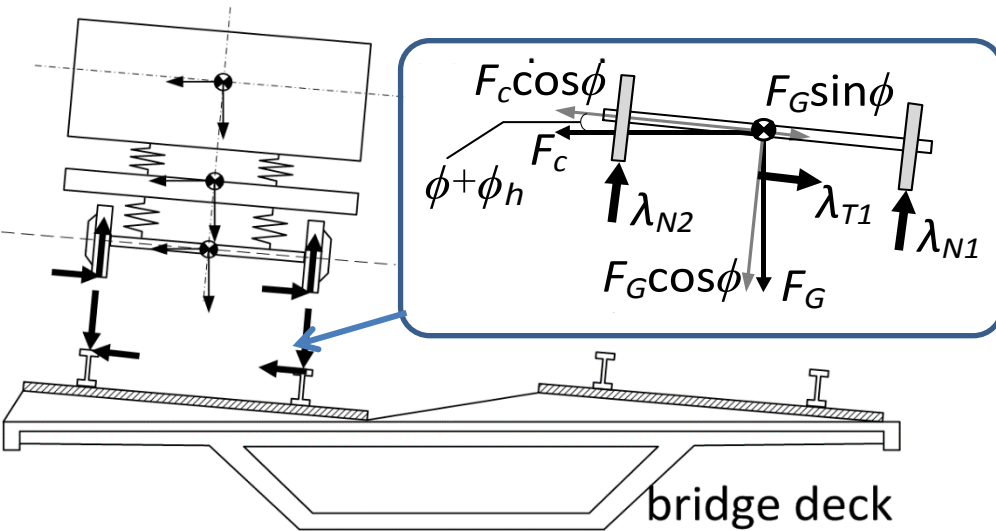
coupled vehicle-bridge system

equation of motion

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\boldsymbol{\lambda} = \mathbf{F}$$

contact forces (coupling)

- global matrices
- **contact forces λ**



\mathbf{W} contains the coupling
is **time-dependent**

$$\left\{ \begin{array}{l} \mathbf{M} = \begin{bmatrix} \mathbf{M}^V(t) & \mathbf{0} \\ \mathbf{0} & \mathbf{M}^B \end{bmatrix}, \mathbf{C} = \begin{bmatrix} \mathbf{C}^V & \mathbf{0} \\ \mathbf{0} & \mathbf{C}^B \end{bmatrix}, \\ \mathbf{K} = \begin{bmatrix} \mathbf{K}^V & \mathbf{0} \\ \mathbf{0} & \mathbf{K}^B \end{bmatrix}, \mathbf{u} = \begin{Bmatrix} \mathbf{u}^V \\ \mathbf{u}^B \end{Bmatrix}, \mathbf{F} = \begin{Bmatrix} \mathbf{F}^V \\ \mathbf{F}^B \end{Bmatrix}, \\ \mathbf{W} = [\mathbf{W}_N \quad \mathbf{W}_H], \boldsymbol{\lambda} = \begin{Bmatrix} \lambda_N \\ \lambda_T \end{Bmatrix}, \\ \mathbf{W}_T = \begin{Bmatrix} \mathbf{W}_T^V \\ -\mathbf{W}_T^B(t) \end{Bmatrix}, \mathbf{W}_N = \begin{Bmatrix} \mathbf{W}_N^V \\ -\mathbf{W}_N^B(t) \end{Bmatrix} \end{array} \right.$$



coupled vehicle-bridge system

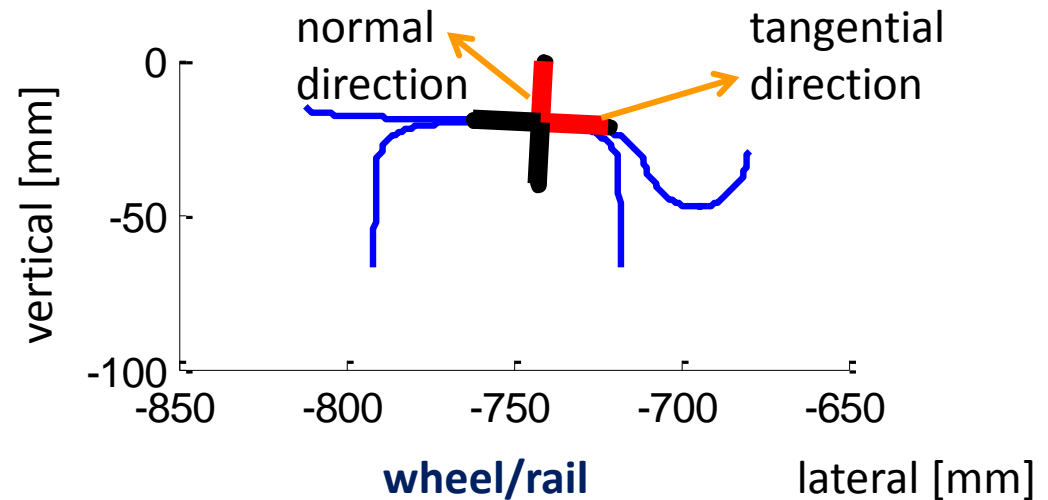
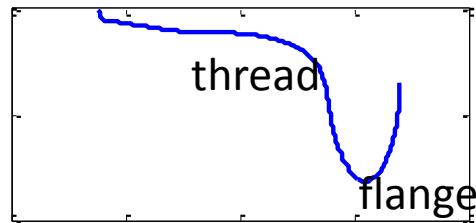
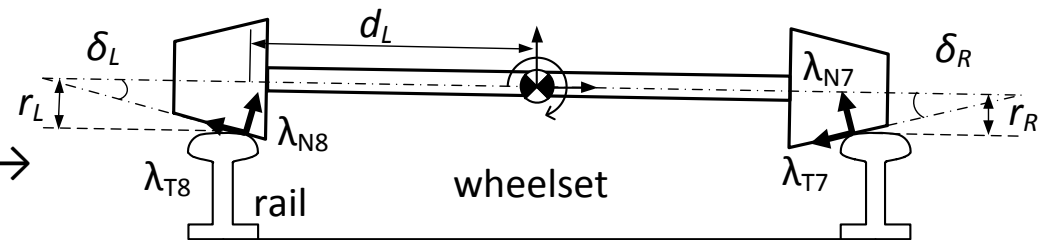
wheel-rail contact interaction

point and direction of contact

- **continuous contact**

the wheel is in contact with the rail \rightarrow
nonlinear wheel, rail profile

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\lambda = \mathbf{F}$$





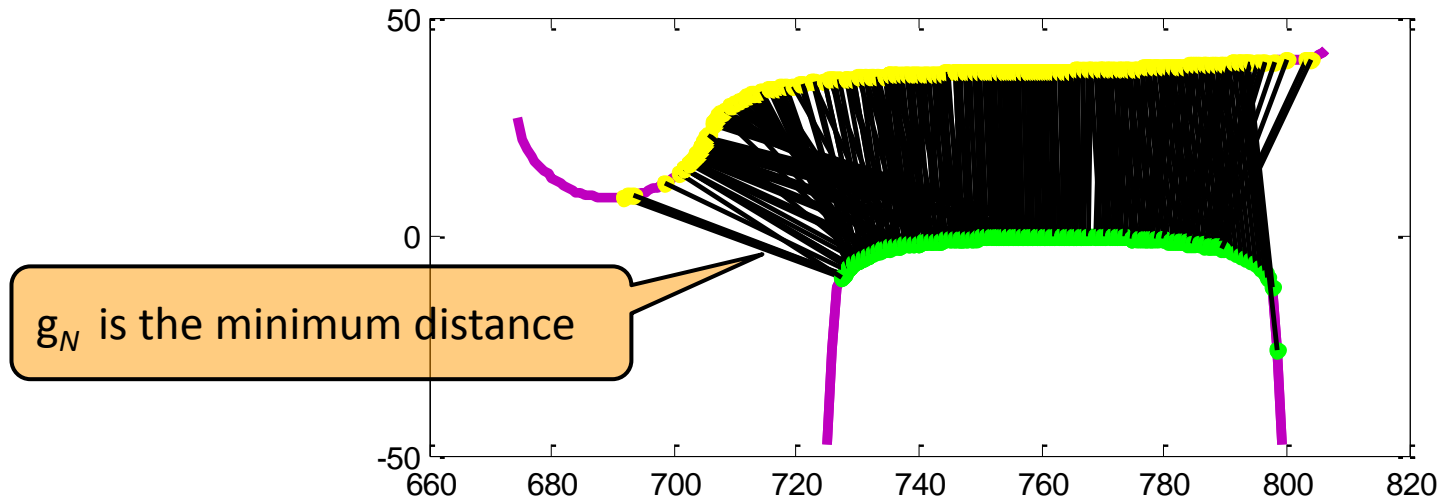
coupled vehicle-bridge system

wheel-rail contact interaction

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\lambda = \mathbf{F}$$

point and direction of contact

- wheel-rail separation/ detachment (uplifting)



- single/double separation



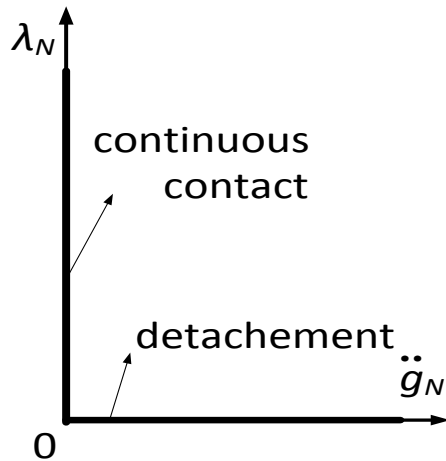
coupled vehicle-bridge system

wheel-rail contact interaction

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\boldsymbol{\lambda} = \mathbf{F}$$

normal direction

- **continuous contact vs detachment** (separation)



contact-detachment transition is formulated as a **Linear Complimentary Problem (LCP)**

→ **nonsmooth approach**

- contact: zero contact acceleration
- detachment: zero normal contact force

$$\begin{cases} \ddot{g}_N = 0 \wedge \lambda_N \geq 0 & \text{continuous contact} \\ \ddot{g}_N \geq 0 \wedge \lambda_N = 0 & \text{detachment} \end{cases}$$

- **impact and recontact**

- Newton's law
- normal contact displacement $g_N = 0$ and $(\dot{g}_N < 0)$
- velocity jump on the velocity level



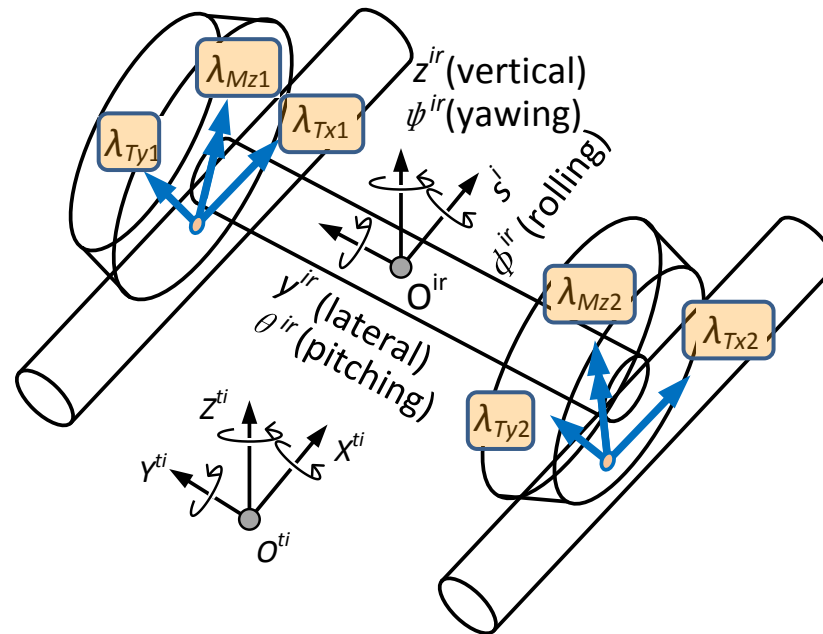
coupled vehicle-bridge system

wheel-rail contact interaction

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\boldsymbol{\lambda} = \mathbf{F}$$

tangential direction $\boldsymbol{\lambda}_T = [\lambda_{Tx} \ \lambda_{Ty} \ \lambda_{Mz}]^T$

- creep lateral / longitudinal forces
- creep spin moment
- rolling contact





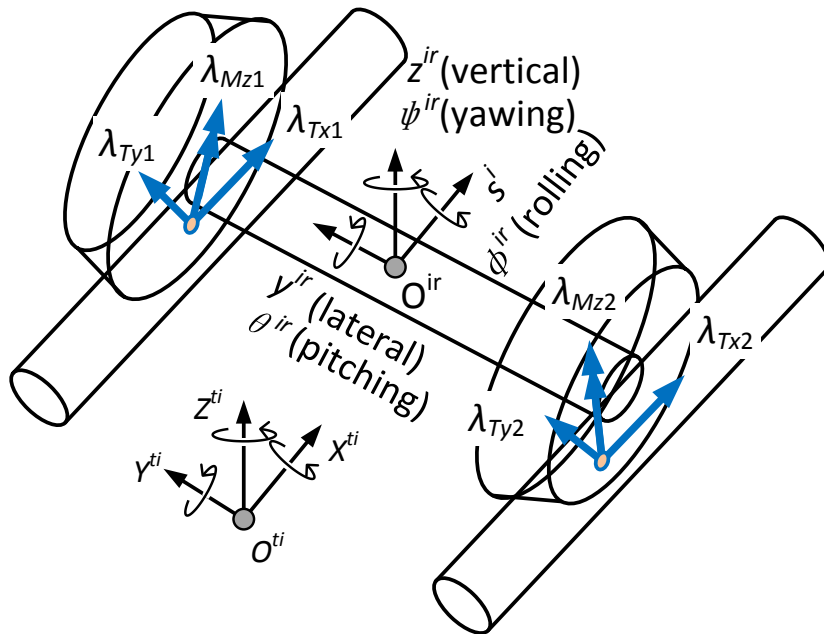
coupled vehicle-bridge system

wheel-rail contact interaction

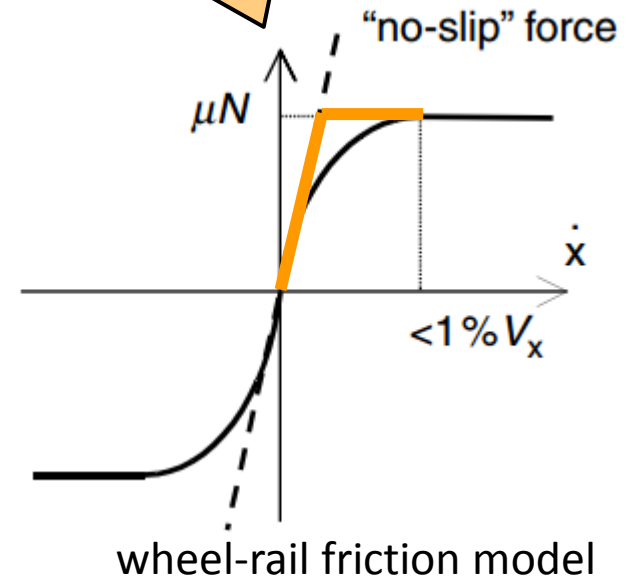
$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} - \mathbf{W}\lambda = \mathbf{F}$$

tangential direction $\lambda_T = [\lambda_{Tx} \ \lambda_{Ty} \ \lambda_{Mz}]^T$

- creep lateral / longitudinal forces
- creep spin moment



nonlinear relationship between creep forces and creepage





coupled vehicle-bridge system

final equations of motion

$$\mathbf{M}^*(t)\ddot{\mathbf{u}}(t) + \mathbf{C}^*(t)\dot{\mathbf{u}}(t) + \mathbf{K}^*(t)\mathbf{u}(t) = \mathbf{F}^*(t)$$

$$\begin{cases} \mathbf{C}^* = \left[\mathbf{E} - \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{W}_N^T \mathbf{M}^{-1} \right] (\mathbf{C} + \mathbf{C}_\xi) + 2\nu \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{W}_N''^T \\ \mathbf{K}^* = \left[\mathbf{E} - \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{W}_N^T \mathbf{M}^{-1} \right] \mathbf{K} + \nu^2 \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{W}_N'^T \\ \mathbf{F}^* = \left[\mathbf{E} - \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{W}_N^T \mathbf{M}^{-1} \right] (\mathbf{F} - \mathbf{F}_\xi) - \nu^2 \mathbf{W}_N \mathbf{G}_{NN}^{-1} \mathbf{r}_{cN}'' \end{cases}$$

effect of: **normal** contact forces **creep** forces **rail irregularities**

- \mathbf{M}^* → **time-dependent** (for curved path)
- \mathbf{K}^* and \mathbf{C}^* → **time-dependent** and **coupled**
- \mathbf{F}^* → **time-dependent**
- \mathbf{E} → identity matrix;
- $\mathbf{G}(t)^{-1} = (\mathbf{W}^T \mathbf{M}^{-1} \mathbf{W})^{-1}$ → the **effective mass** during contact
- $()'$ and $()''$ → the derivatives with respect to the arc length



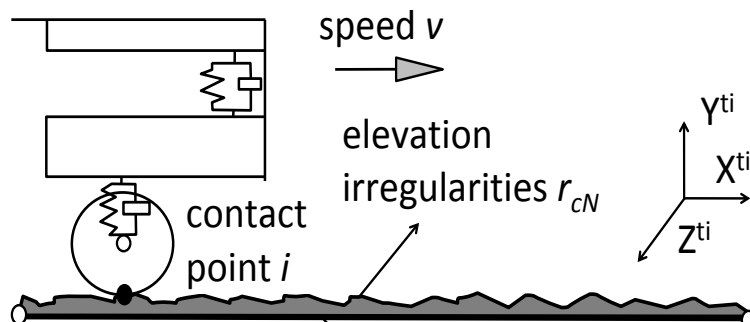
coupled vehicle-bridge system

final equations of motion

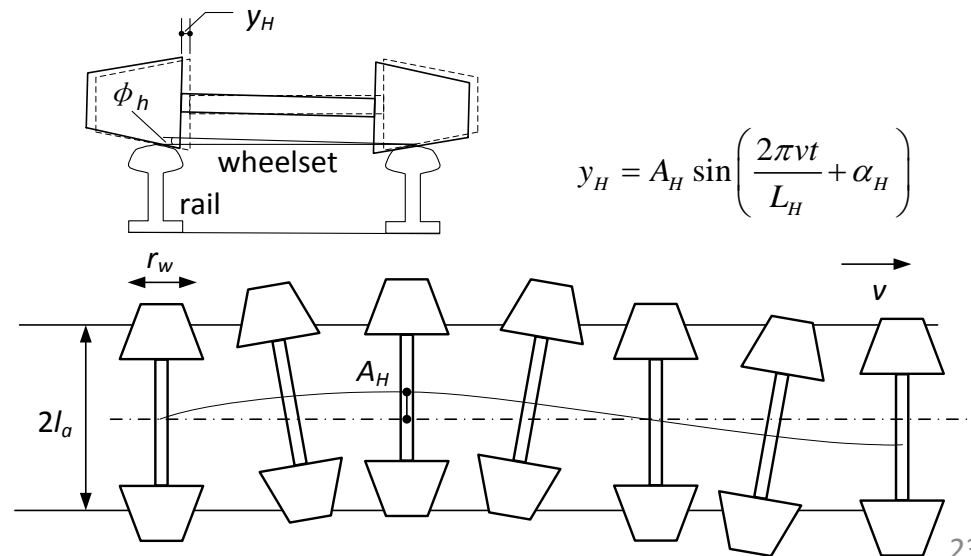
$$\mathbf{M}^*(t)\ddot{\mathbf{u}}(t) + \mathbf{C}^*(t)\dot{\mathbf{u}}(t) + \mathbf{K}^*(t)\mathbf{u}(t) = \mathbf{F}^*(t)$$

sources of excitation

- **external excitation:** earthquake ground motion, wind loading etc.
- **Coriolis and centrifugal forces:** curved bridges and/or curved rails
- **self-excitation :** wheel-hunting, creep forces, rail irregularities



$$r_c = \sqrt{2} \sum_{n=1}^{N_c} A_n \cos(\omega_n s^i + \alpha_n)$$



$$y_H = A_H \sin\left(\frac{2\pi vt}{L_H} + \alpha_H\right)$$



proposed analysis platform

finite element software
multibody software



in-house algorithm



pre-processing

ANSYS → bridge FEM model
(\mathbf{M}^B , \mathbf{C}^B and \mathbf{K}^B)

Workbench → vehicle multibody model
($\mathbf{M}^V(t)$, \mathbf{C}^V and \mathbf{K}^V)



processing

system **global matrices**
(mass/stiffness/damping)

\mathbf{M}^* , \mathbf{C}^* and \mathbf{K}^*



perform VBI **analysis**
in MATLAB →
time-history solutions

time-history
solutions



post-processing

deformed shapes,
member forces diagrams

ANSYS → **bridge**
Workbench → **vehicle**



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results – frequent earthquakes

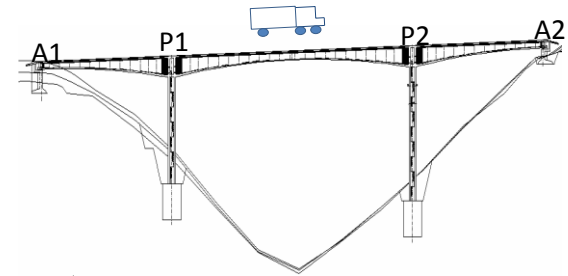
results – rare earthquakes

conclusions

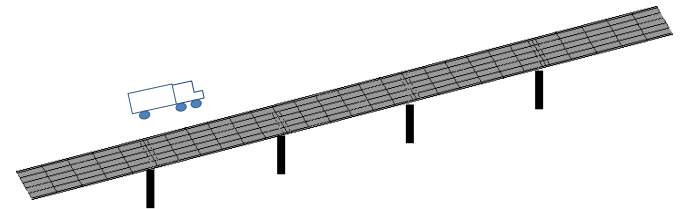


case studies

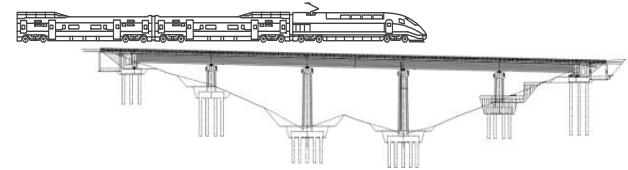
straight continuous highway bridge
interacting with trucks during earthq. (2D)



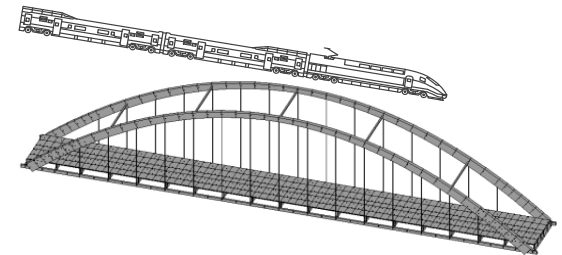
straight continuous slab highway bridge
interacting with trucks no earthq. (3D)



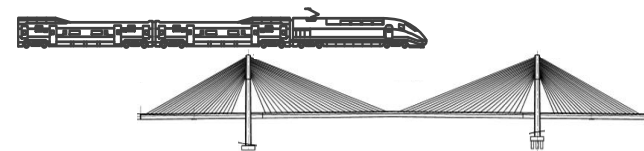
curved continuous railway bridge
interacting with train during earthq. (3D)



straight steel arch truss railway bridge
interacting with train no earthq. (3D)



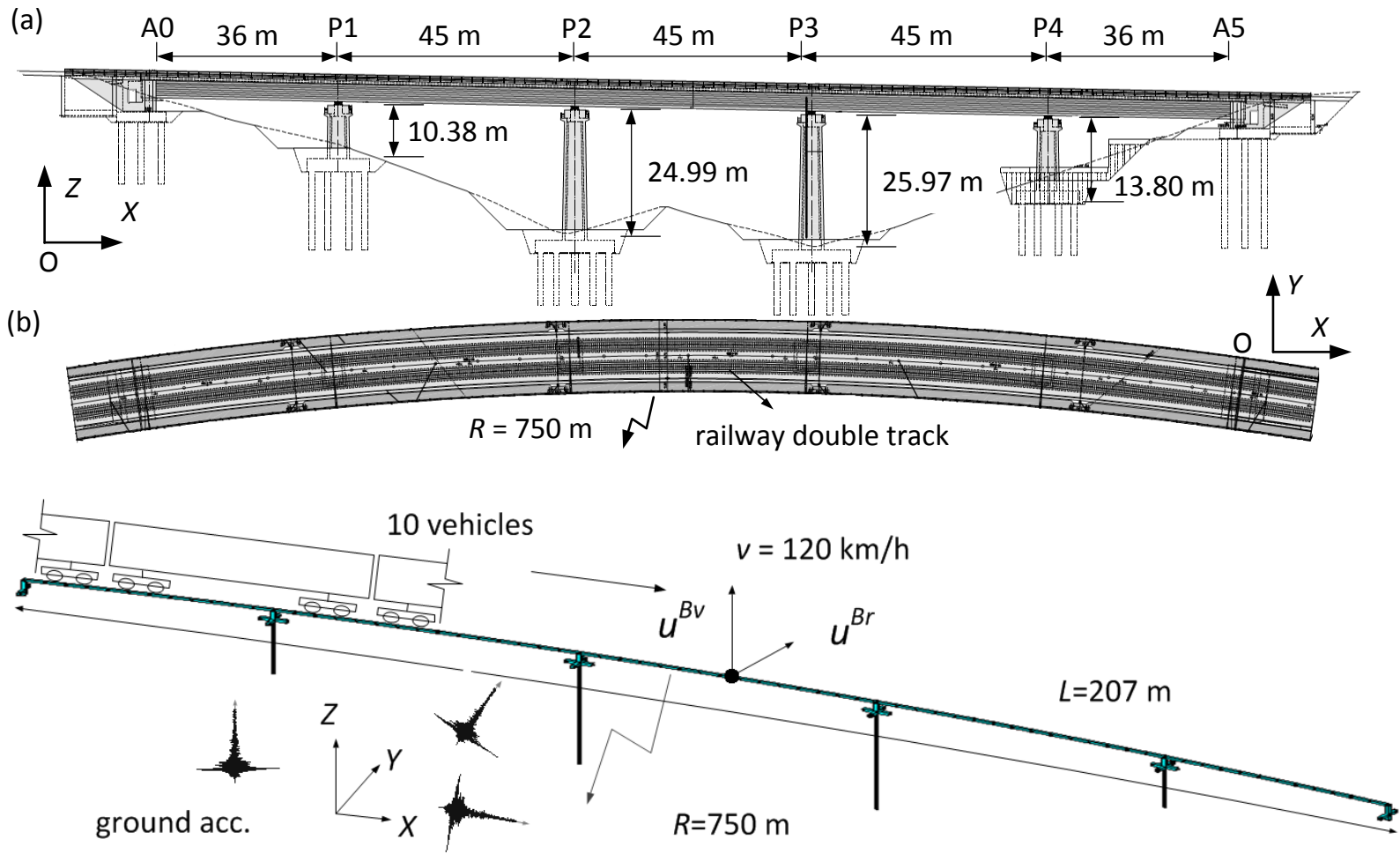
straight cable-stayed bridge
interacting with train no earthq. (3D)





SVBI frequent earthquakes

horizontally curved continuous bridge





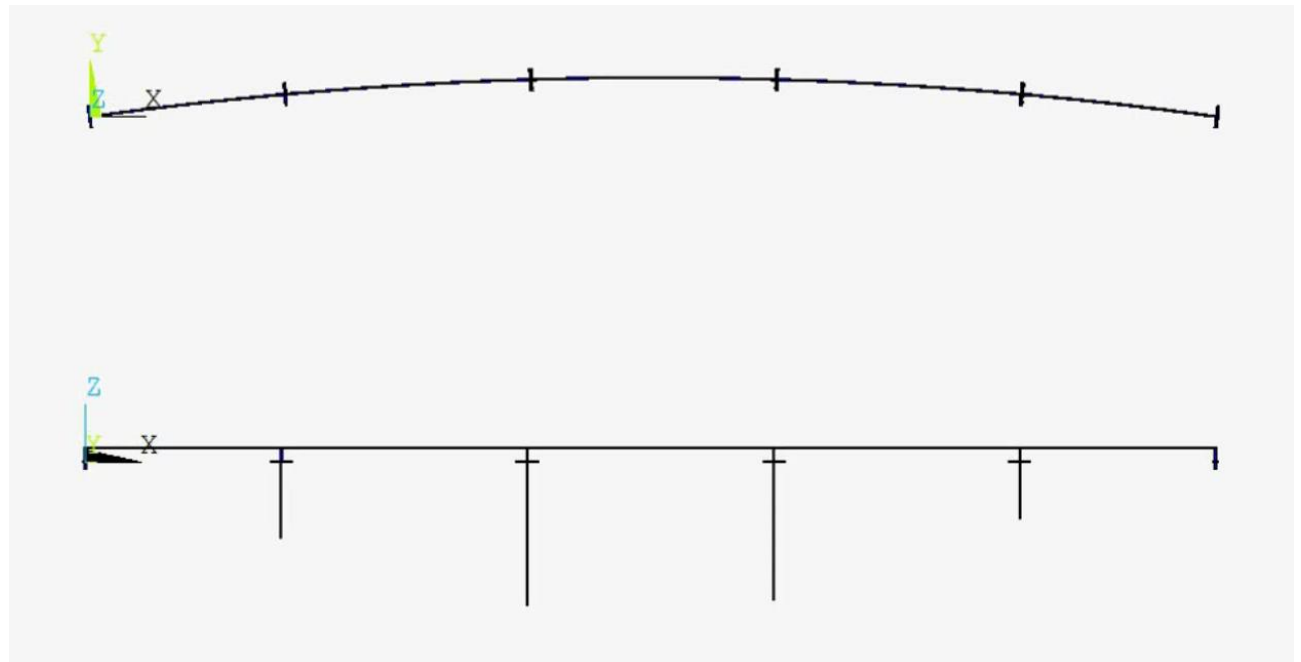
SVBI frequent earthquakes

horizontally curved continuous bridge

deformation animation of the whole bridge

- 10 passing vehicles, **without** earthquake

top view



elevation view



SVBI frequent earthquakes

horizontally curved continuous bridge

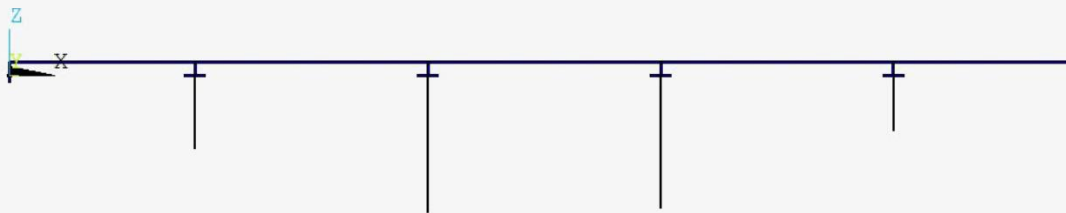
deformation animation of the whole bridge

- 10 passing vehicles, **with** earthquake

top view



elevation view



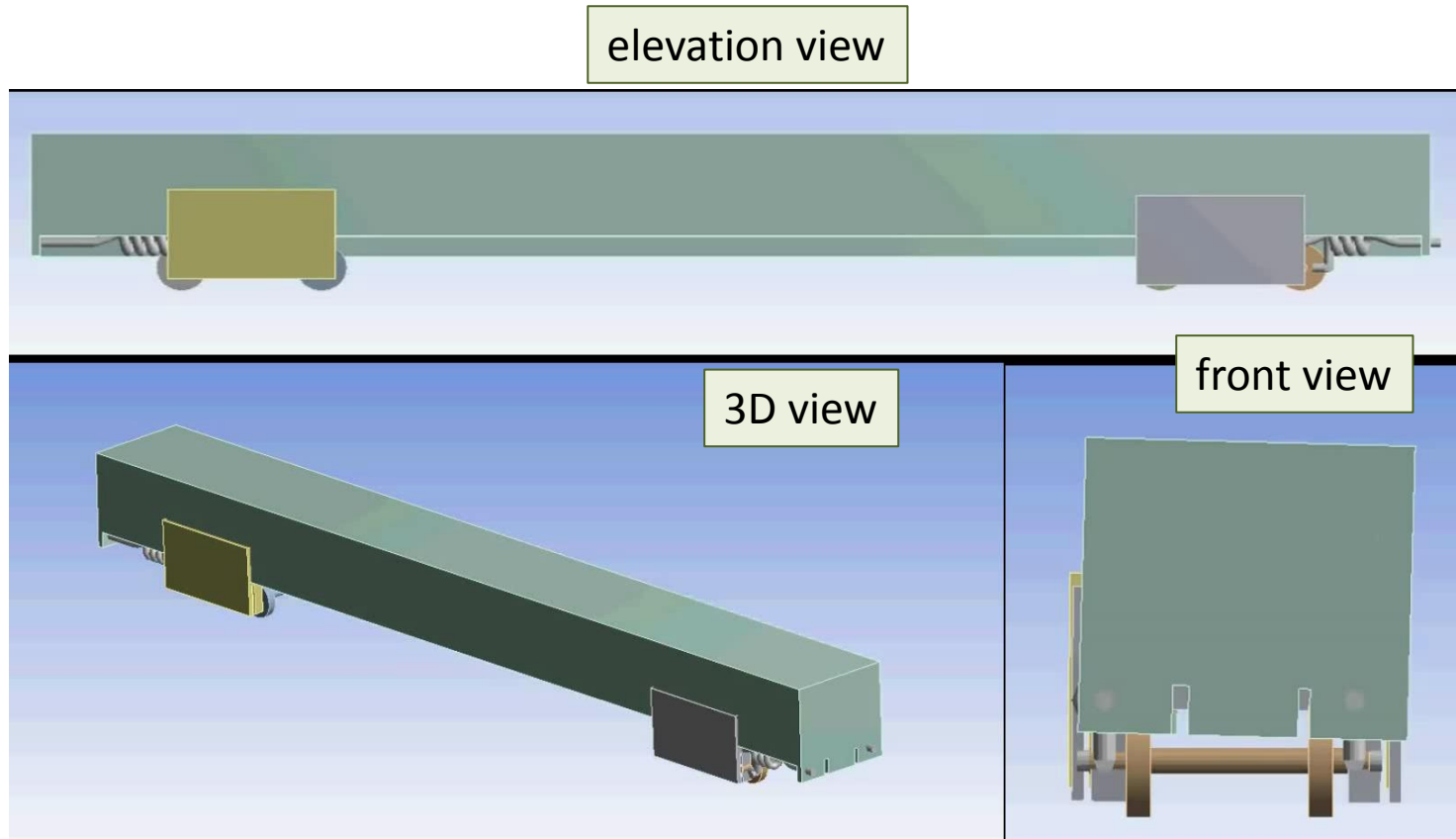


SVBI frequent earthquakes

horizontally curved continuous bridge

deformation animation of the vehicle

- 10 passing vehicles, **with** earthquake



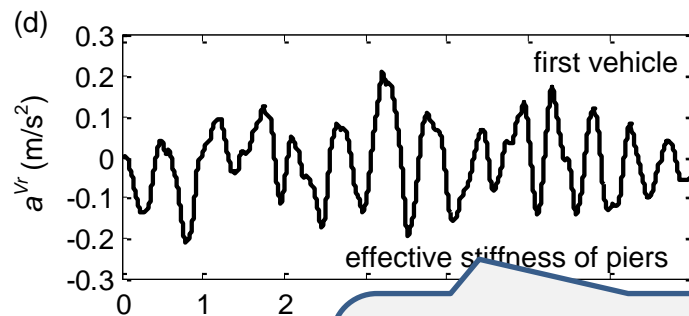
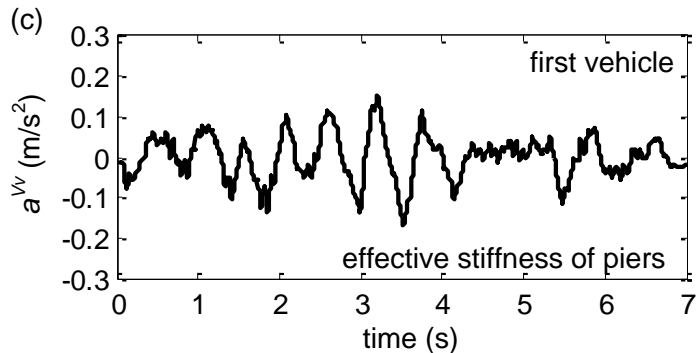
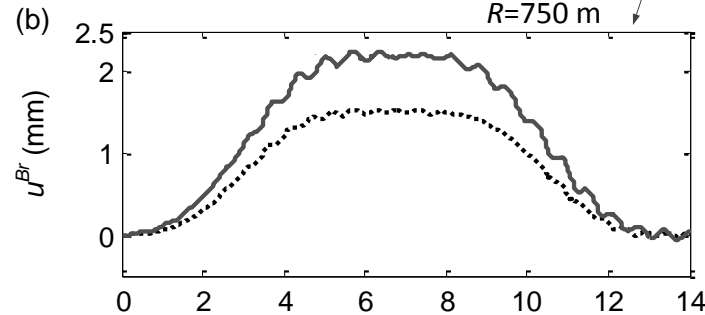
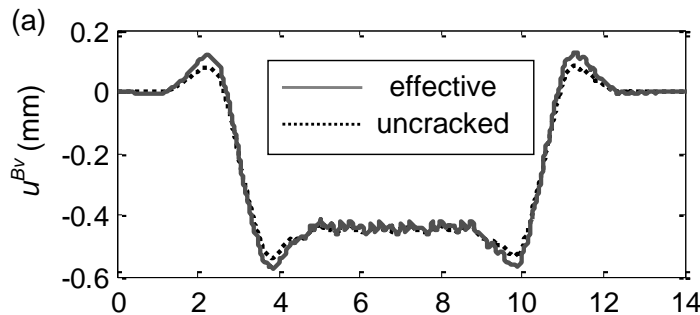
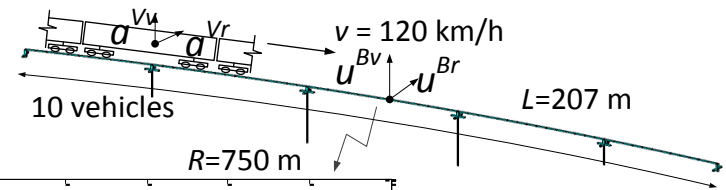


SVBI frequent earthquakes

horizontally curved continuous bridge

- VBI model
- no earthquake excitation
- u : displacement • a : acceleration

- vertical and radial disp. of bridge midpoint
- vertical and radial accel. of vehicle car-body



riding comfort of the passengers
 → acceleration of the car-body

- vertical ≤ 2.0 m/s²
- radial (lateral) ≤ 1.5 m/s²

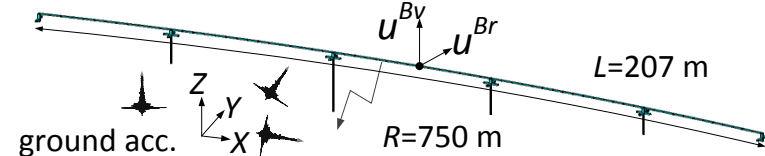


SVBI frequent earthquakes

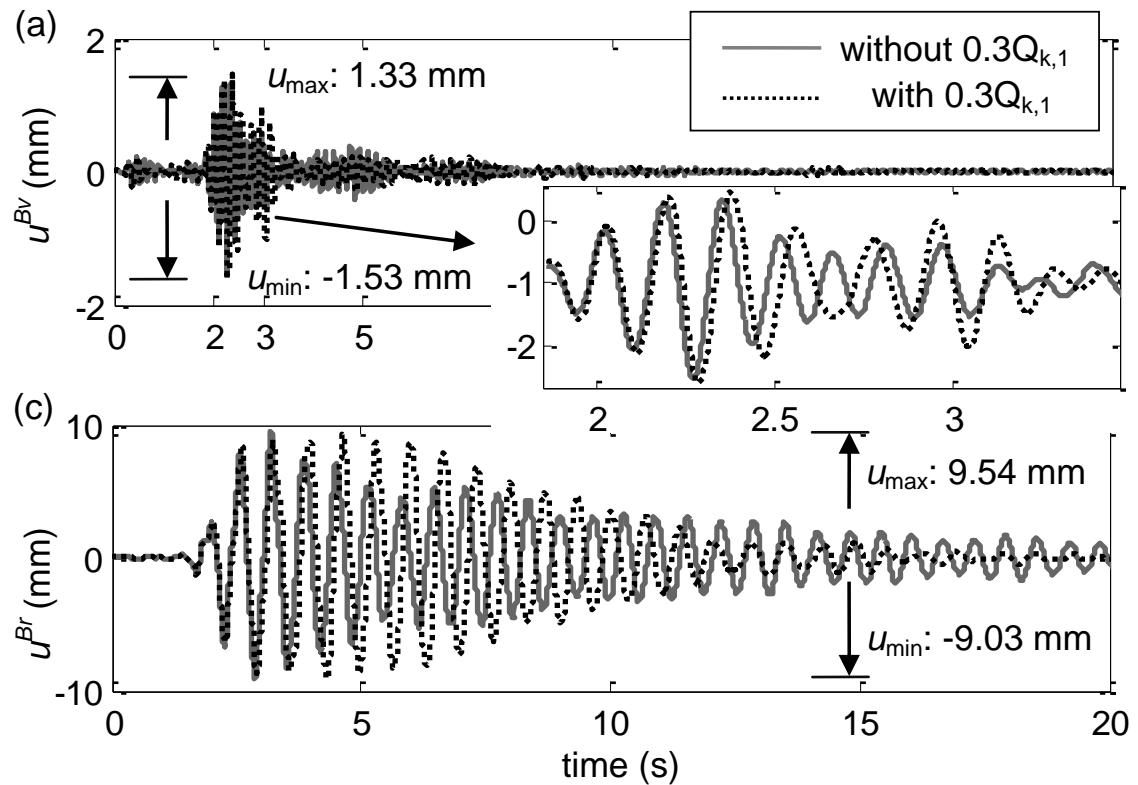
horizontally curved continuous bridge

- vertical and radial disp. of bridge midpoint

- no passing vehicles
- earthquake excitation in 3 directions
- u : displacement



• $0.3Q_{k,1}$: the additional mass due to traffic



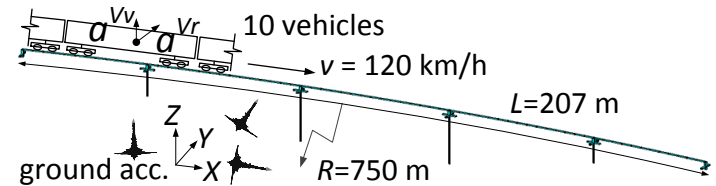


SVBI frequent earthquakes

horizontally curved continuous bridge

- vertical and radial accel. of car-body
- accel. of the vehicle on bridge
> accel. of the vehicle on ground

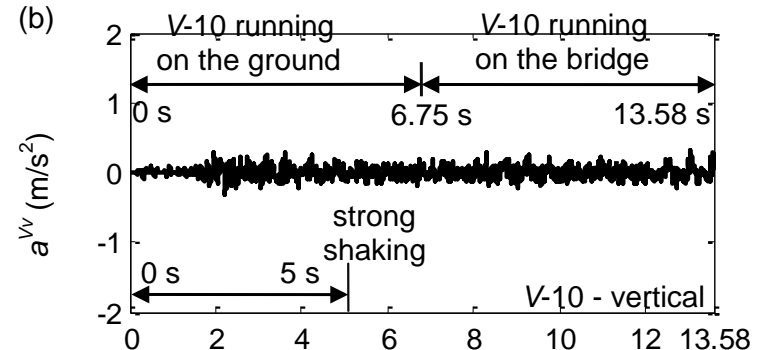
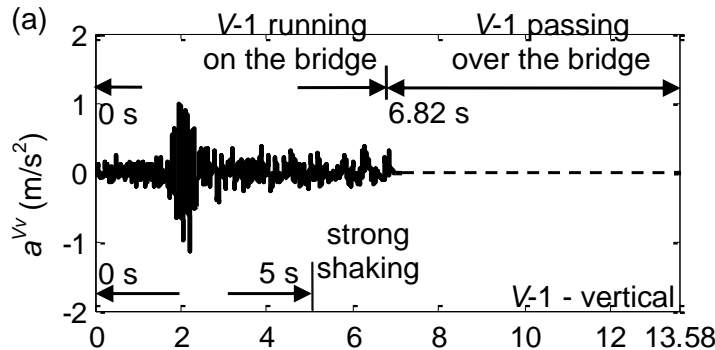
- VBI model
- earthquake excitation in 3 directions
- a : acceleration
- V-1 and V-10: the first and tenth vehicle



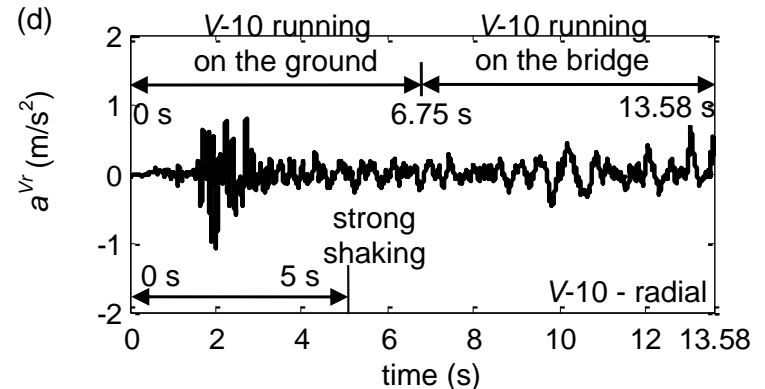
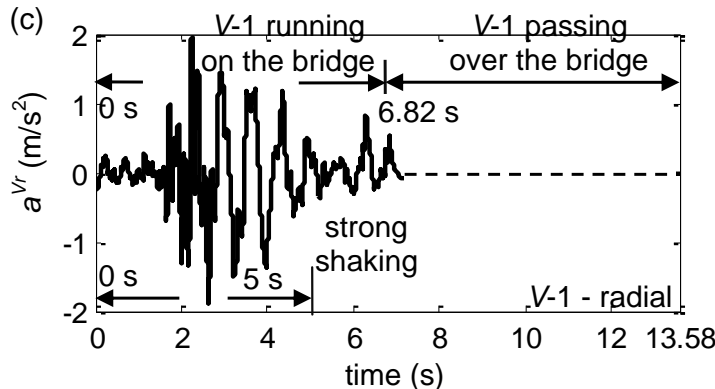
1st vehicle

10th vehicle

vertical



radial





SVBI frequent earthquakes

horizontally curved continuous bridge

Table I. Properties of the examined earthquakes.

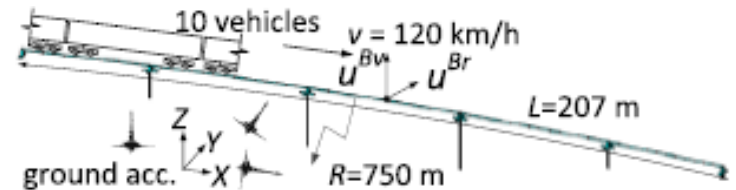
number	name	Station	Epic. Dist.		Dur. (s)	X PGA (g)	Y PGA (g)	Z PGA (g)
			Mag.	(km)				
1	Coyote Lake	CDMG Station 1492	5.74	26.85	26.83	0.07	0.11	0.04
2	Livermore	CDMG Station 67070	5.42	31.54	30.00	0.11	0.05	0.01
3	San Francisco	CDMG Station 1117	5.28	27.03	25.50	0.10	0.11	0.05
4	Trinidad	CDMG Station 1498	5.7	71.24	21.45	0.17	0.13	0.03
5	Jiashi	Xiker, Northwest China	5.8	39.73	40.00	0.14	0.08	0.05
6	Chalfant Valley	CDMG 54100	5.77	27.03	39.97	0.06	0.05	0.03
7	Matata, New Zealand	Edgecumbe substation	5.7	45.76	29.50	0.04	0.04	0.04
8	Yorba Linda	La Harba & Monte Vista	4.27	16.63	43.00	0.03	0.04	0.01
9	Northwest Calif-01	Ferndale City Hall	5.5	43.28	40.00	0.15	0.09	0.03
10	Lytle Creek	Cedar Springs Pumphouse	5.33	22.94	10.22	0.06	0.07	0.04
11	Almiros-01, Greece	Almiros	5.2	14.76	22.59	0.07	0.07	0.07
12	Hollister-04	CDMG 47189	5.45	11.35	80.00	0.04	0.09	0.05
13	Nakagawa	HKD025	4.2	7.00	70.00	0.11	0.10	0.03
14	San Francisco	Golden Gate Park	5.28	11.02	39.72	0.09	0.10	0.03
15	Managua Nicaragua-02	Managua ESSO	5.2	4.33	48.00	0.26	0.22	0.18
16	Oroville-04	Medical Center	4.37	10.50	12.52	0.08	0.05	0.03
17	Oroville-03	DWR Garage	4.7	6.03	13.60	0.11	0.22	0.09
18	Imperial Valley-07	Calexico Fire Station	5.01	13.32	19.42	0.10	0.07	0.03
19	Almiros-02, Greece	Almiros	5.2	13.25	22.60	0.07	0.07	0.09
20	Mammoth Lakes-10	Convict Creek	5.34	6.50	40.00	0.16	0.15	0.10



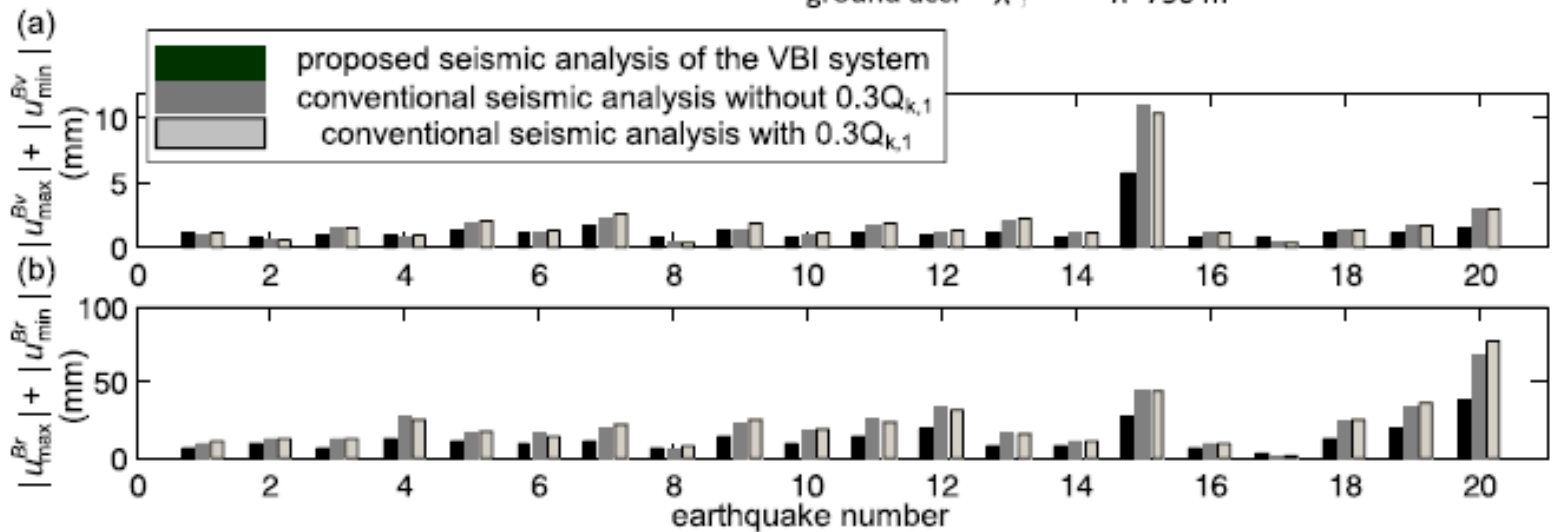
SVBI frequent earthquakes

horizontally curved continuous bridge

- VBI model
- earthquake excitation in 3 directions
- u : displacement
- max: maximum • min: minimum



vertical



- vertical and radial disp. of bridge midpoint
- the conventional seismic analysis overestimates the response of the bridge
- the multibody vehicle acts as a additional damping to the bridge and reduce its response



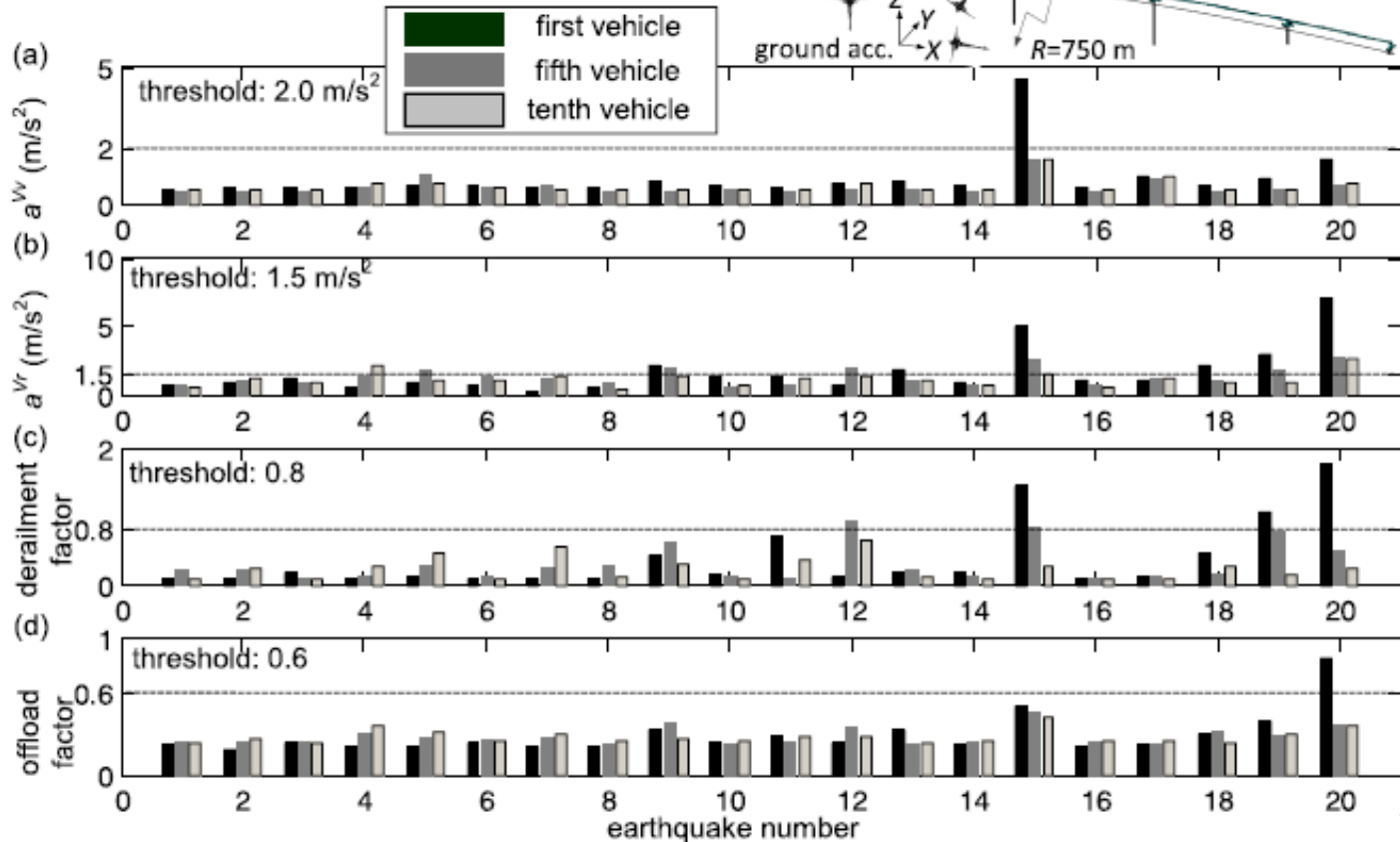
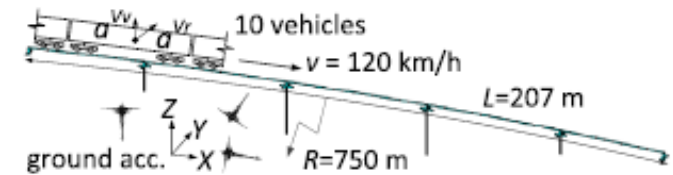
SVBI frequent earthquakes



horizontally curved continuous bridge

- 20 different earthquakes
- comfort: vertical and radial accel. of car-body
- safety: derailment and offload factor

- VBI model
- earthquake excitation in 3 directions
- a: acceleration



comfort:

safety

Derail factor

$$= \frac{\lambda_{Ti}}{\lambda_{Ni}}$$

Offloading factor

$$= \frac{|\lambda_{Nli} - \lambda_{Nri}|}{\lambda_{Nli} + \lambda_{Nri}}$$



outline

motivation

proposed model

results – frequent earthquakes

results – rare earthquakes

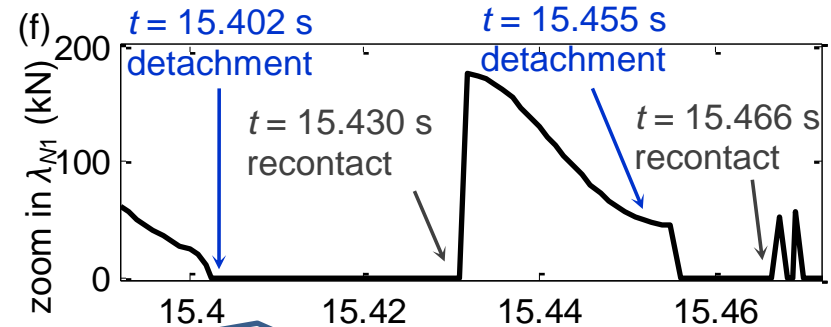
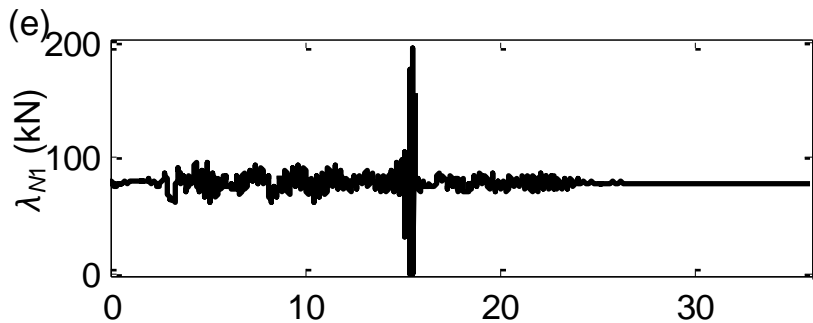
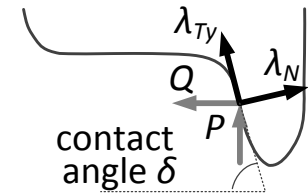
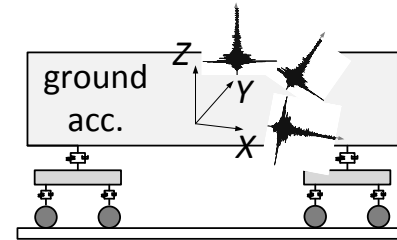
conclusions



SVBI rare earthquakes

horizontally curved continuous bridge

- a^{Vr} and a^{Vv} : radial and vertical accel. of car body
- u^{Vr} and $u^{V\phi}$: vertical and rolling disp. of car body
- λ_{N1} : normal contact force of wheel 1
- P and Q : dynamic vertical and horizontal force



- contact: nonzero normal contact force
- detachment: zero normal contact force

- three components of the ground motion recorded on April 25, 1992 in Cape Mendocino USA, at Petrolia station (0.59g, 0.66g, 0.19g)

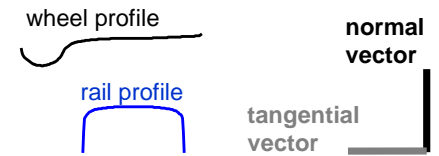
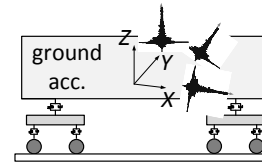


SVBI rare earthquakes

separation sequence

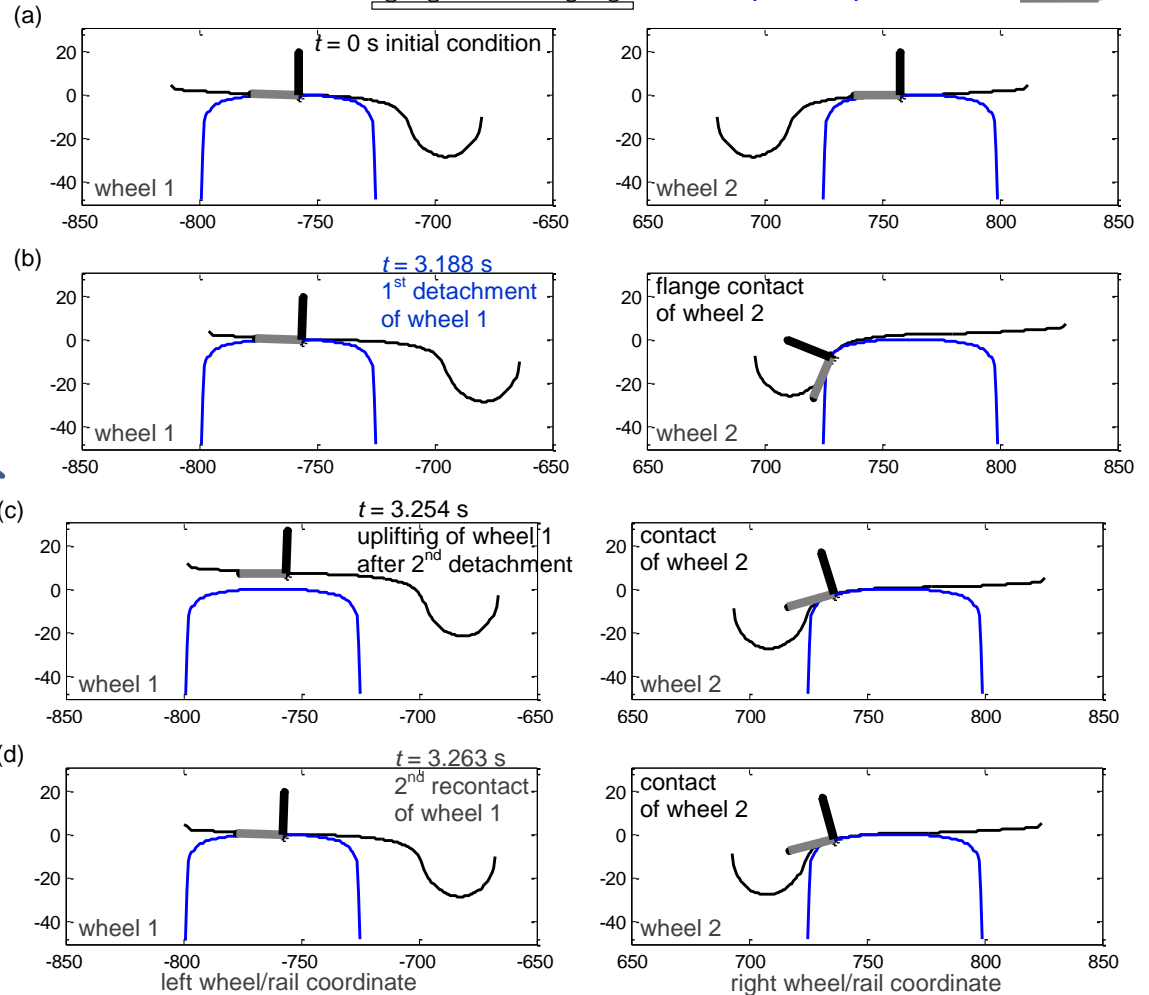
list of state change of wheel 1

- $t = 3.188$ s 1st detachment
- $t = 3.228$ s 1st recontact
- $t = 3.232$ s 2nd detachment
- $t = 3.263$ s 2nd recontact



separation

- no need for high lateral accelerations



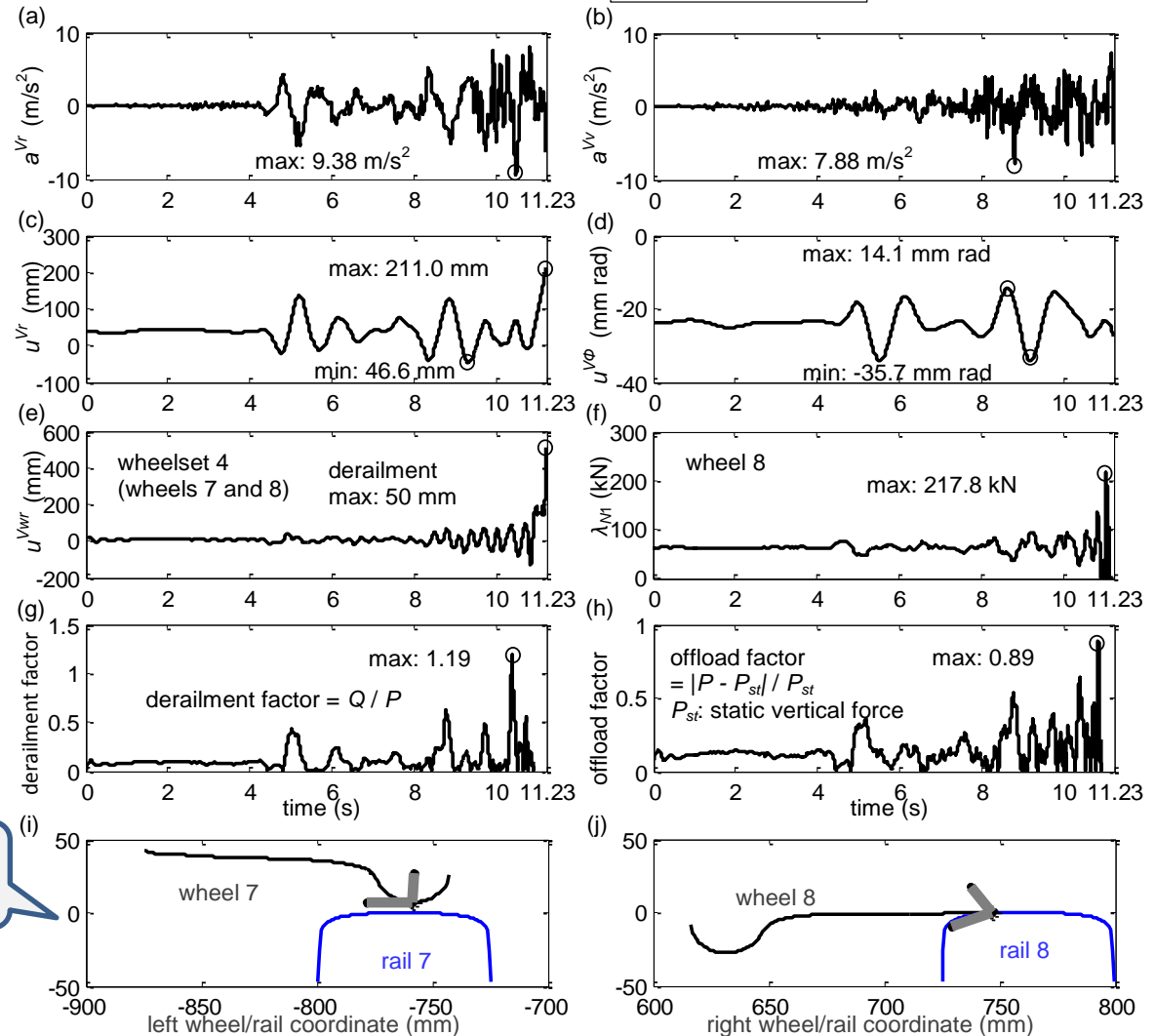
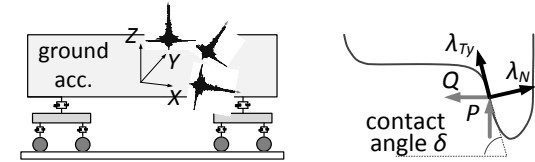


SVBI rare earthquakes



separation sequence

- a^{Vr} and a^{Vv} : radial and vertical accel. of car body
- u^{Vr} and $u^{V\phi}$: vertical and rolling disp. of car body
- u^{Vwr} : radial disp. of the wheelset
- λ_{N1} : normal contact force of wheel 1
- P and Q : dynamic vertical and horizontal force



derailment



outline

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results – frequent earthquakes

results – rare earthquakes

conclusions



conclusions

- scheme for seismic response of interacting vehicle and horizontally **curved** bridges
- the mass / stiffness / damping matrix of the coupled vehicle-bridge system become **time-dependent**
- the scheme accommodates easily different number of vehicles, and with various DOFs
- the seismic response of the bridge affects (adversely) the safety of the vehicle
- Vehicles-bridge-earthquake **timing** problem
- lack of **performance** (comfort and safety) **criteria** for vehicles → probabilistic
- complicated dynamics, multi-parametric problem



references

list of relevant journal publications

1. Zeng Q., **Dimitrakopoulos** E.G. (2016) "Seismic Response Analysis of an Interacting Curved Bridge-Train System Under Frequent Earthquakes" *Earthquake Engineering and Structural Dynamics*, published online, 13 Jan 2016 DOI 10.1002/eqe.2699
2. Zeng Q., Yang Y.B., **Dimitrakopoulos** E.G. (2016) "Dynamic response of high speed vehicles and sustaining curved bridges under conditions of resonance" *Engineering Structures*, published 1 May 2016, vol. 114 pp 61-74, DOI: 10.1016/j.engstruct.2016.02.006
3. **Dimitrakopoulos** E.G. & Zeng Q. (2015) "A Three-dimensional Dynamic Analysis Scheme for the Interaction between Trains and Curved Railway Bridges" *Computers & Structures*, vol. 149 43-60.
4. Paraskeva T.S., **Dimitrakopoulos** E.G., Zeng Q., (2016) "Dynamic Vehicle-Bridge Interaction Under Simultaneous Vertical Earthquake Excitation" *Bulletin of Earthquake Engineering*, accepted 28/5/2016





thank you for your kind attention!



low-cost high impact bamboo bridges





case studies and results

steel arch truss bridge

Ting Sihe Bridge of High-speed railway line in China



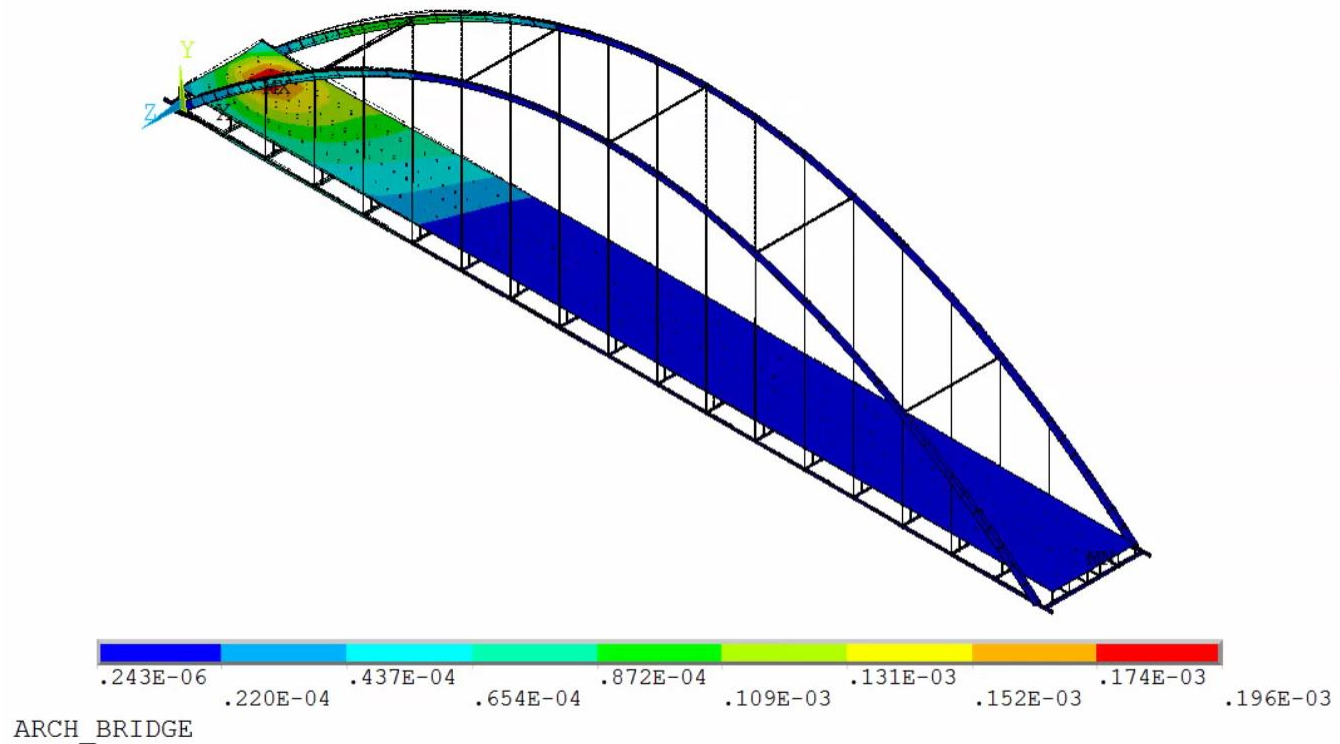
<http://campus.liepin.com/tsy/enterprisefeatures> (2015)



case studies and results

steel arch truss bridge

- deformed shape of the whole bridge
- 1 vehicle: speed of train = 300 km/h





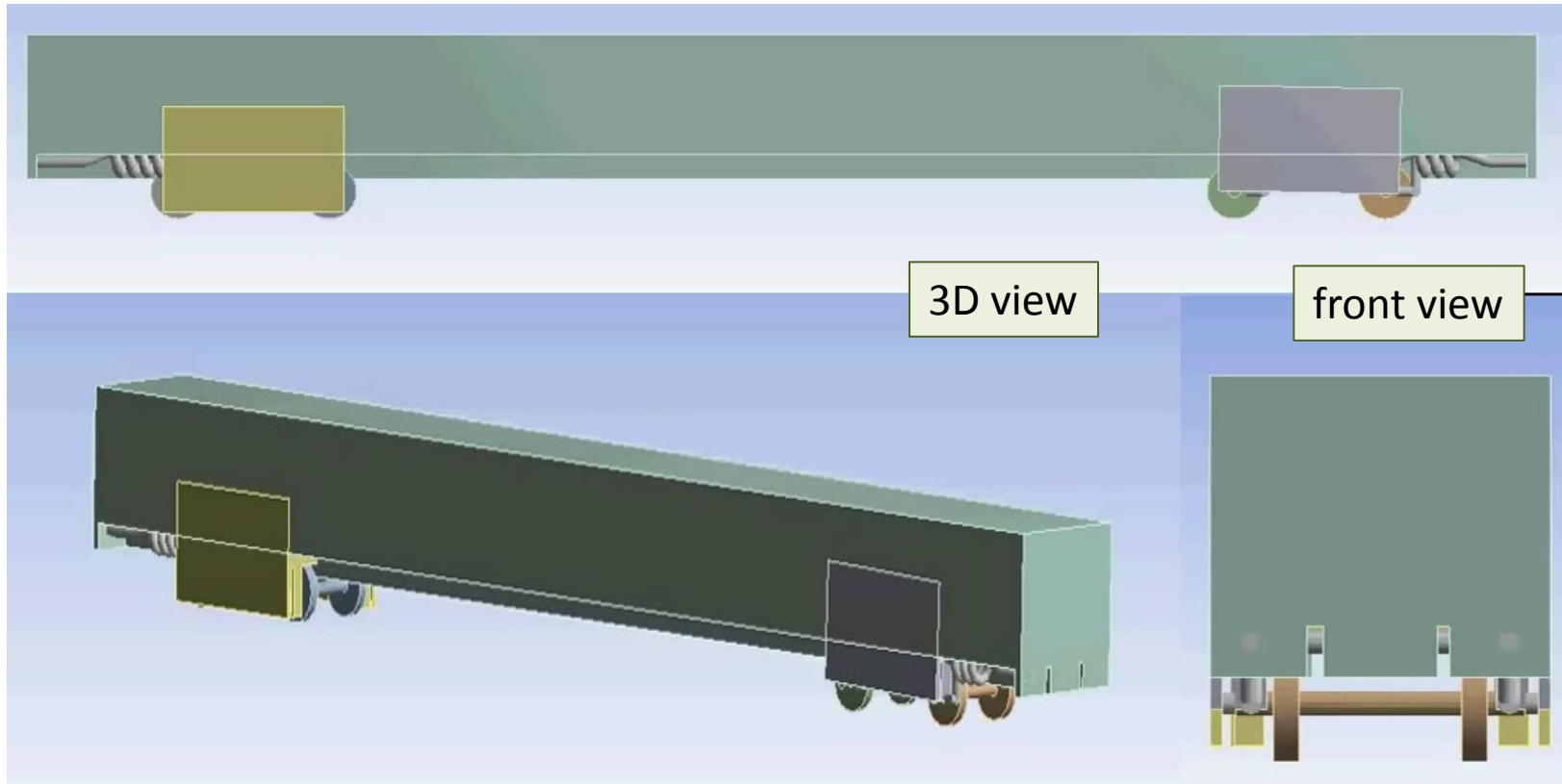
case studies and results

steel arch truss bridge

deformation animation of the vehicle

- 1 vehicle: speed of train = 300 km/h
- vibration due to the **track irregularities**

elevation view



3D view

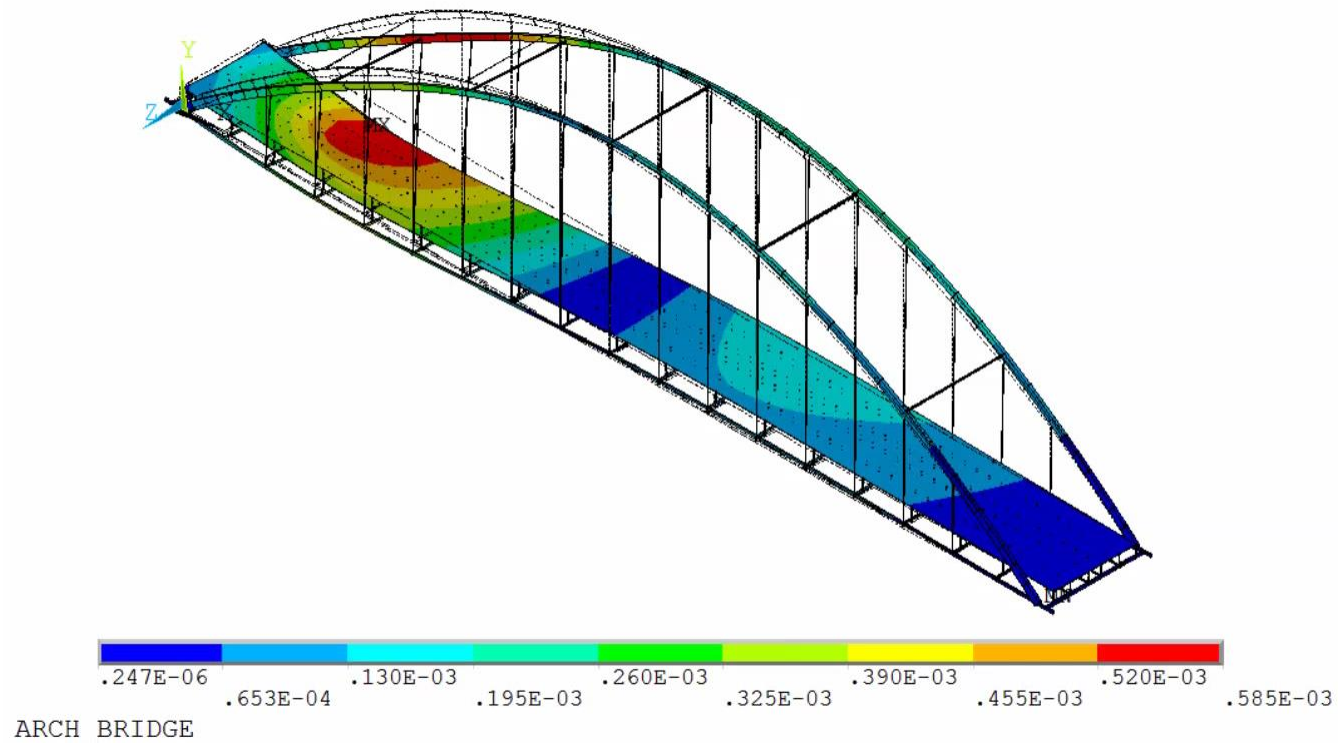
front view



case studies and results

steel arch truss bridge

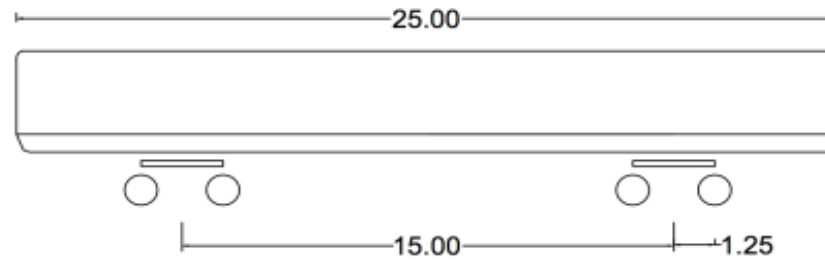
- deformed shape of the whole bridge
- 10 vehicle: speed of train = 300 km/h





case studies and results

cable-stayed bridge with the passage of MTR



Kap Shui Mun Bridge (KSMB) in **Hong Kong**



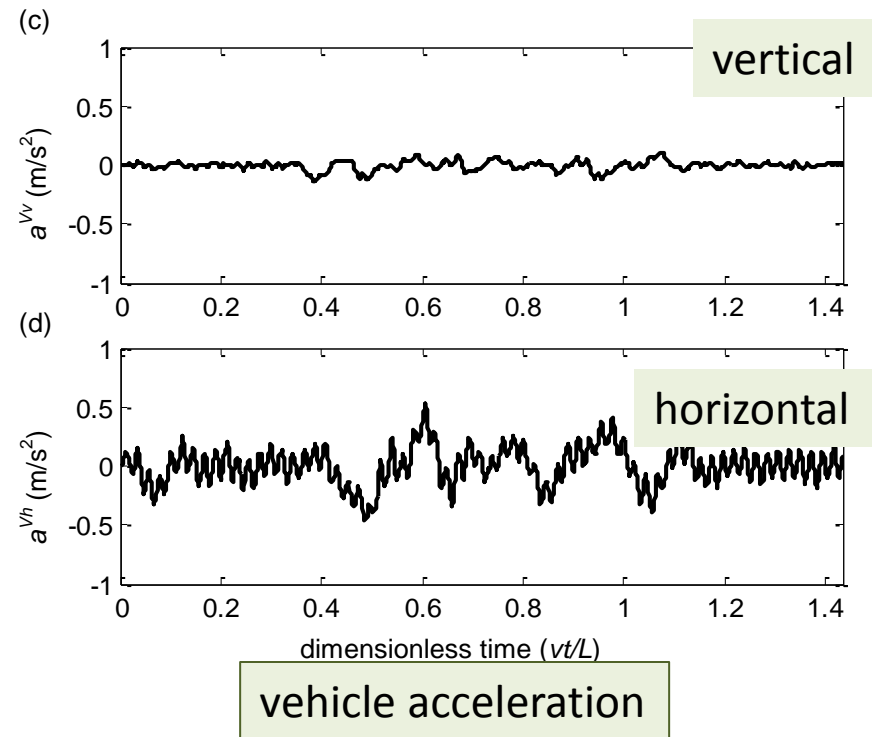
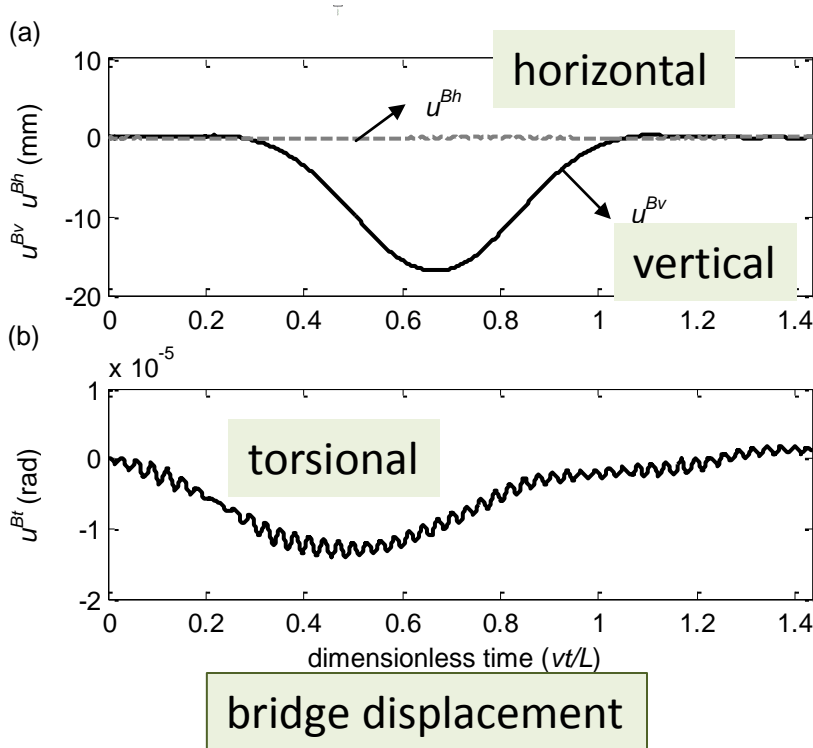
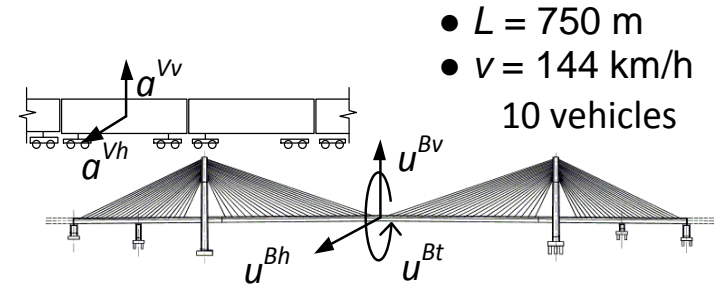
http://en.wikipedia.org/wiki/Kap_Shui_Mun_Bridge



case studies and results

cable-stayed bridge with the passage of MTR

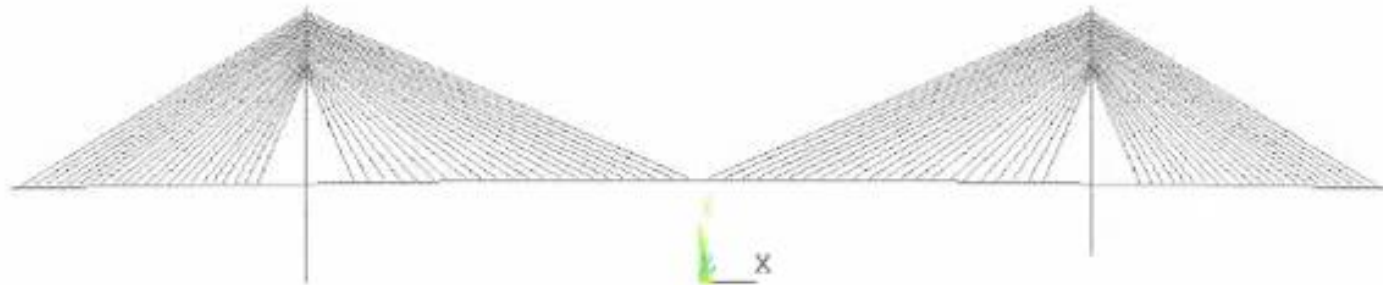
- (a) and (b) bridge midpoint **vertical horizontal** and **torsional displacements**
- (c) and (d) vehicle **vertical** and **horizontal accelerations**





case studies and results

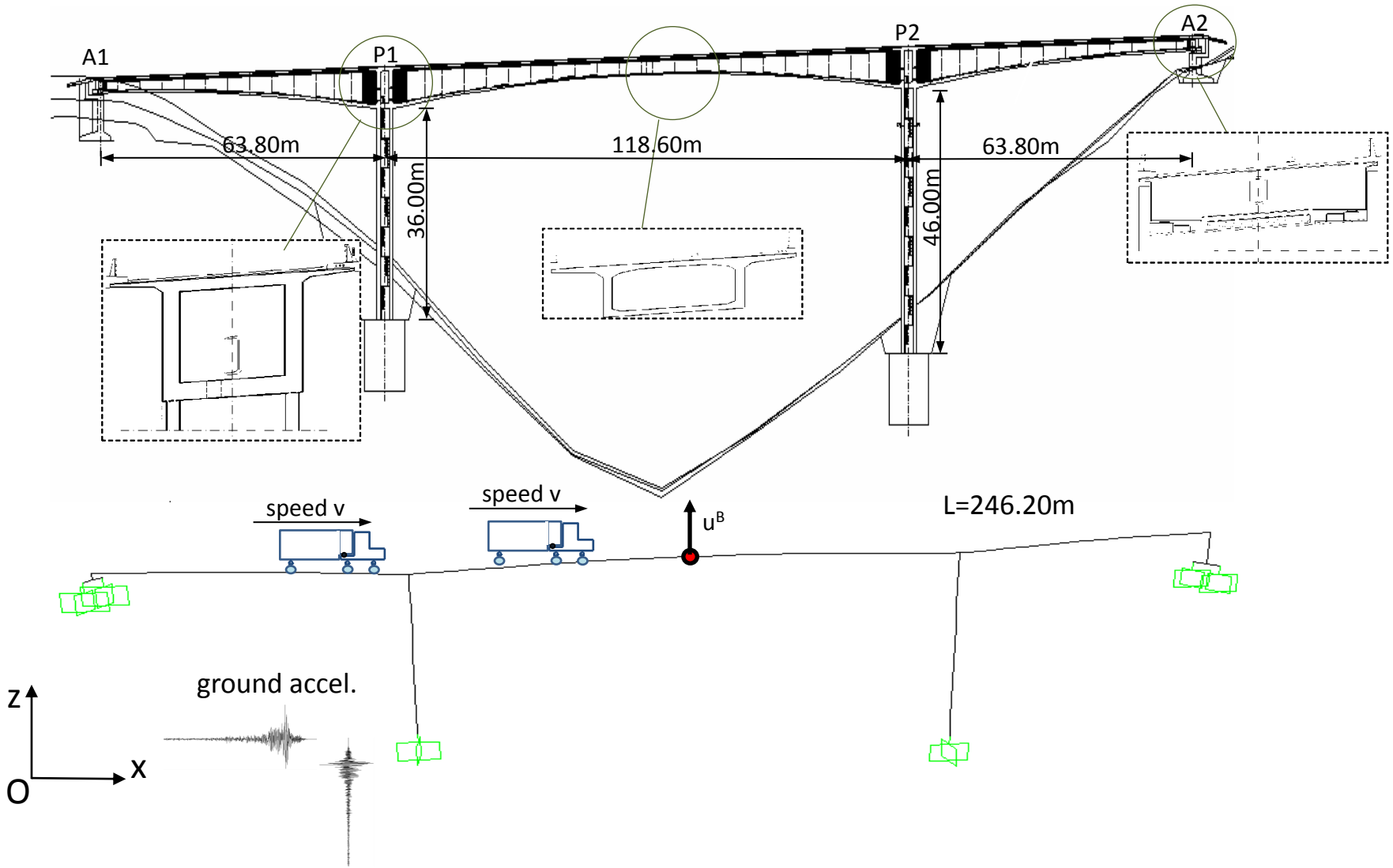
cable-stayed bridge with the passage of MTR





case studies and results

straight highway bridge

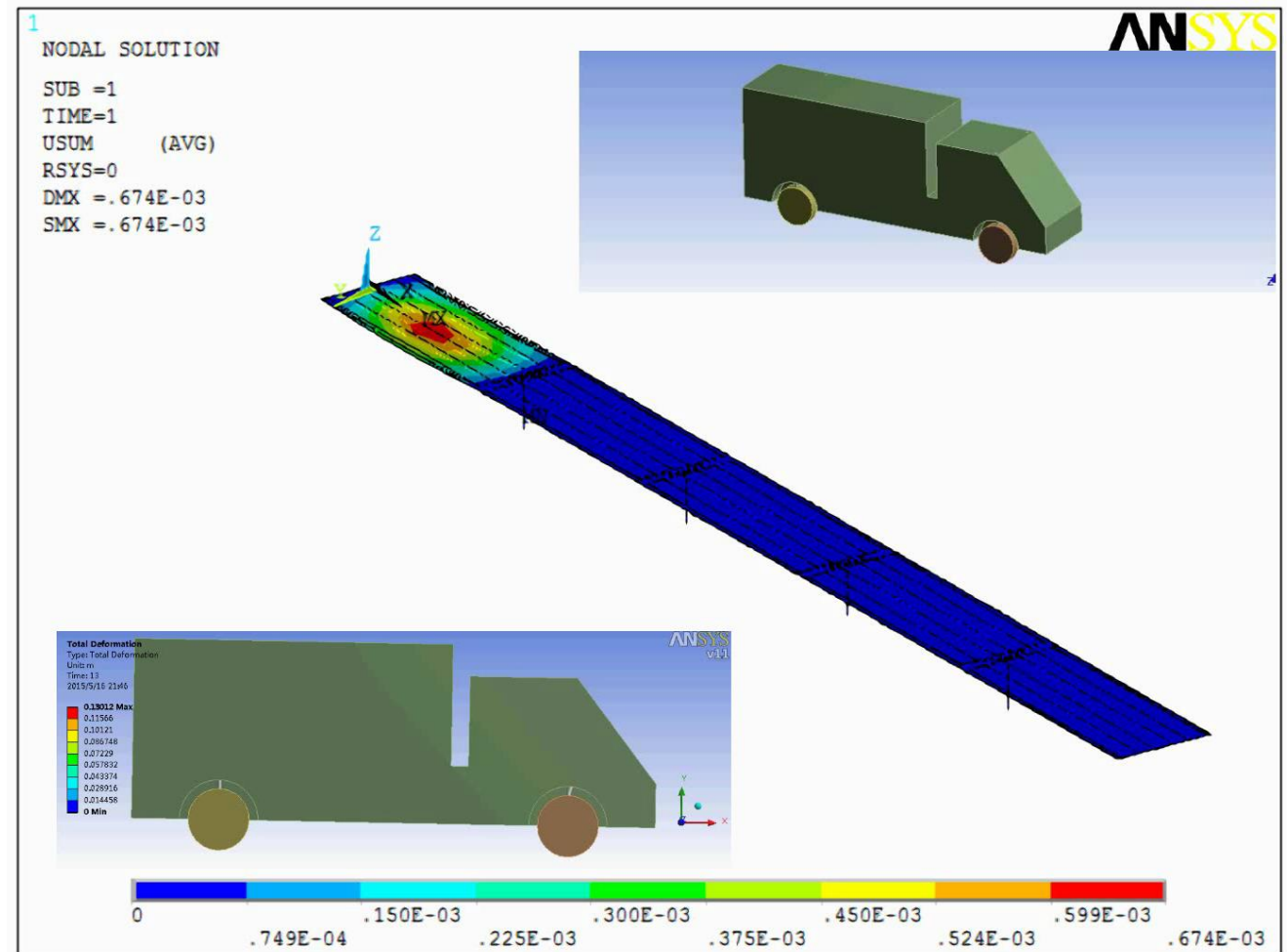




case studies and results

5-span highway continuous bridge with the passage of trucks

- deformed shape of the whole bridge and the vehicle
- 1 vehicle: speed of truck = 80 km/h





case studies and results

5-span highway continuous bridge with the passage of trucks



- deformed shape of the whole bridge
- 5 vehicle: speed of truck = 80 km/h

