

Παράρτημα ΣΤ

Πρόγραμμα μητρικής μελέτης κατασκευής *gril3d*

Στο παράρτημα αυτό περιλαμβάνεται ο πηγαίος κώδικας προγράμματος επίλυσης κατασκευών στην ελαστική περιοχή, με τη μητρική μέθοδο (μέθοδο των μετατοπίσεων). Περιλαμβάνονται επίσης παραδείγματα αρχείων εισόδου και αντίστοιχων αποτελεσμάτων το πρόγραμμα.

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C . . . . .
C
C           Linear Elastic Analysis of a 3-D Grillage
C
C           using the Matrix Stiffness Method
C
C           This program was developed by Dr. P.A. Caridis
C           Department of Naval Architecture and Marine
C           Engineering, NTUA, Athens
C           April 1991.
C
C . . . . .
C
C   - Program gril3d.f can be used to analyse the response
C     of a 3-D structure with up to 100 joints. This
C     corresponds to a rectangular grillage having 8 beams
C     in each direction. Array sizes have to be modified
C     should larger structures be considered.
C   - The properties of each beam are allowed to vary
C     although the geometrical and material particulars are
C     assumed constant between joints.
C
C . . . . . C
C   REAL IZ,IY,K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ,
C   &LENXZ,LEN1,NU
C   COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
C   &),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
C   &KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
C   &,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
C   &,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100
C   &,5),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
C   &2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PPIX
C   &(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
C   &LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)
C   COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
C   &N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
C   &DOF,IOUT(100),IYLD(100,5),ISPAC
C   COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),TW(
C   &100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TORC(1
C   &00),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),ZY(
C   &100),UDL(100),YS(100)
C
C . . . . .
C
C   OPEN(5, FILE='gril3.dat')
C   OPEN(6, FILE='gril3.out')
C
C   Initialisations
C
C

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CALL INITL

C
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L e g e n d

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READ(5,*) ISPAC,MNO,JNO,NUMSEC
READ(5,*) NLOAD,NUDL,ISUPNO,IOMAX
READ(5,*) (I,XJC(I1),YJC(I1),ZJC(I1),I1=1,JNO)
READ(5,*) (I,E(I1),NU(I1),YS(I1),B(I1),TP(I1),HW(I1),
&TW(I1),BF(I1),TF(I1),I1=1,NUMSEC)
  READ(5,*) (IMEM,ISEC(I1),J1(I1),J2(I1),
&ANG(I1),I1=1,MNO)
  IF(NLOAD.NE.0) READ(5,*) (JNT,IDOF,PJNT(JNT,
&IDOF),LOD=1,NLOAD)
  IF(NUDL.NE.0) READ(5,*) (IMEM,UDL(IMEM),LOD=1,NUDL)
DO 1 ISUP=1,ISUPNO
  READ(5,*) JNT,IDOF
    
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1   ID(JNT, IDOF)=1
   DO 2 I=1, IOMAX
   READ(5, *) J
2   IOUT(J)=1
   DO 3 IMEM=1, MNO
   DO 3 I=1, 5
3   IYLD(IMEM, I)=0
C
C
C . . . . .
C
C
C   Length and orientation angle of each member
C
   DO 4 I=1, MNO
   J=J1(I)
   X1(I)=XJC(J)
   Y1(I)=YJC(J)
   Z1(I)=ZJC(J)
   J=J2(I)
   X2(I)=XJC(J)
   Y2(I)=YJC(J)
4  Z2(I)=ZJC(J)
C
   DO 5 I=1, MNO
   LX(I)=X2(I)-X1(I)
   LY(I)=Y2(I)-Y1(I)
   LZ(I)=Z2(I)-Z1(I)
   XX=LX(I)*LX(I)+LY(I)*LY(I)
   XY=XX+LZ(I)*LZ(I)
   L(I)=SQRT(XY)
   XZ=LX(I)*LX(I)+LZ(I)*LZ(I)
   LENXZ(I)=SQRT(XZ)
   LEN1(I)=L(I)*LENXZ(I)
   IF(ISPAC.EQ.1) GO TO 5
   RATIO=LY(I)/L(I)
   ANG(I)=ASIN(RATIO)
5  CONTINUE
   NDOF=6*JNO
C
C   Geometrical properties of all sections
C
   CALL PROPS
C
C   Echo of input data
C
   CALL INPUT
C
C . . . . .
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C      Assemble member stiffness matrices
C
      DO 20 IMEM=1,MNO
      CALL STIF(IMEM,ISEC,E,NU,AREA,L,IZ,IY,TORC,K)
C
C      WRITE(6,39) IMEM
C      WRITE(6,42) (K(I,J),I=1,12),J=1,12)
C
C      Member transformation matrix
C
      CALL ROT(IMEM,ISPAC,ANG,R,T,TT,L,LX,LY,LZ,LEN1,LENXZ)
C
C      -----
C
C      Obtain particular solution with clamped joints for
C      distributed loads
C
      IF(UDL(IMEM).EQ.0.0) GO TO 10
      CALL PARSOL(IMEM)
C
C      Reactions at joints due to UDLs
C
C      a) from member local to member global coords
C
      DO 7 J=1,12
      PMG(IMEM,J)=0.0
      DO 7 I=1,12
7      PMG(IMEM,J)=PMG(IMEM,J)+TT(IMEM,I,J)*PML(IMEM,I)
C
C      b) from member global to joint global loads due to
C      UDLs
C
      JNT1=J1(IMEM)
      JNT2=J2(IMEM)
      DO 8 IDOF=1,6
      PJP(JNT1,IDOF)=PJP(JNT1,IDOF)+PMG(IMEM,IDOF)
      PJP(JNT2,IDOF)=PJP(JNT2,IDOF)+PMG(IMEM,IDOF+6)
      IF(ID(JNT1,IDOF).EQ.1) PFIX(JNT1,IDOF)=PJP(JNT1,IDOF)
      IF(ID(JNT2,IDOF).EQ.1) PFIX(JNT2,IDOF)=PJP(JNT2,IDOF)
      IF(ID(JNT1,IDOF).EQ.1) PJP(JNT1,IDOF)=0.0
8      IF(ID(JNT2,IDOF).EQ.1) PJP(JNT2,IDOF)=0.0
C
C      Column load vector containing reactions to UD loads
C
      DO 9 JNT=1,JNO
      DO 9 IDOF=1,6
      INOD=6*(JNT-1)
9      PP(INOD+IDOF)=PJP(JNT,IDOF)
10     CONTINUE
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C      -----

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C
C   Structural load vector including member UDL loads and
C   joint loads
C
      DO 11 JNT=1,JNO
      DO 11 IDOF=1,6
      INOD=6*(JNT-1)
11   P(INOD+IDOF)=PJNT(JNT, IDOF)-PP(INOD+IDOF)
C
      DO 12 J=1,12
      DO 12 I=1,12
12   KMEM(IMEM,I,J)=K(I,J)
C
C   Transform member stiffness matrix to global coordinate
C   system
C
      CALL STIFGL(IMEM)
C
      DO 13 JNT=1,JNO
      DO 13 IDOF=1,6
      INOD=6*(JNT-1)
13   IDLIN(INOD+IDOF)=ID(JNT, IDOF)
C
C   Partition member stiffness matrix
C
      DO 14 J=1,6
      DO 14 I=1,6
      K11(I,J)=K(I,J)
      K12(I,J)=K(I+6,J)
      K21(I,J)=K(I,J+6)
14   K22(I,J)=K(I+6,J+6)
C
C   WRITE(*,101)IMEM
C   PRINT *,IMEM
      IF(IOUT(IMEM).EQ.0) GO TO 15
C   WRITE(6,45) IMEM
C   WRITE(6,44) ((R(I,J),I=1,3),J=1,3)
C   WRITE(6,46) IMEM
C   WRITE(6,42) ((T(IMEM,I,J),I=1,12),J=1,12)
C   WRITE(6,47) IMEM
C   WRITE(6,42) ((TT(IMEM,I,J),I=1,12),J=1,12)
C   WRITE(6,34) IMEM
C   WRITE(6,42) ((K(I,J),I=1,12),J=1,12)
C   WRITE(6,35) IMEM
C   WRITE(6,43) ((K11(I,J),I=1,6),J=1,6)
C   WRITE(6,36) IMEM
C   WRITE(6,43) ((K12(I,J),I=1,6),J=1,6)
C   WRITE(6,37) IMEM
C   WRITE(6,43) ((K21(I,J),I=1,6),J=1,6)
C   WRITE(6,38) IMEM

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C      WRITE(6,43) ((K22(I,J),I=1,6),J=1,6)
C
C      Form structural stiffness matrix {K} using the direct
C      stiffness method
C
15     JNUM1=J1(IMEM)
        JF=1+6*(JNUM1-1)
        IF=JF
        DO 16 J=JF,JF+5
            JEL=J-JF+1
            DO 16 I=IF,IF+5
                IEL=I-IF+1
16     KS(I,J)=KS(I,J)+K11(IEL,JEL)
C
        JNUM2=J2(IMEM)
        IF=1+6*(JNUM2-1)
        JF=1+6*(JNUM1-1)
        DO 17 J=1,6
            DO 17 I=1,6
                IS=IF-1+I
                JS=JF-1+J
17     KS(IS,JS)=KS(IS,JS)+K12(I,J)
C
        IF=1+6*(JNUM1-1)
        JF=1+6*(JNUM2-1)
        DO 18 J=1,6
            DO 18 I=1,6
                IS=IF-1+I
                JS=JF-1+J
18     KS(IS,JS)=KS(IS,JS)+K21(I,J)
C
        IF=1+6*(JNUM2-1)
        JF=1+6*(JNUM2-1)
        DO 19 J=1,6
            DO 19 I=1,6
                IS=IF-1+I
                JS=JF-1+J
19     KS(IS,JS)=KS(IS,JS)+K22(I,J)
20     CONTINUE
        WRITE(*,102)
C
        DO 21 J=1,NDOF
            DO 21 I=1,NDOF
21     KSS(I,J)=KS(I,J)
C
C      Obtain reduced structural stiffness matrix
C
        DO 22 J=1,NDOF
            DO 22 I=1,NDOF
                IF((IDLIN(J).EQ.1).AND.(I.EQ.J)) KS(I,J)=1.0
22     IF((IDLIN(J).EQ.1).AND.(I.NE.J)) KS(I,J)=0.0

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C
      DO 23 I=1,NDOF
      DO 23 J=1,NDOF
23     IF((KS(I,I).EQ.0.0).AND.(J.NE.I)) KS(I,J)=0.0
      DO 24 J=1,NDOF
      DO 24 I=1,NDOF
24     RED(I,J)=KS(I,J)
      DO 25 I=1,NDOF
25     IF(IDLIN(J).EQ.1) P(J)=0.0
      WRITE(*,103)
C
C     Solve reduced system of equations using Gauss
C     elimination
C
C     a) Stiffness matrix
C
      DO 26 I=1,NDOF-1
      DO 26 J=1,NDOF
      IF(J.LE.I) GO TO 26
      IF(KS(I,J).EQ.0.0) GO TO 26
      FACTOR=KS(I,J)/KS(I,I)
      KS(I,J)=KS(I,J)-FACTOR*KS(I,I)
      DO 27 M=I+1,NDOF
27     KS(M,J)=KS(M,J)-FACTOR*KS(M,I)
C
C     b) Load vector
C
      P(J)=P(J)-FACTOR*P(I)
26     CONTINUE
      WRITE(*,104)
C
C     Check ill-conditioning of stiffness matrix
C
      ICONT=1
      DO 28 I=1,NDOF
      IF(KS(I,I).LT.0.0) WRITE(*,40) I,KS(I,I)
      IF(KS(I,I).EQ.0.0) ICONT=0
28     IF(KS(I,I).EQ.0.0) WRITE(*,41) I
      IF(ICONT.EQ.0) GO TO 100
C
C     Back-substitute to obtain displacement vector
C
      DO 29 JJ=1,NDOF
      J=NDOF-JJ+1
      SUM=0.0
      DO 30 I=J+1,NDOF
30     SUM=SUM+KS(I,J)*D(I)
29     D(J)=(P(J)-SUM)/KS(J,J)
      WRITE(*,105)
C

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C      Structure load vector {R} (incl. reactions at
C      supports)
C
      DO 31 J=1,NDOF
      RS(J)=0.0
      DO 31 I=1,NDOF
31     RS(J)=RS(J)+KSS(I,J)*D(I)
C
C      Structure load vector {R} including reactions due to
C      UD loads
C
      DO 32 I=1,NDOF
32     RS(I)=RS(I)+PP(I)
      DO 33 JNT=1,JNO
      DO 33 IDOF=1,6
      INOD=6*(JNT-1)
33     RS(INOD+IDOF)=RS(INOD+IDOF)+PFIX(JNT,IDOF)
C
C      Obtain member load vectors in local coordinates
C
      CALL LOAD
C
C      Output
C
      WRITE(*,106)
      CALL OUT
      GO TO 34
44     FORMAT(3(10X,G12.5))
39     FORMAT(//,25X,'Member No. ',I2,' - Stiffness matrix
&{k}',//)
45     FORMAT(//,25X,'Member No. ',I2,' - Rotation matrix
&{Ro}',//)
46     FORMAT(//,25X,'Member No. ',I2,' - Transformation
&matrix {T}',//)
47     FORMAT(//,25X,'Member No. ',I2,' - Transpose of
&Transformation matrix {Tt}',//)
C 34     FORMAT(//,25X,'Member No. ',I2,
C      &' - Stiffness matrix {k',1H','} (= {Tt}{k}{T})',//)
35     FORMAT(//,25X,'Member No. ',I2,
&' - Partitioned stiffness matrix {k11',1H','}',//)
36     FORMAT(//,25X,'Member No. ',I2,
&' - Partitioned stiffness matrix {k12',1H','}',//)
37     FORMAT(//,25X,'Member No. ',I2,
&' - Partitioned stiffness matrix {k21',1H','}',//)
38     FORMAT(//,25X,'Member No. ',I2,
&' - Partitioned stiffness matrix {k22',1H','}',//)
40     FORMAT(//,5X,'*** WARNING - Negative Diagonal Term -
&I = ',I2,5X,'KS = ',G12.5,//)
41     FORMAT(//,5X,'*** WARNING - I = ',I2,5X,
&'Stiffness Matrix Found Indeterminate',
&//,25X,'PROGRAM ABORTS',/)

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42   FORMAT(12(2X,G9.2))
43   FORMAT(6(5X,G12.5))
101  FORMAT(/,5X,'Member stiffness matrix {k} no',I3,'
&partitioned',/)
102  FORMAT(/,5X,'Structural stiffness matrix {K}
&assembled',/)
103  FORMAT(5X,'Reduction of {K} accomplished',/)
104  FORMAT(5X,'Upper triangular form of {K} obtained',/)
105  FORMAT(5X,'Displacements at all joints obtained',/)
106  FORMAT(5X,'Reactions at all joints obtained -
&Solution completed',/)
200  FORMAT(5X,'I = ',I2,2X,'M = ',I2,2X,'J = ',I2,2X,'KS
&',G12.5)
203  FORMAT(' I = ',I2,' IDOF= ',I2,' RS = ',G12.5)
100  CALL OUT
34   CONTINUE
     STOP
     END
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SUBROUTINE INITL
C
COMMON/real/ VAR1(1138146)
COMMON/mats/ VAR3(2000)
COMMON/ints/ IVAR(2210)
C
C Initialisations
C
DO 1 I=1,1138146
1 VAR1(I)=0.0
DO 3 I=1,2000
3 VAR3(I)=0.0
DO 5 I=1,2210
5 IVAR(I)=0
RETURN
END
SUBROUTINE PROPS
C
REAL IY,IZ,NU
COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),
&TW(100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TOR
&C(100),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),
&ZY(100),UDL(100),YS(100)
COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
&N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
&DOF,IOUT(100),IYLD(100,5),ISPAC
C
C Section properties for flat plating and attached
C stiffeners
C
DO 1 I=1,NUMSEC
AP=B(I)*TP(I)
AW=HW(I)*TW(I)
AF=BF(I)*TF(I)
AREA(I)=AP+AW+AF
IF(BF(I).EQ.0.0) TF(I)=0.0
IF(TF(I).EQ.0.0) BF(I)=0.0
C
C Flatbar stiffener
C
IF(BF(I).NE.0.0) GO TO 2
YZZ(I)=(AP*TP(I)/2.0+AW*(TP(I)+HW(I)/2.0))/AREA(I)
CGF1=B(I)/2.0
YYY(I)=(AP+AW)*CGF1/AREA(I)
C
IZ(I)=(B(I)*(TP(I)**3.0)+(HW(I)**3.0)*TW(I))/12.0+
&(HW(I)/2.0+TP(I)-YZZ(I))**2.0+HW(I)*TW(I)+
&B(I)*TP(I)*(YZZ(I)-TP(I)/2.0)**2.0
C
IY(I)=(AP*B(I)*B(I)+AW*TW(I)*TW(I))/12.0+
&AREA(I)*(B(I)-YYY(I))*(B(I)-YYY(I))

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        GO TO 3
C
C      b) T-bar or angle-bar stiffener
C
2  YZZ(I)=(B(I)*(TP(I)**2.0)/2.0+(HW(I)**2.0)*
    &TW(I)/2.0+HW(I)*TP(I)*TW(I)+BF(I)*TF(I)*HW(I)+
    &BF(I)*TF(I)*TP(I)+BF(I)*(TF(I)**2.0)/2.
    &0)/(B(I)*TP(I)+HW(I)*TW(I)+BF(I)*TF(I))
    CGF1=B(I)/2.0
    CGF2=CGF1
    IANG=0
    IF(IANG.EQ.1) CGF2=CGF2+BF(I)/2.0
    YYY(I)=((AP+AW)*CGF1+AF*CGF2)/AREA(I)
C
    IZ(I)=(B(I)*(TP(I)**3.0)+TW(I)*(HW(I)**3.0)+
    &BF(I)*(TF(I)**3.0))/12.0+B(I)*TP(I)*(YZZ(I)-
    &TP(I)/2.0)**2.0+HW(I)*TW(I)*(HW(I)/2.0+TP(I)
    &-YZZ(I))**2.0+BF(I)*TF(I)*(HW(I)+TP(I)+TF(I)/2.0
    &-YZZ(I))**2.
C
    IY(I)=(AP*B(I)*B(I)+AW*TW(I)*TW(I)+AF*BF(I)*
    &BF(I))/12.0+AREA(I)*(B(I)-YYY(I))*(B(I)-YYY(I))
C
3  CONTINUE
C
    RADZ(I)=SQRT(IZ(I)/AREA(I))
    RADY(I)=SQRT(IY(I)/AREA(I))
    ZZ(I)=IZ(I)/YZZ(I)
    ZY(I)=IY(I)/YYY(I)
    TORC1=0.0
    TORC(I)=AP*TP(I)*TP(I)+AW*TW(I)*TW(I)+AF*TF(I)*TF(I)
    TORC(I)=TORC(I)/3.0
1  CONTINUE
C
    RETURN
    END

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SUBROUTINE PARSOL(IMEM)
C
  REAL IZ,IY,K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ,
&LENXZ,LEN1,NU

  COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
&),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
&KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
&,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
&,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100
&,5),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
&2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PFIK
&(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
&LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)
  COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
&N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
&DOF,IOUT(100),IYLD(100,5),ISPAC
  COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),TW
&(100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TORC(
&100),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),ZY
&(100),UDL(100),YS(100)

C
C   Reactions pz1, pz2 and moments mz1, mz2 on loaded mem
C   ber
C
  PML(IMEM,3)=-UDL(IMEM)*L(IMEM)/2.0
  PML(IMEM,9)=PML(IMEM,3)
C
  PML(IMEM,5)=-UDL(IMEM)*L(IMEM)*L(IMEM)/12.0
  PML(IMEM,11)=-PML(IMEM,5)
  RETURN
  END

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      SUBROUTINE STIF(I,ISEC,E,NU,AREA,L,IZ,IY,TORC,K)
C
      REAL IY,IZ,K,L,L1,L2,L3,NU
      DIMENSION E(100),NU(100),AREA(100),IZ(100),IY(100),
&TORC(100),K(12,12),L(100),ISEC(100)
C
      IS=ISEC(I)
      L1=1.0/L(IS)
      L2=1.0/(L(IS)*L(IS))
      L3=1.0/(L(IS)*L(IS)*L(IS))
      TORQ=TORC(IS)/(2.0*L(IS)*(1.0+NU(IS)))
C
      DO 1 J1=1,12
      DO 1 J2=1,12
1     K(J1,J2)=0.0
C
C     Non-zero upper triangular elements of member stiffness
C     matrix {k}
C
      K(1,1)  =+AREA(IS)*L1
      K(7,1)  =-AREA(IS)*L1
      K(2,2)  =+12.0*IZ(IS)*L3
      K(6,2)  =+6.0*IZ(IS)*L2
      K(8,2)  =-12.0*IZ(IS)*L3
      K(12,2) =+6.0*IZ(IS)*L2
      K(3,3)  =+12.0*IY(IS)*L3
      K(5,3)  =-6.0*IY(IS)*L2
      K(9,3)  =-12.0*IY(IS)*L3
      K(11,3) =-6.0*IY(IS)*L2
      K(4,4)  =+TORQ
      K(10,4) =-TORQ
      K(5,5)  =+4.0*IY(IS)*L1
      K(9,5)  =+6.0*IY(IS)*L2
      K(11,5) =+2.0*IY(IS)*L1
      K(6,6)  =+4.0*IZ(IS)*L1
      K(8,6)  =-6.0*IZ(IS)*L2
      K(12,6) =+2.0*IZ(IS)*L1
      K(7,7)  =+AREA(IS)*L1
      K(8,8)  =+12.0*IZ(IS)*L3
      K(12,8) =-6.0*IZ(IS)*L2
      K(9,9)  =+12.0*IY(IS)*L3
      K(11,9) =+6.0*IY(IS)*L2
      K(10,10)=+TORQ
      K(11,11)=+4.0*IY(IS)*L1
      K(12,12)=+4.0*IZ(IS)*L1
C
C     Symmetry about leading diagonal
C
      DO 2 J1=1,12
      DO 2 I1=1,12

```

```

      K(I1,J1)=E(IS)*K(I1,J1)
2    IF(J1.GT.I1) K(I1,J1)=K(J1,I1)
      RETURN
      END
      SUBROUTINE ROT(I,ISPAC,ANG,R,T,TT,L,LX,LY,LZ,
C     LEN1,LENXZ)
C
      REAL L,LX,LY,LZ,LEN1,LENXZ
      DIMENSION T(100,12,12),TT(100,12,12),R(3,3),ANG(100),
&L(100),LX(100),LY(100),LZ(100),LEN1(100),LENXZ(100)
C
C     Rotation Matrix {Ro}
C
      SS=SIN(ANG(I))
      CS=COS(ANG(I))
      ABSS=ABS(SS)
      ABCS=ABS(CS)
      IF(ABSS.LT.0.10E-02) SS=0.0
      IF(ABCS.LT.0.10E-02) CS=0.0
      IF(ISPAC.EQ.1) GO TO 1
C
      R(1,1)=CS
      R(2,1)=SS
      R(1,2)=-SS
      R(2,2)=CS
      R(3,3)=1.0
      GO TO 2
C
1    R(1,1)=LX(I)/L(I)
      R(2,1)=LY(I)/L(I)
      R(3,1)=LZ(I)/L(I)
      R(1,2)=-LX(I)*LY(I)*CS
      R(1,2)=R(1,2)-L(I)*LZ(I)*SS
      R(1,2)=R(1,2)/LEN1(I)
      R(2,2)=LENXZ(I)*CS/L(I)
      R(3,2)=-LY(I)*LZ(I)*CS
      R(3,2)=R(3,2)+L(I)*LX(I)*SS
      R(3,2)=R(3,2)/LEN1(I)
      R(1,3)=LX(I)*LY(I)*SS
      R(1,3)=R(1,3)-L(I)*LZ(I)*CS
      R(1,3)=R(1,3)/LEN1(I)
      R(2,3)=-LENXZ(I)*SS/L(I)
      R(3,3)=LY(I)*LZ(I)*SS
      R(3,3)=R(3,3)+L(I)*LX(I)*CS
      R(3,3)=R(3,3)/LEN1(I)
C
      ISET=0
      IF((LX(I).EQ.0.0).AND.(LZ(I).EQ.0.0)) ISET=1
      IF(ISET.EQ.0) GO TO 3
      R(1,2)=1.0
      R(3,2)=1.0

```

```

        R(1,3)=1.0
        R(3,3)=1.0
    3  CONTINUE
C
C      Transformation Matrix {T}
C
    2  T(I,1,1)=R(1,1)
        T(I,2,1)=R(2,1)
        T(I,1,2)=R(1,2)
        T(I,2,2)=R(2,2)
        T(I,3,3)=R(3,3)
        T(I,4,4)=R(1,1)
        T(I,5,4)=R(2,1)
        T(I,4,5)=R(1,2)
        T(I,5,5)=R(2,2)
        T(I,6,6)=R(3,3)
        T(I,7,7)=R(1,1)
        T(I,8,7)=R(2,1)
        T(I,7,8)=R(1,2)
        T(I,8,8)=R(2,2)
        T(I,9,9)=R(3,3)
        T(I,10,10)=R(1,1)
        T(I,11,10)=R(2,1)
        T(I,10,11)=R(1,2)
        T(I,11,11)=R(2,2)
        T(I,12,12)=R(3,3)
C
C      Transpose of transformation matrix {Tt}
C
        DO 4 J=1,12
        DO 4 I1=1,12
    4  TT(I,I1,J)=T(I,J,I1)
        RETURN
        END

```



```

SUBROUTINE STIFGL(IMEM)
C
  REAL K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ
C
  &,LENXZ,LEN1

  COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
&),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
&KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
&,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
&,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100
&,5),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
&2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PFIK
&(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
&LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)

C
C   Member stiffness matrix in global coordinates {k'}
C
  DO 1 J=1,12
  DO 1 I=1,12
  SUM=0.0
  DO 2 M=1,12
2  SUM=SUM+K(M,J)*T(IMEM,I,M)
  PROD(I,J)=SUM
1  CONTINUE

C
  DO 3 J=1,12
  DO 3 I=1,12
  SUM=0.0
  DO 4 M=1,12
4  SUM=SUM+TT(IMEM,M,J)*PROD(I,M)
  K(I,J)=SUM
3  CONTINUE
  RETURN
  END

```

```

SUBROUTINE LOAD
C
  REAL IZ,IY,K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ,
  &LENXZ,LEN1,NU

  COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
  &),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
  &KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
  &,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
  &,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100
  &,5),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
  &2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PFIX
  &(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
  &LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)
  COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
  &N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
  &DOF,IOUT(100),IYLD(100,5),ISPAC
  COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),TW
  &(100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TORC(
  &100),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),ZY
  &(100),UDL(100),YS(100)
C
C   DMG - member displacement vectors in global co-ordi-
C   nates {r'}
C
  DO 8 IMEM=1,MNO
  X(1)=0.0
  X(2)=L(IMEM)*0.25
  X(3)=L(IMEM)*0.50
  X(4)=L(IMEM)*0.75
  X(5)=L(IMEM)
C
  JN1=J1(IMEM)
  JN2=J2(IMEM)
  DO 1 IDOF=1,6
  JF=6*(JN1-1)
1  DMG(IMEM,IDOF)=D(JF+IDOF)
  DO 2 IDOF=1,6
  JF=6*(JN2-1)
2  DMG(IMEM,6+IDOF)=D(JF+IDOF)
C
C   DML - member displacement vectors in local coordinates
C   {r}={T}{r'}
C
  DO 3 J=1,12
  DML(IMEM,J)=0.0
  DO 3 I=1,12
3  DML(IMEM,J)=DML(IMEM,J)+T(IMEM,I,J)*DMG(IMEM,I)
C
  ISNO=ISEC(IMEM)

```

```

DENOM=24.0*E(ISNO)*IZ(ISNO)
UDL1=UDL(IMEM)/DENOM
DO 4 I=1,5
C1=X(I)-L(IMEM)
C2=C1*C1
C3=X(I)*X(I)
DMEM(IMEM,I)=UDL1*C3*C2
C4=X(I)/L(IMEM)
C5=DML(IMEM,9)-DML(IMEM,3)
C6=DML(IMEM,3)+C5*C4
4 DMEM(IMEM,I)=DMEM(IMEM,I)+C6
C
C RML - member load vectors in local coords {p}={k}{r}
C
DO 5 J=1,12
RML(IMEM,J)=0.0
DO 5 I=1,12
5 RML(IMEM,J)=RML(IMEM,J)+KMEM(IMEM,I,J)*DML(IMEM,I)
C
C RMG - member load vectors in global coords
C {p'}={Tt}{p}
C
DO 9 J=1,12
RMG(IMEM,J)=0.0
DO 9 I=1,12
9 RMG(IMEM,J)=RMG(IMEM,J)+TT(IMEM,I,J)*RML(IMEM,J)
C
C Bending Moments in each member (at x=0, L/4, L/2,
C 3L/4, L)
C
L6 =L(IMEM)/6.0
UDL2=UDL(IMEM)/12.0
C
DO 6 I=1,5
C1=X(I)-L(IMEM)
C2=6.0*X(I)*C1
C3=L(IMEM)*L(IMEM)
C4=C2+C3
BMOM(IMEM,I)=UDL2*C4
C5=RML(IMEM,11)+RML(IMEM,5)
C6=X(I)/L(IMEM)
C7=C5*C6
C8=RML(IMEM,5)-C7
BMOM(IMEM,I)=BMOM(IMEM,I)+C8
6 WRITE(*,13) IMEM,I,BMOM,C8,C7,C6,C5,C4,C3,C2,C1
13 FORMAT(2(2X,I2),9(2X,G10.3))
C
C Maximum total stresses in each member at each location
C
YMAX=HW(ISNO)+TP(ISNO)+TF(ISNO)-YZZ(ISNO)
IF(YMAX.LT.YZZ(ISNO)) YMAX=YZZ(ISNO)

```

```
ZMIN=IZ( ISNO ) / YMAX
SXC=PML( IMEM, 1 ) / AREA( ISNO )
DO 7 I=1, 5
SXB=BMOM( IMEM, I ) / ZMIN
SX( IMEM, I ) =SXB+SXC
C
C      Design criterion
C
STRES=1.2*ABS( SX( IMEM, I ) )
IF( STRES.GT.YS( ISNO ) ) IYLD( IMEM, I )=1
7  CONTINUE
8  CONTINUE
RETURN
END
```

```
SUBROUTINE INPUT
```

```
C
```

```
REAL IZ,IY,K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ,
C &LENXZ,LEN1,NU
```

```
COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
&),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
&KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
&,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
&,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100
&,5),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
&2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PFIK
&(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
&LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)
```

```
COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
&N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
&DOF,IOUT(100),IYLD(100,5),ISPAC
```

```
COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),TW
&(100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TORC(
&100),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),ZY
&(100),UDL(100),YS(100)
```

```
C
```

```
90 FORMAT(20(/),30X,25(' . '))
91 FORMAT(30X,
&' . Linear Elastic Analysis of a 3-D Grillage .')
92 FORMAT(30X,
&' . using the Matrix Stiffness Method .')
93 FORMAT(30X,25(' . '),35(/))
94 FORMAT(30X,' . ',47X,' . ')
10 FORMAT(6X,'No of members',2X,I3,6X,'No of
&joints',2X,I3,6X,'No of section types',2X,I2,/)
11 FORMAT(/,6X,'Joint No.',16X,'X Coord',20X,'Y Co
&ord',20X,'Z Coord',/)
12 FORMAT(/,6X,'Member No',4X,'Jnt No. at end 1',4X,
&'Jnt No at end 2',4X,'Section No.',5X,'Length',14X,
&'Angle',/)
88 FORMAT(/,2X,'Sect No',6X,'E',10X,'nu',12X,'ys',12X,
&'bp',13X,'tp',12X,'hw',12X,'tw',12X,'bf',12X,'tf'
&,/,13X,'N/mm2',20X,'N/mm2',12X,'mm',12X,'mm',
&12X,'mm',12X,'mm',12X,'mm',12X,'mm2',/)
95 FORMAT(/,2X,'Sect No',4X,'Yzz',11X,'Izz',11X,'Zzz',
&11X,'Rzz',11X,'Yyy',12X,'Iyy',10X,'Zyy',11X,'Ryy',
&15X,'J',/,12X,' mm',12X,'mm4',11X,'mm3',11X,'mm',12X,
&'mm',12X,'mm4',10X,'mm3',11X,'mm',14X,'mm4',/)
89 FORMAT(5X,I2,10(2X,G12.5))
14 FORMAT(25X,'Joint Loads',/,15X,'Joint
&No.',10X,'Degree of freedom no.',10X,'Load',/)
37 FORMAT(/,25X,'Uniformly Distributed Loads',
&/,15X,'Member No.',21X,'Load',/)
15 FORMAT(34X,'Suppressions',/,28X,'Joint No.',10X,
&'d.o.f.',/)
23 FORMAT(/,6X,'Member No. d.o.f. Applied
```

```

&load', //)
21  FORMAT(/, 22X, 'Member No ', I2, 12X, 'Uniformly distrib
&uted load = ', G12.5, ' N/mm')
C
26  FORMAT(8X, I3, 19X, F8.2, 19X, F8.2, 19X, F8.2)
27  FORMAT(10X, I2, 15X, I2, 18X, I2, 14X, I2, 9X, F9.3, 9X, F9.3)
28  FORMAT(5X, I3, 6(4X, G12.5))
29  FORMAT(//)
35  FORMAT(32X, I2, 15X, I2)
36  FORMAT(18X, I2, 23X, I2, 18X, G12.5)
38  FORMAT(18X, I2, 23X, F8.3)
C
C   Screen output
C
C   WRITE(*, 29)
C   WRITE(*, 10) MNO, JNO, NUMSEC
C   WRITE(*, 11)
C   WRITE(*, 26) (I, XJC(I), YJC(I), ZJC(I), I=1, JNO)
C   WRITE(*, 29)
C   WRITE(*, 12)
C   WRITE(*, 27) (I, J1(I), J2(I), ISEC(I), L(I),
&ANG(I), I=1, MNO)
C   WRITE(*, 29)
C   WRITE(*, 88)
C   DO 5 I=1, NUMSEC
C 5  WRITE(*, 89) I, E(I), NU(I), YS(I), B(I), TP(I),
&HW(I), TW(I), BF(I), TF(I)
C   WRITE(*, 95)
C   DO 6 I=1, NUMSEC
C 6  WRITE(*, 89) I, YZZ(I), IZ(I), ZZ(I), RADZ(I), YYY(I), IY(I),
&ZY(I), RADY(I), TORC(I)
C   WRITE(*, 29)
C   WRITE(*, 14)
C   DO 1 JNT=1, JNO
C   DO 1 IDOF=1, 6
C 1  IF(PJNT(JNT, IDOF).NE.0.0) WRITE(*, 36) JNT, IDOF,
&PJNT(JNT, IDOF)
C   WRITE(*, 29)
C   WRITE(*, 15)
C   DO 2 JNT=1, JNO
C   DO 2 IDOF=1, 6
C 2  IF(ID(JNT, IDOF).EQ.1) WRITE(*, 35) JNT, IDOF
C
C   File output
C
C   WRITE(6, 90)
C   WRITE(6, 94)
C   WRITE(6, 94)
C   WRITE(6, 91)
C   WRITE(6, 94)

```

```

WRITE(6,94)
WRITE(6,92)
WRITE(6,94)
WRITE(6,94)
WRITE(6,93)
WRITE(6,29)
WRITE(6,10) MNO,JNO,NUMSEC
WRITE(6,11)
WRITE(6,26) (I,XJC(I),YJC(I),ZJC(I),I=1,JNO)
WRITE(6,29)
WRITE(6,12)
WRITE(6,27) (I,J1(I),J2(I),ISEC(I),L(I),
&ANG(I),I=1,MNO)
WRITE(6,29)
WRITE(6,88)
DO 8 I=1,NUMSEC
8 WRITE(6,89) I,E(I),NU(I),YS(I),B(I),TP(I),HW(I),TW(I),
&BF(I),TF(I)
WRITE(6,95)
DO 9 I=1,NUMSEC
9 WRITE(6,89) I,YZZ(I),IZ(I),ZZ(I),RADZ(I),YYY(I),IY(I),
&ZY(I),RADY(I),TORC(I)
WRITE(6,29)
WRITE(6,14)
DO 3 JNT=1,JNO
DO 3 IDOF=1,6
3 IF(PJNT(JNT,IDOF).NE.0.0) WRITE(6,36) JNT,IDOF,
&PJNT(JNT,IDOF)
WRITE(6,37)
DO 7 IMEM=1,MNO
7 IF(UDL(IMEM).NE.0.0) WRITE(6,38) IMEM,UDL(IMEM)
WRITE(6,29)
WRITE(6,15)
DO 4 JNT=1,JNO
DO 4 IDOF=1,6
4 IF(ID(JNT,IDOF).EQ.1) WRITE(6,35) JNT,IDOF
RETURN
END

```

```

SUBROUTINE OUT
C
  REAL IZ,IY,K,KMEM,KSS,KS,K11,K12,K21,K22,L,LX,LY,LZ,
&LENXZ,LEN1,NU
  COMMON/real/R(3,3),T(100,12,12),TT(100,12,12),K(12,12
&),P(600),D(600),PJNT(100,6),PMG(100,12),KSS(600,600),
&KS(600,600),XJC(100),YJC(100),X1(100),Y1(100),X2(100)
&,Y2(100),K11(6,6),K12(6,6),K21(6,6),K22(6,6),ANG(100)
&,L(100),PROD(12,12),RED(600,600),PML(100,12),BMOM(100,1
&2,12),SX(100,5),X(5),DMG(100,12),DML(100,12),KMEM(100,1
&2,12),RML(100,12),RMG(100,12),PP(600),PJP(100,6),PFIX
&(100,6),RS(600),DMEM(100,5),Z1(100),Z2(100),ZJC(100),
&LX(100),LY(100),LZ(100),LENXZ(100),LEN1(100)
  COMMON/ints/MNO,JNO,ISSNO,ICLNO,LC,NUMSEC,ID(100,6),J
&N(100),J1(100),J2(100),ISEC(100),IDLIN(600),JNUM(2),N
&DOF,IOUT(100),IYLD(100,5),ISPAC
  COMMON/mats/ E(100),NU(100),B(100),TP(100),HW(100),TW
&(100),BF(100),TF(100),AREA(100),IZ(100),IY(100),TORC(
&100),YZZ(100),RADZ(100),ZZ(100),YYY(100),RADY(100),ZY&
(100),UDL(100),YS(100)
C
10 FORMAT(//,25X,'Structural stiffness matrix {K}
  &({Tt}){k}{T}',//)
11 FORMAT(//,25X,'Reduced structural stiffness matrix
  &{K}',//)
12 FORMAT(//,25X,'Upper triangular form of the reduced'
  &'structural stiffness matrix {K}',//)
20 FORMAT(/,5X,'Member No.',I2,6X,'{r',2H'}',11X,
  &'{p',2H'}',11X,'{r}',11X,'{p}',/)
13 FORMAT(//,18X,'Displacements and support reactions
  &(global coords)',//,33X,'{D}',12X,'{P}',//)
16 FORMAT(//,8X,'Member No. ',25X,'Bending Mo
  &ments',//,23X,'0',13X,'L/4',12X,'L/2',12X,
  &'3L/4',11X,'L',/)
17 FORMAT(//,8X,'Member No.',20X,'Max total stresses
  &{s}',//,23X,'0',12X,'L/4',12X,'L/2',12X,
  &'3L/4',11X,'L',/)
23 FORMAT(//,8X,'Member No.',20X,'Deflections along mem
  &ber length',//,23X,'0',12X,'L/4',12X,'L/2',12X,
  &'3L/4',11X,'L',/)
24 FORMAT(//,8X,'Member No.',20X,'Member loads
  &{p',2H'}',//,23X,'3',13X,'4',13X,'5',13X,'9',
  &13X,'10',12X,'11',/)
21 FORMAT(/,11X,'Yielding is occurring in the following
  &members',//,10X,'No.',10X,'Member No.',11X,
  &'Longl bend. stress',/)
14 FORMAT(7(2X,G12.5))
15 FORMAT(15X,I3,10X,2(2X,G12.5))
16 FORMAT(12(2X,G9.2))
19 FORMAT(15X,I2,5(2X,G12.5))

```



```

24  FORMAT(9X,I3,13X,I3,14X,G12.5)
26  FORMAT(15X,I2,6(2X,G12.5))
C
C   WRITE(6,10)
C   WRITE(6,16) ((KSS(I,J),I=1,12),J=1,NDOF)
C   WRITE(6,10)
C   WRITE(6,16) ((KSS(I,J),I=13,24),J=1,NDOF)
C   WRITE(6,11)
C   WRITE(6,16) ((RED(I,J),I=1,12),J=1,NDOF)
C   WRITE(6,11)
C   WRITE(6,16) ((RED(I,J),I=13,24),J=1,NDOF)
C   WRITE(6,12)
C   WRITE(6,16) ((KS(I,J),I=1,12),J=1,NDOF)
C   WRITE(6,12)
C   WRITE(6,16) ((KS(I,J),I=13,24),J=1,NDOF)
C
C   WRITE(6,13)
C   DO 3 J=1,NDOF
C 3  WRITE(6,15) J,D(J),RS(J)
C   DO 4 IMEM=1,MNO
C   IF(IOUT(IMEM).EQ.0) GO TO 4
C   WRITE(6,20) IMEM
C   DO 5 IDOF=1,12
C   WRITE(6,19) IDOF,DMG(IMEM,IDOF),RMG(IMEM,IDOF),
&DML(IMEM,IDOF),RML(IMEM,IDOF)
4  CONTINUE
C   WRITE(6,17)
C   DO 7 IMEM=1,MNO
7  WRITE(6,19) IMEM,(BMOM(IMEM,I),I=1,5)
C   WRITE(6,18)
C   DO 6 IMEM=1,MNO
6  WRITE(6,19) IMEM,(SX(IMEM,I),I=1,5)
C   WRITE(6,23)
C   DO 8 IMEM=1,MNO
8  WRITE(6,19) IMEM,(DMEM(IMEM,I),I=1,5)
C   WRITE(6,25)
C   DO 21 IMEM=1,MNO
22 WRITE(6,26) IMEM,RMG(IMEM,3),RMG(IMEM,4),
&RMG(IMEM,5),RMG(IMEM,9),RMG(IMEM,10),RMG(IMEM,11)
C   KOUNT=0
C   WRITE(6,22)
C   DO 9 IMEM=1,MNO
C   DO 9 I=1,5
C   IF(IYLD(IMEM,I).EQ.1) KOUNT=KOUNT+1
9  IF(IYLD(IMEM,I).EQ.1) WRITE(6,24) KOUNT,IMEM,
&SX(IMEM,I)
C   RETURN
C   END

```